

# Pavement Thickness Design Parameter Impacts



2012 Municipal Streets Seminar  
November 14, 2012

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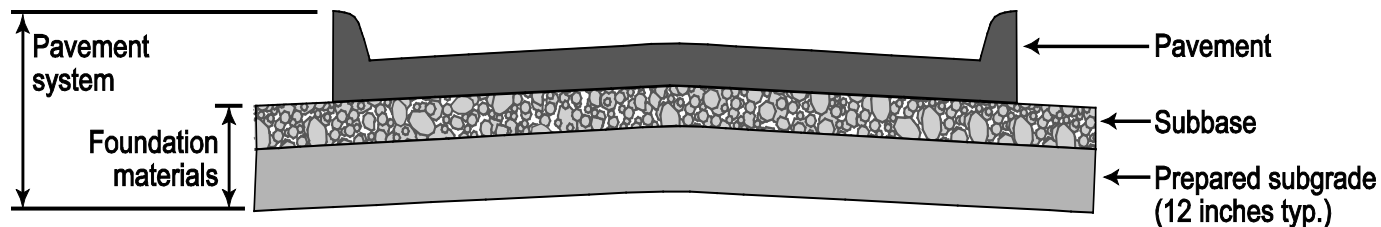


# Pavement Thickness Design

- How do cities decide how thick to build their pavements?
  - A data-based analysis
  - Use same thickness streets based on what we have always done
  - Use standard thicknesses based on your city's policies
  - Discuss it with a contractor and do what you can afford

# Pavement Thickness Design

- Correct answer – A data-based analysis!
- Doesn't have to be difficult and time consuming
- Several methods available, but design information generally the same
- Terminology:



# Pavement Thickness Design

- Good design uses these parameters:
  - Soil characteristics (subgrade)
  - Soil compaction (CBR or DCP)
  - Use of subbase
  - Traffic volumes including % trucks
  - Design Life – 20 to 50 years
  - Expected traffic growth per year over design life
  - Type of pavement – HMA or PCC

# Pavement Thickness Design

- Serviceability index
  - Rating system from 5 (perfect) to 0 (impassable)
  - New PCC = 4.5; New HMA = 4.2
  - Terminal Serviceability,  $P_t$

$P_t$	Classifications
2.00	Secondary Roads and Local Residential Streets
2.25	Minor Collectors, Industrial, and Commercial Streets
2.50	Major Collectors and Arterials

# Pavement Thickness Design

- Design Life
  - Old standard = 20 years
  - Current recommendation = 50 years
    - Streets will perform longer and better
    - Limited funds for major rehab and reconstruction



# Pavement Thickness Design

- Design Traffic
  - Average daily traffic volume
  - Percent trucks on the street
    - Usually 2% – 5%
    - Be aware of unusual situations, even if low volume
  - Annual growth rate
    - Usually 2%
  - Length of the analysis period
    - 50 years

# Pavement Thickness Design

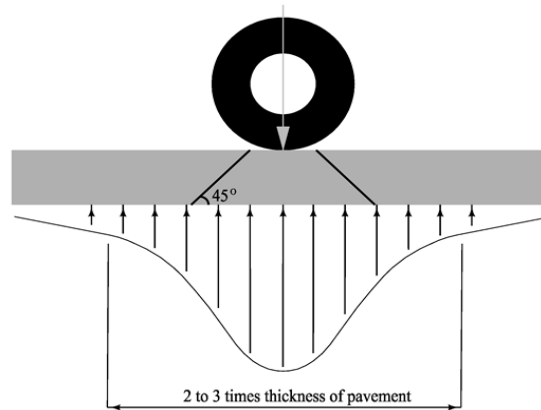
- Truck traffic
  - Cars don't count – trucks wear out streets
  - Equivalent single axle loads (ESALS)
    - 18,000 pound load used as the standard
    - Different truck types are converted to ESALS
    - Measure of the pavement damage created
  - Different values for PCC and HMA pavements due to different damage created



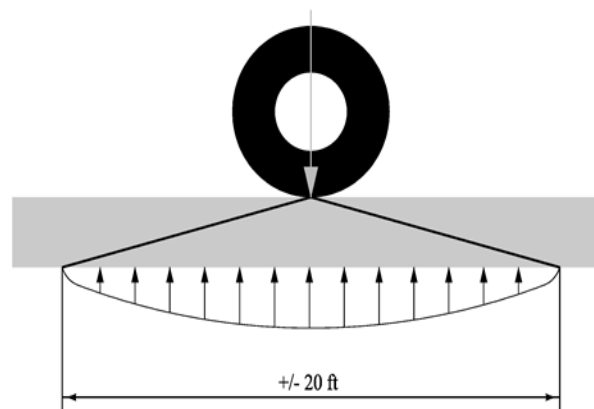
# Pavement Thickness Design

- Pavement Loading Distribution

- HMA



- PCC



# Pavement Thickness Design

- Soil Resilient Modulus  $M_R$ 
  - Property of the soil indicating the stiffness or elasticity of the soil under dynamic loading
  - Calculated based on California Bearing Ratio (CBR)

