



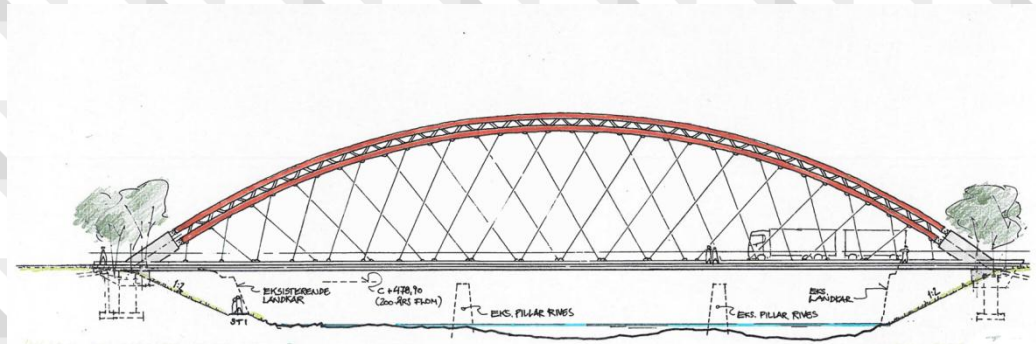
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Steien Network Arch Bridge

Johannes Veie
Norwegian Public Road Administration

Rune B Abrahamsen
Sweco

Egil Rønnekleiv
Plan architects



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Existing situation

- Location: Alvdal municipality. Hedmark County, 300 km north of the capital Oslo.
- Existing bridges build in 1953 and 1983
- The main bridge is in a bad condition
- High maintenance costs.
- A preliminary study in 2010 concluded that both should be replaced



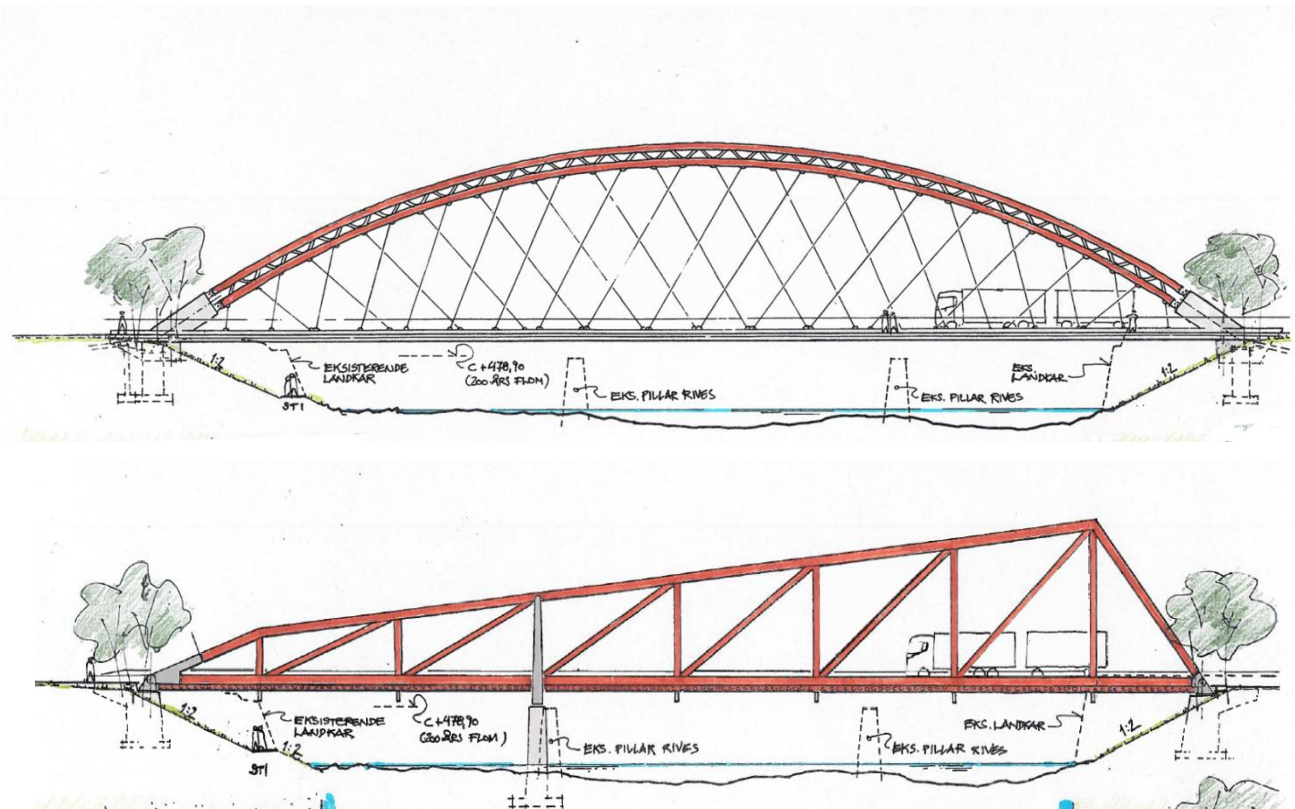
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Network arch bridge and a glulam truss bridge

To alternatives was considered in the end of the preliminary study.

The study was performed by: NPRA, Sweco technical consultants and PLAN architects.