<b>CBR Value</b>	<b><math>M_R</math> Value</b>
3	4120
5	5840
10	9400

- Simple strength test comparing a given soil with well-graded crushed stone
  - Used in both HMA and PCC design processes
  - Used directly for HMA design

# Pavement Thickness Design

- For PCC, use Modulus of Subgrade Reaction
  - For concrete pavements, uniformity of support is paramount
  - Modulus of Subgrade reaction,  $k = M_R / 19.4$
  - Composite Modulus of Subgrade Reaction = ( $k_c$ )
    - Used when a subbase is used
    - Represents the strength of the support layer corrected for the additional support from the subbase material

# Pavement Thickness Design

- Other important design elements
  - Reliability that the design will exceed the life of the pavement
  - Standard deviation based on AASHTO equations
  - PCC properties
    - Modulus of Elasticity and Modulus of Rupture
  - HMA layer coefficients
    - Used to generate structural numbers
  - Drainage – how long is the subgrade/subbase saturated?
  - Loss of support – PCC only; potential loss of subgrade support due to erosion or differential soil movement

# Pavement Thickness Design

- Remember - I said this was easy – right??



# Pavement Thickness Design

- Design Methods
  - Asphalt Paving Associations
    - APAI I-Pave (Iowa)
    - PerRoadXpress (Asphalt Institute)
  - American Concrete Paving Association
    - StreetPave
  - AASHTO 1993 Pavement Design Guide
  - SUDAS
    - Section 5F-1

# Pavement Thickness Design

- Different design methods give different results based on inputs/default values used in the software/process
- Pavement design is not exact, so ranges of variables are often available
- Within the software, some inputs can be changed and other defaults are not available to users

# Pavement Thickness Design

- Design Example:
  - Two lanes
  - Collector classification
  - Average Annual Daily Traffic = 5,000 vpd
  - Percent trucks = 4%
  - Design period = 50 years
  - Annual traffic growth rate = 2%



# Pavement Thickness Design

- Asphalt Paving Association
  - I-Pave - Iowa
  - PerRoadXpress - National





# I-PAVE

## LOW VOLUME ROAD DESIGN GUIDE

DESIGNED BY

**Joseph Podolsky**

Department of Civil, Construction and Environmental Engineering  
Iowa State University

IN COOPERATION WITH



ASPHALT PAVING  
ASSOCIATION  
OF IOWA

IOWA STATE UNIVERSITY  
Department of Civil Engineering



# I-PAVE

LOW VOLUME ROAD DESIGN GUIDE

INPUT

FLEXIBLE

RIGID

FLEX LCCA

RIGID LCCA

SOIL DATA

PRINT

CONTACT

Project Name

Harrington Dr.

Location

Ankeny

County

Polk

Design Period (Y) Years

50

## STRUCTURE

	Flexible	Rigid
Stone Base Thickness, in	6	6
Subbase Stabilization Depth, in	12	12
Subbase Soil Type	Unsuitable (Poor)	

Lane Configuration

2

Average Daily Traffic (ADT)

5000

Percent Trucks (T)

4%

Annual Growth Rate (%)

2

## ESALS

Terminal Serviceability, pt

2.25

Reliability, R (%)

88

Run Calculations



# I-PAVE

LOW VOLUME ROAD DESIGN GUIDE

INPUT

FLEXIBLE

RIGID

FLEX LCCA

RIGID LCCA

SOIL DATA

PRINT

CONTACT

\*AASHTO 1993 (<http://training.ce.washington.edu/PGI/>)

log(W18) Input	6.20205564901158
log(W18) Predicted	6.20205842324901
Standard Normal Deviate, ZR	-
	1.17498679174602
Standard Deviation, S0	0.45
ΔPSI	1.95
Effective Subgrade Resilient Modulus, MR (psi)	10000
Structural Number, SN	3.22721000001267
Crushed Stone Elastic Modulus, E2 (psi)	30000
Subgrade Layer Coeff., a3	0
Stabilized Depth, D3	12
Subgrade moisture coeff., m3	1
Granular Subbase Layer Coeff., a2	0.14
Granular Subbase Thickness, D2 (in)	6
Subbase moisture coeff., m2	1
HMA Layer Coefficient, a1	0.44
D1	5.42547727275608
D1 Final	5.5
D1Final2	5.5

$$\log_{10}(W_{18}) = Z_R \times S_o + 9.36 \times \log_{10}(SN+1) - 0.20 + \frac{\log_{10}\left(\frac{\Delta PSI}{4.2-1.5}\right)}{0.40 + \frac{1094}{(SN+1)^{5.19}}} + 2.32 \times \log_{10}(M_R) - 8.07$$

(these variables will be further explained in [Section 3.1.2, Inputs](#))

where:  $W_{18}$  = predicted number of 80 kN (18,000 lb.) ESALS

$Z_R$  = [standard normal deviate](#)

$S_o$  = [combined standard error of the traffic prediction and performance prediction](#)

SN = [Structural Number](#) (an index that is indicative of the total pavement thickness required)

=  $a_1D_1 + a_2D_2m_2 + a_3D_3m_3 + \dots$

$a_i$  =  $i^{\text{th}}$  layer coefficient

$D_i$  =  $i^{\text{th}}$  layer thickness (inches)

$m_i$  =  $i^{\text{th}}$  layer drainage coefficient

DPSI = difference between the initial design [serviceability index](#),  $p_o$ , and the design terminal serviceability index,  $p_t$

$M_R$  = [subgrade resilient modulus](#) (in psi)



# I-PAVE

LOW VOLUME ROAD DESIGN GUIDE

INPUT	FLEXIBLE	RIGID	FLEX LCCA	RIGID LCCA	SOIL DATA	PRINT	CONTACT
-------	----------	-------	-----------	------------	-----------	-------	---------

Terminal Serviceability, pt 2.25  
Reliability, R (%) 88

\*Wang, 2008, [http://www.intrans.iastate.edu/reports/mepdq\\_testing.pdf](http://www.intrans.iastate.edu/reports/mepdq_testing.pdf)  
\*\*Method 1

log(W18) Input	6.439
log(W18) Predicted	6.35
Standard Normal Deviate, Z <sub>R</sub>	-1.175
Standard Deviation, S <sub>0</sub>	0.35
*Concrete Modulus of Rupture, S <sub>c</sub> (psi)	646
Drainage Coeff., C <sub>d</sub>	1
Load Transfer Coeff., J	3.2
Concrete Elastic Modulus E <sub>c</sub> , psi	4200000
**Modulus of Subgrade Reaction, k (psi/in)	333.33
ΔPSI	2.25
Trial Thickness, D	7.163
Final Thickness, DF	7.5

\*Minimum cover requirements limit thickness to 6" for 1 inch dowel bars  
(<http://www.fhwa.dot.gov/pavement/t504030.cfm>)

$$\log_{10}(W_{18}) = Z_R \times S_0 + 7.35 \times \log_{10}(D+1) - 0.06 + \frac{\log_{10}\left(\frac{\Delta PSI}{4.5-1.5}\right)}{1 + \frac{1.624 \times 10^7}{(D+1)^{8.46}}} + (4.22 - 0.32p_t) \times \log_{10} \left[ \frac{(S'_c)(C_d)(D^{0.75} - 1.132)}{215.63(J) \left( D^{0.75} - \frac{18.42}{\left(\frac{E_c}{k}\right)^{0.25}} \right)} \right]$$

(these variables will be further explained in [Section 4.1.2, Inputs](#))

where: W<sub>18</sub> = predicted number of 80 kN (18,000 lb.) ESALs

Z<sub>R</sub> = [standard normal deviate](#)



# I-PAVE

LOW VOLUME ROAD DESIGN GUIDE

INPUT	FLEXIBLE	RIGID	FLEX LCCA	RIGID LCCA	SOIL DATA	PRINT	CONTACT
-------	----------	-------	-----------	------------	-----------	-------	---------

### Relative Quality of Roadbed Soil

Iowa Soil Type	CBR	R-value	Layer Coefficient	DCP (in/blow)	Resilient Modulus Range (Low Moisture to High Moisture), psi		Resilient Modulus, psi	k-value (psi/in), Method 1	k-value (psi/in), Method 2
Select	7	13	0.04	0.56	2,905	11,865	7,385	246	251.00
Suitable	6	11	0.03	0.64	2,765	11,249	7,007	234	232.00
Unsuitable	5	11	0.03	0.53	3,495	9,483	6,489	216	259.00

\*Ceylan, 2008, Characterization of Unbound Materials for MEPDG: MEPDG Work Plan Task 5, Iowa DOT

\*For stabilized soils, the following equations are used to characterize the material

$$M_r = 30000 \left( \frac{a_i}{0.14} \right)^{20}$$

$M_r$ , psi

\*This equation is solved for  $M_r$

$M_r$  fly ash = 17,500 psi

[http://www.intrans.iastate.edu/reports/White%20et%20al.%202005\\_Stab\\_Vol21.pdf](http://www.intrans.iastate.edu/reports/White%20et%20al.%202005_Stab_Vol21.pdf)

Effective Modulus of Subgrade Reaction, psi/in

Method 1:  $k = M_r/30$

Method 2: Correlation with DCP





# I-PAVE

LOW VOLUME ROAD DESIGN GUIDE

INPUT

FLEXIBLE

RIGID

FLEX LCCA

RIGID LCCA

SOIL DATA

PRINT

CONTACT

Project Name

Harrington Dr.

Location

Ankeny

County

Polk

Design Period (Y) Years

50

STRUCTURE

Flexible

Rigid

Stone Base Thickness, in

6

6

Subbase Stabilization Depth, in

12

12

Subbase Soil Type

Unsuitable (Poor)

Lane Configuration

2

Average Daily Traffic (ADT)

5000

Percent Trucks (T)

4

Annual Growth Rate (%)

2

ESALs

1,592,413

Terminal Serviceability, pt

2.25

Reliability, R (%)

88

Flexible Thickness = 5.5"

Initial Cost = \$248,129.65

EUAC Cost = \$9,900.19

Run Calculations

Rigid Thickness = 7.5"

Initial Cost = \$352,184.30

EUAC Cost = \$10,542.82

FLEXIBLE

STONE BASE 6"

SOIL 12"

RIGID

STONE BASE 6"

SOIL 12"



Press F1 to access full help file. Press Shift+F1 to access context-sensitive pop-up help.

Functional Classification:

Two-Way AADT:  (500 to 5000)

%Trucks:  (1 to 20)

%Growth:  (0 to 3)

Design Trucks:  (Total Trucks in 30 Years)

Design ESALs:  (Total ESALs in 30 Years)

AASHTO Soil Classification:

Soil Modulus:  (10,000 to 30,000 psi)

Aggregate Base Thickness:  (0 to 10 in.)

HMA Modulus:  (400,000 to 1,000,000 psi)

Calculated HMA  in.

Design HMA  in.

Calculated thickness rounded up to nearest 0.25".



# Pavement Thickness Design

- American Concrete Paving Association
  - StreetPave software



Project Information

Next

Project Name

Project Description

Route

Location

Owner / Agency

Design Engineer

Software Use

▾

Help

Determine a comparable new asphalt pavement thickness?

Option On

Conduct a life cycle cost analysis (LCCA)?

Option Off

Traffic Category / Load Spectrum

**Typical Traffic Spectrums**    **ACI 330 Traffic Spectrums**    [Help](#)

- Residential                       Category A
- Collector**                               Category B
- Minor Arterial                       Category C
- Major Arterial                       Category D

[Custom Traffic Spectrum](#)

Truck Traffic over the Pavement Design Life

Trucks per Day (two-way, at time of construction)  [Calculate](#)

Traffic Growth Rate  % per year [Help](#)

Design Life  years [Help](#)

Directional Distribution  % [Help](#)

Design Lane Distribution  % [Help](#)

Average Trucks per Day in Design Lane over the Design Life                      **169**

Total Trucks in Design Lane over the Design Life    **8,458**

Traffic Category: Collector	
Axle load, kips	Axles / 1000 trucks
<b>Single Axles</b>	
26	0.07
24	1.6
22	2.6
20	6.63
18	16.61
16	23.88
14	47.76
12	116.76
10	142.7
8	233.6
<b>Tandem Axles</b>	
44	1.16
40	7.76
36	38.79
32	54.76
28	44.43
24	30.74
20	45
16	59.25
12	91.15
8	47.01
<b>Tridem Axles (User Defined Only)</b>	
62	0
56	0
50	0
44	0
38	0
32	0
26	0
20	0
14	0
8	0

[Next](#)

Next

General Design Inputs

Terminal Serviceability

Help

Reliability  %

Help

Resilient Modulus of the Subgrade

Convert CBR or R-value to MRS

Input a known MRS

Help

Calculate

4,118 psi

psi

Resilient Modulus of the Subgrade: 4,118 psi

Corresponding Subgrade Static k-value: 100 psi/in.

To determine the k-value for a subbase layer system, use the calculator tool below. First input the subbase(s)

### Step 1 - From the Top Down, Input Subbase(s) Modulus of Elasticity and

Number of subbase layers between subgrade  
and concrete pavement:

1 Layer

Top Layer Unstabilized Subbase (e.g., sand/gravel, crushed stone)

Layer Modulus of Elasticity 30,000 psi

Allowable Range: 15,000 - 45,000

Layer Thickness 6 in.

Layer 2 Choose Layer

Layer Modulus of Elasticity 0 psi

Allowable Range: Choose Layer Type

Layer Thickness 0 in.

Layer 3 Choose Layer

Layer Modulus of Elasticity 0 psi

Allowable Range: Choose Layer Type

Layer Thickness 0 in.

Step 2 - Calculate K

Calculated Composite Static k-Value 244 psi/in.

Close Window and Save k-Value

Help

Help

Percent of Slabs Cracked at End of Design Life

Slabs Cracked  %

Composite Modulus of Subgrade Reaction (Static k-Value)

Use calculated composite static k-value  Enter a known static k-value

psi/in.

psi/in.

Concrete Material Properties

28-Day Flexural Strength (MR)  psi

Modulus of Elasticity (E)  psi

Macrofibers in Concrete?  ▾

Edge Support

Edge support (e.g., tied concrete shoulder, curb and gutter, or widened lane) provided?  yes  no

Next

### Resilient Modulus of the Subgrade

Use Value from Global Input

4,118 psi

Use Different Resilient Modulus of Subgrade than Concrete Pavement Design

4,118 psi

Help

### Comparable Asphalt Thickness Design Details

Mean Annual Air Temperature (MAAT)

45°F

Help

Subgrade Modulus Coefficient of Variation

38 %

Help

Design Resilient Modulus of the Subgrade

**2,279** psi

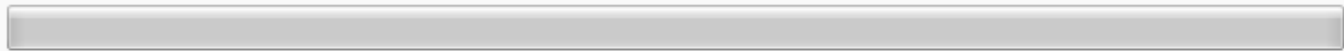
Help

Asphalt Design Type per the Asphalt Institute's MS-1, "Thickness Design - Highways and Streets"

Asphalt on a 6 in. Unstabilized (Granular) Base

Full-depth asphalt design is not possible because the design resilient modulus of the subgrade is too low; see the Design Resilient Modulus of the Subgrade help screen for more details.

Run Design



**CONCRETE PAVEMENT DESIGN**

Rigid ESALs = 988,437  
 Composite Modulus of Subgrade Reaction (Static k-Value) = 244 psi/in.  
 Top Layer = Unstabilized Subbase 6 in.

Save Project As

View/Print Design Summary

**Sensitivity Analysis of Concrete Pavement Design**

k-value       Reliability  
 Concrete Strength       % Slabs Cracked  
 Design Life

Generate

	Min. Required Thickness in.	Design Thickness in.	Max Joint Spacing ft	Failure Controlled By
Doweled				Doweled concrete pavement is not recommended
Undoweled	6.14	6.50	13	Cracking

Load Transfer Rec.

Jointing Rec.

Cracking/Faulting Table

Rounding Considerations

**ASPHALT PAVEMENT DESIGN**

Resilient Modulus of the Subgrade:      Subbase Selected = 6 inch  
 Calculated/Inputted = 4,118 psi      Flexible ESALs = 875,726  
 Used in Design = 2,279 psi      Required Asphalt Thickness = 9 in.

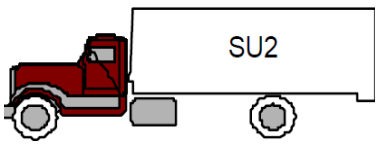
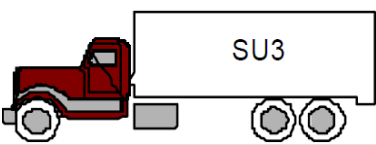
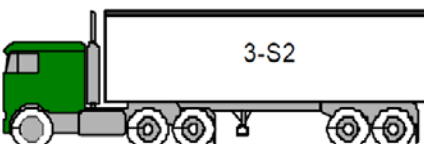
Help



# Pavement Thickness Design

- SUDAS Chapter 5, Section 5F-1
  - Uses 1993 AASHTO Design Guide as the base document
  - Traffic is based on 2010 Iowa DOT traffic inventories
  - Minimum pavement thickness
    - HMA = 6"
    - PCC = 6"

# Pavement Thickness Design

Vehicle Type	Percent of Total Trucks	Loading	Percent of Truck Type	Vehicle Weight (lbs)	Axle Type <i>S - Single</i> <i>TA - Tandem</i>	Axle Load (lbs)	ESAL Factor (per axle)		LEF (by Vehicle)	
							Rigid	Flexible	Rigid	Flexible
 Single Unit (2 axles) (Class 5/6 Truck)	30%	Empty	30%	14,500	Front - S	7,000	0.019	0.024		
					Rear - S	7,500	0.025	0.032		
		Partial Load (50% Capacity)	50%	20,500	Front - S	8,000	0.033	0.041		
					Rear - S	12,500	0.212	0.242		
Fully Loaded	20%	26,000	Front - S	9,000	0.053	0.066				
			Rear - S	17,000	0.785	0.799	0.3033	0.3313		
 Dump Trucks - 3 axles (Class 7/8 truck) (doesn't address cheater axles)	10%	Empty	50%	22,000	Front - S	10,000	0.083	0.101		
					Rear - TA	12,000	0.026	0.018		
		Fully Loaded	50%	54,000	Front - S	20,000	1.558	1.52		
					Rear - TA	34,000	1.9	1.099		
 Semis (5 axles)	60%	Empty	20%	26,000	Front - S	12,000	0.178	0.206		
					Rear - TA	7,000	0.003	0.002		
					Trailer - TA	7,000	0.003	0.002		
		Partial Load (50% Capacity)	60%	53,000	Front - S	13,000	0.251	0.282		
					Rear - TA	20,000	0.208	0.138		
					Trailer - TA	20,000	0.208	0.138		
Fully Loaded	20%	80,000	Front - S	20,000	1.558	1.52				
			Rear - TA	34,000	1.9	1.099	1.5086	1.1204		
Trailer - TA	34,000	1.9	1.099							
<b>Composite Load Equivalency Factor (LEF) for "Trucks"</b>									<b>1.1745</b>	<b>0.90853</b>

# Pavement Thickness Design

- Base Year ESALs Rigid Pavement

% Trucks	Two Way, Base Year AADT							
	1,000	2,000	3,000	4,000	5,000	10,000	15,000	20,000
1	1,000	3,000	4,000	9,000	11,000	21,000	32,000	43,000
2	3,000	6,000	8,000	17,000	21,000	43,000	64,000	86,000
3	4,000	8,000	13,000	26,000	32,000	64,000	96,000	129,000
4	9,000	17,000	26,000	34,000	43,000	86,000	129,000	171,000
5	11,000	21,000	32,000	43,000	54,000	107,000	161,000	214,000
6	13,000	26,000	39,000	51,000	64,000	129,000	193,000	257,000
7	15,000	30,000	45,000	60,000	75,000	150,000	225,000	300,000
8	17,000	34,000	51,000	69,000	86,000	171,000	257,000	343,000
9	19,000	39,000	58,000	77,000	96,000	193,000	289,000	386,000
10	21,000	43,000	64,000	86,000	107,000	214,000	322,000	429,000
12	26,000	51,000	77,000	103,000	129,000	257,000	386,000	514,000
14	30,000	60,000	90,000	120,000	150,000	300,000	450,000	600,000
16	34,000	69,000	103,000	137,000	171,000	343,000	514,000	686,000
18	39,000	77,000	116,000	154,000	193,000	386,000	579,000	772,000
20	43,000	86,000	129,000	171,000	214,000	429,000	643,000	857,000
22	47,000	94,000	141,000	189,000	236,000	472,000	707,000	943,000
24	51,000	103,000	154,000	206,000	257,000	514,000	772,000	1,029,000
26	56,000	111,000	167,000	223,000	279,000	557,000	836,000	1,115,000
28	60,000	120,000	180,000	240,000	300,000	600,000	900,000	1,200,000
30	64,000	129,000	193,000	257,000	322,000	643,000	965,000	1,286,000

Assume two lane roadway with 50/50 directional split of base year AADT

Values within "box" assume a low volume mix of trucks

# Pavement Thickness Design

- Base Year ESALs Flexible Pavement

% Trucks	Two Way, Base Year AADT							
	1,000	2,000	3,000	4,000	5,000	10,000	15,000	20,000
1	1,000	2,000	4,000	7,000	8,000	17,000	25,000	33,000
2	2,000	5,000	7,000	13,000	17,000	33,000	50,000	66,000
3	4,000	7,000	11,000	20,000	25,000	50,000	75,000	99,000
4	7,000	13,000	20,000	27,000	33,000	66,000	99,000	133,000
5	8,000	17,000	25,000	33,000	41,000	83,000	124,000	166,000
6	10,000	20,000	30,000	40,000	50,000	99,000	149,000	199,000
7	12,000	23,000	35,000	46,000	58,000	116,000	174,000	232,000
8	13,000	27,000	40,000	53,000	66,000	133,000	199,000	265,000
9	15,000	30,000	45,000	60,000	75,000	149,000	224,000	298,000
10	17,000	33,000	50,000	66,000	83,000	166,000	249,000	332,000
12	20,000	40,000	60,000	80,000	99,000	199,000	298,000	398,000
14	23,000	46,000	70,000	93,000	116,000	232,000	348,000	464,000
16	27,000	53,000	80,000	106,000	133,000	265,000	398,000	531,000
18	30,000	60,000	90,000	119,000	149,000	298,000	448,000	597,000
20	33,000	66,000	99,000	133,000	166,000	332,000	497,000	663,000
22	36,000	73,000	109,000	146,000	182,000	365,000	547,000	730,000
24	40,000	80,000	119,000	159,000	199,000	398,000	597,000	796,000
26	43,000	86,000	129,000	172,000	216,000	431,000	647,000	862,000
28	46,000	93,000	139,000	186,000	232,000	464,000	696,000	929,000
30	50,000	99,000	149,000	199,000	249,000	497,000	746,000	995,000

Assume two lane roadway with 50/50 directional split of base year AADT

Values within "box" assume a low volume mix of trucks

Subbase:	Natural			4" Granular			6" Granular			8" Granular			10" Granular			12" Granular			
CBR Value:	3	5	10	3	5	10	3	5	10	3	5	10	3	5	10	3	5	10	
<b>Rigid Pavement Parameters</b>																			
Initial Serviceability Index, $P_o$	4.5																		
Terminal Serviceability Index, $P_t$	Local Roads = 2.00 Collector Roads = 2.25 Arterials = 2.50																		
Reliability, $R$	Local Roads = 80% Collector Roads = 88% Arterial Roads = 95%																		
Overall Standard Deviation, $S_o$	0.35																		
Loss of Support, $LS$	1			0															
Soil Resilient Modulus, $M_R$ Per NCHRP Project 128 $M_R = 1941.488 \times CBR^{0.6844709}$	4120	5840	9400	4120	5840	9400	4120	5840	9400	4120	5840	9400	4120	5840	9400	4120	5840	9400	
Subbase Resilient Modulus, $E_{SB}$ * Assumed	Not Applicable			30,000															
Modulus of Subgrade Reaction, $k$ , and Composite Modulus of Subgrade Reaction, $k_c$ Use AASHTO Chapter 3, Table 3.2 and Figures 3.3 - 3.6 to determine	252	327	469	263	332	455	284	354	477	308	379	504	332	406	535	356	433	566	
Adjusted $k$ or $k_c$ for Loss of Support Use AASHTO Part 2, Figure 3.6	85	105	160	263	332	455	284	354	477	308	379	504	332	406	535	356	433	566	
Coefficient of Drainage, $C_d$	1.00			1.10															
Modulus of Rupture, $S'_c$ $S'_c = 2.3 \times f'_c^{0.667}$ * Assumed 4,000 psi concrete	580																		
Modulus of Elasticity, $E_c$ $E_c = 6,750 \times S'_c$ * Assumed 4,000 psi concrete	3,915,000																		
Load Transfer, $J$	$J = 3.1$ (Pavement Thickness < 8") $J = 2.7$ (Pavement Thickness $\geq$ 8")																		
<b>Flexible Pavement Parameters</b>																			
Initial Serviceability Index, $P_o$	4.2																		
Terminal Serviceability Index, $P_t$	Local Roads = 2.00 Collector Roads = 2.25 Arterials = 2.50																		
Reliability, $R$	Local Roads = 80% Collector Roads = 88% Arterial Roads = 95%																		
Overall Standard Deviation, $S_o$	0.45																		
Layer Coefficients	Surface/Intermediate Course = 0.44 Base Course = 0.40 Granular Subbase = 0.14																		
Soil Resilient Modulus, $M_R$ Per NCHRP Project 128 $M_R = 1941.488 \times CBR^{0.6844709}$	4120	5840	9400	4120	5840	9400	4120	5840	9400	4120	5840	9400	4120	5840	9400	4120	5840	9400	
Effective Soil Resilient Modulus, $MR$ Use AASHTO Chapter 2, Figure 2.3 to determine	2460	3480	5580	2460	3480	5580	2460	3480	5580	2460	3480	5580	2460	3480	5580	2460	3480	5580	
Coefficient of Drainage, $M_i$	1.00			1.15															

# Pavement Thickness Design

- Rigid Pavement Thickness - Collectors

Subbase ESAL/CBR	Natural Subgrade			4" Granular			6" Granular		
	3	5	10	3	5	10	3	5	10
750,000	7	7	7	6	6	6*	6	6	6*
1,000,000	7.5	7.5	7.5	6.5	6	6	6.5	6	6
1,500,000	8	8	8	7	6.5	6.5	7	6.5	6.5
2,000,000	8	8	8	7.5	7	7	7	7	7
3,000,000	8.5	8	8	8	7.5	7.5	8	7.5	7.5
4,000,000	8.5	8.5	8.5	8	8	8	8	8	8
5,000,000	9	9	8.5	8	8	8	8	8	8
7,500,000	9.5	9.5	9.5	8.5	8.5	8	8.5	8	8
10,000,000	10	10	9.5	9	8.5	8.5	9	8.5	8.5
12,500,000	10.5	10	10	9	9	9	9	9	9
15,000,000	10.5	10.5	10.5	9.5	9.5	9	9.5	9.5	9
17,500,000	11	10.5	10.5	9.5	9.5	9.5	9.5	9.5	9.5
20,000,000	11	11	11	10	10	9.5	10	9.5	9.5

\* The value shown represents a 6 inch minimum; the actual value is less.

# Pavement Thickness Design

- Flexible Pavement Thickness - Collectors

Subbase ESAL/CBR	Natural Subgrade			4" Granular			6" Granular			8" Granular			10" Granular			12" Granular		
	3	5	10	3	5	10	3	5	10	3	5	10	3	5	10	3	5	10
750,000	11.5	10.5	9	10	9	7.5	9	8	6.5	8.5	7.5	6*	8	6.5	6*	7	6*	6*
1,000,000	12	10.5	9	10.5	9	7.5	9.5	8.5	7	9	7.5	6	8	7	6*	7.5	6	6*
1,500,000	12.5	11.5	9.5	11	10	8	10.5	9	7.5	9.5	8.5	6.5	9	7.5	6	8	7	6*
2,000,000	13	12	10	11.5	10.5	8.5	11	9.5	8	10	8.5	7	9.5	8	6.5	8.5	7.5	6*
3,000,000	14	12.5	10.5	12.5	11	9	11.5	10	8.5	11	9.5	8	10	8.5	7	9	8	6
4,000,000	---	13	11	13	11.5	9.5	12	10.5	9	11.5	10	8	10.5	9	7.5	10	8.5	6.5
5,000,000	---	13.5	11.5	13.5	12	10	12.5	11	9	11.5	10.5	8.5	11	9.5	8	10	8.5	7
7,500,000	---	14	12	14	12.5	10.5	13.5	12	10	12.5	11	9	11.5	10	8.5	11	9.5	7.5
10,000,000	---	---	12.5	---	13	11	14	12.5	10.5	13	11.5	9.5	12.5	10.5	9	11.5	10	8
12,500,000	---	---	13	---	13.5	11.5	---	12.5	10.5	13.5	12	10	13	11	9	12	10.5	8.5
15,000,000	---	---	13.5	---	14	12	---	13	11	14	12.5	10.5	13	11.5	9.5	12.5	10.5	8.5
17,500,000	---	---	13.5	---	14	12	---	13.5	11.5	---	12.5	10.5	13.5	12	10	12.5	11	9
20,000,000	---	---	14	---	---	12.5	---	13.5	11.5	---	13	11	14	12	10	13	11.5	9

\* The value shown represents a 6 inch minimum; the actual value is less.

# Pavement Thickness Design

## Two Lane Collector Roadway, PCC

AADT = 5,000

Trucks = 4%

Annual Growth Rate = 2%

Design Period = 50 years

Base Year Design ESALs (from Table 5F-1.07) = 43,000

Growth Factor (from Table 5F-1.11) = 84.6

43,000 ESALs X 84.6 = 3,637,800 ESALs

Subbase ESAL/CBR	Natural Subgrade			4" Granular			6" Granular		
	3	5	10	3	5	10	3	5	10
750,000	7	7	7	6	6	6*	6	6	6*
1,000,000	7.5	7.5	7.5	6.5	6	6	6.5	6	6
1,500,000	8	8	8	7	6.5	6.5	7	6.5	6.5
2,000,000	8	8	8	7.5	7	7	7	7	7
3,000,000	8.5	8	8	8	7.5	7.5	8	7.5	7.5
4,000,000	8.5	8.5	8.5	8	8	8	8	8	8
5,000,000	9	9	8.5	8	8	8	8	8	8

\* The value shown represents a 6 inch minimum; the actual value is less.



# Pavement Thickness Design

## Two Lane Collector Roadway, HMA

AADT = 5,000

Trucks = 4%

Annual Growth Rate = 2%

Design Period = 50 years

Base Year Design ESALs (from Table 5F-1.08) = 33,000

Growth Factor (from Table 5F-1.11) = 84.6

33,000 ESALs X 84.6 = 2,791,800 ESALs

Subbase ESAL/CBR	Natural Subgrade			4" Granular			6" Granular			8" Granular			10" Granular			12" Granular		
	3	5	10	3	5	10	3	5	10	3	5	10	3	5	10	3	5	10
750,000	11.5	10.5	9	10	9	7.5	9	8	6.5	8.5	7.5	6*	8	6.5	6*	7	6*	6*
1,000,000	12	10.5	9	10.5	9	7.5	9.5	8.5	7	9	7.5	6	8	7	6*	7.5	6	6*
1,500,000	12.5	11.5	9.5	11	10	8	10.5	9	7.5	9.5	8.5	6.5	9	7.5	6	8	7	6*
2,000,000	13	12	10	11.5	10.5	8.5	11	9.5	8	10	8.5	7	9.5	8	6.5	8.5	7.5	6*
3,000,000	14	12.5	10.5	12.5	11	9	11.5	10	8.5	11	9.5	8	10	8.5	7	9	8	6
4,000,000	---	13	11	13	11.5	9.5	12	10.5	9	11.5	10	8	10.5	9	7.5	10	8.5	6.5

\* The value shown represents the 6 inch minimum; the actual value is less.

# Pavement Thickness Design

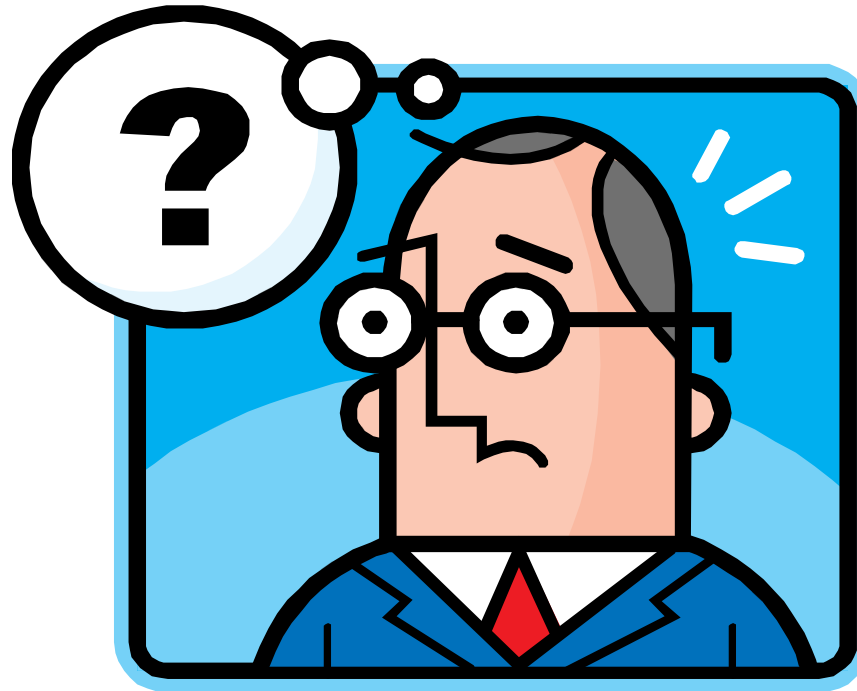
- Summary

<b>Design Model</b>	<b>HMA ESALS</b>	<b>HMA Thickness</b>	<b>PCC ESALS</b>	<b>PCC Thickness</b>
APAI I-Pave	1,591,413	5 ½"	1,591,413	7 ½"
PerRoadXpress	441,258	9"	-----	-----
ACPA StreetPave	875,726	9"	801,589	6 ½"
SUDAS	2,791,800	10"	3,637,800	8"

# Pavement Thickness Design

- Inconsistencies in Design Models
  - I-Pave
    - ESAL calculations much different
    - Effective soil  $M_R = 10,000$  psi; AASHTO's value = 3480 psi
  - PerRoadXpress
    - Only 30 year design life
    - $M_R = 10,000$  psi; AASHTO value = 3480
  - StreetPave
    - ESAL calculations much different
    - For HMA - maximum  $M_R = 2279$  psi; AASHTO's value = 3480 psi

# Questions?



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