The network arch was chosen as the preferred alternative.





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Architectural comments

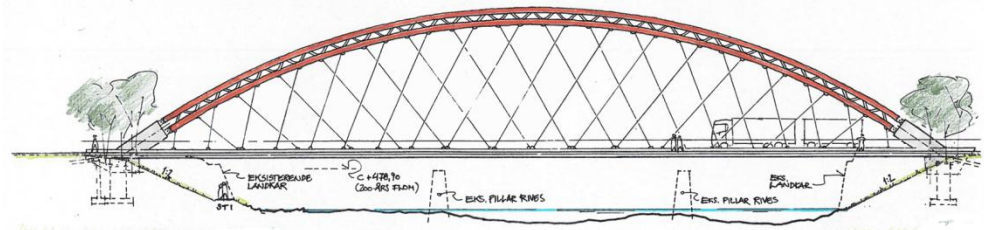
- Steien network arch bridge in one span over the river Glomma will provide an innovative and elegant design with strong identity and architectural quality.
- Double timber arches connected with diagonals in tension made of plates in stainless steel, along with a slender network, gives a very light and airy superstructure with a good side visibility and transparency. The bridge will appear as a new landmark in Alvdal.
- Walkways on the outside of the network planes provide a good contact with the river scenery.



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Some general facts

- Span: 88.0 meters
- The bridge carries two traffic lanes, 8 meters wide, and two 3 meters wide pedestrian walkways. Total 19 meters wide.
- Cross section of arches: $w \times d = 850 \times 600$ mm
- Height from centre slab to centre lower arch: 14 meters
- Distance between the centrelines of two arches: 1.25 meter
- Spacing of hangers and diagonals along the arches: 2.5 meters
- The slab is made of in situ casted light weight aggregate concrete with prestressing.
- Hangers: $\varnothing 48$ mm tension bars.

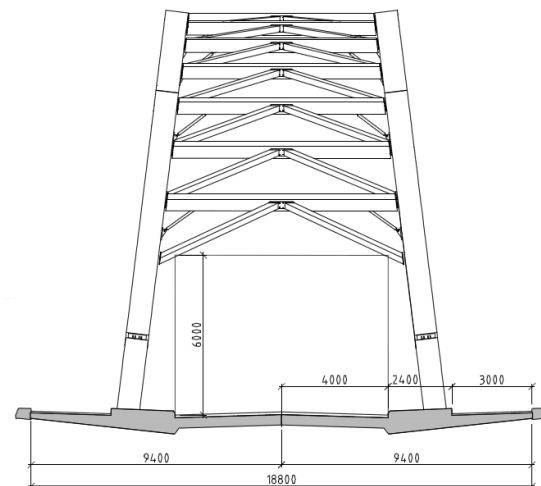




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FINAL DESIGN





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Definition of a network arch bridge

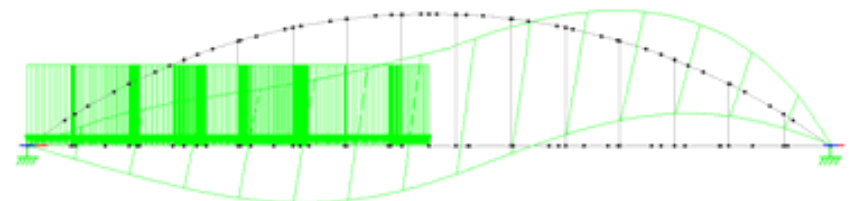
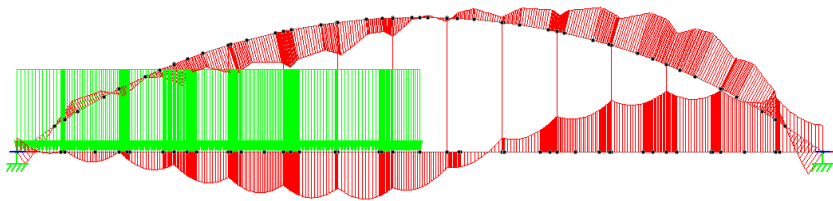
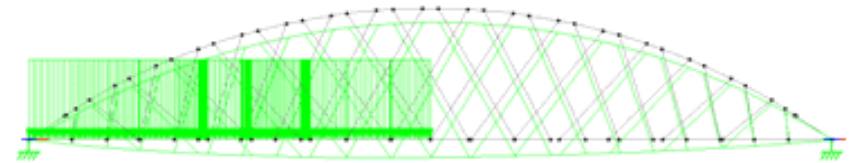
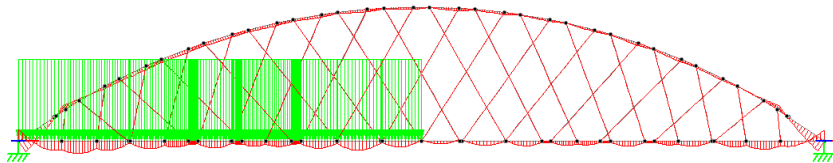
Characteristics of an optimal network arch bridge (Tveit 2011):

- Deck made out of concrete
- Ties imbedded in the deck in the form of prestressing cables.
- Arches made as part of a circle
- The upper node of the hangers are evenly spaced along the arch and the hangers not being merged in the nodal points.
- Most hangers crossing at least two other hangers



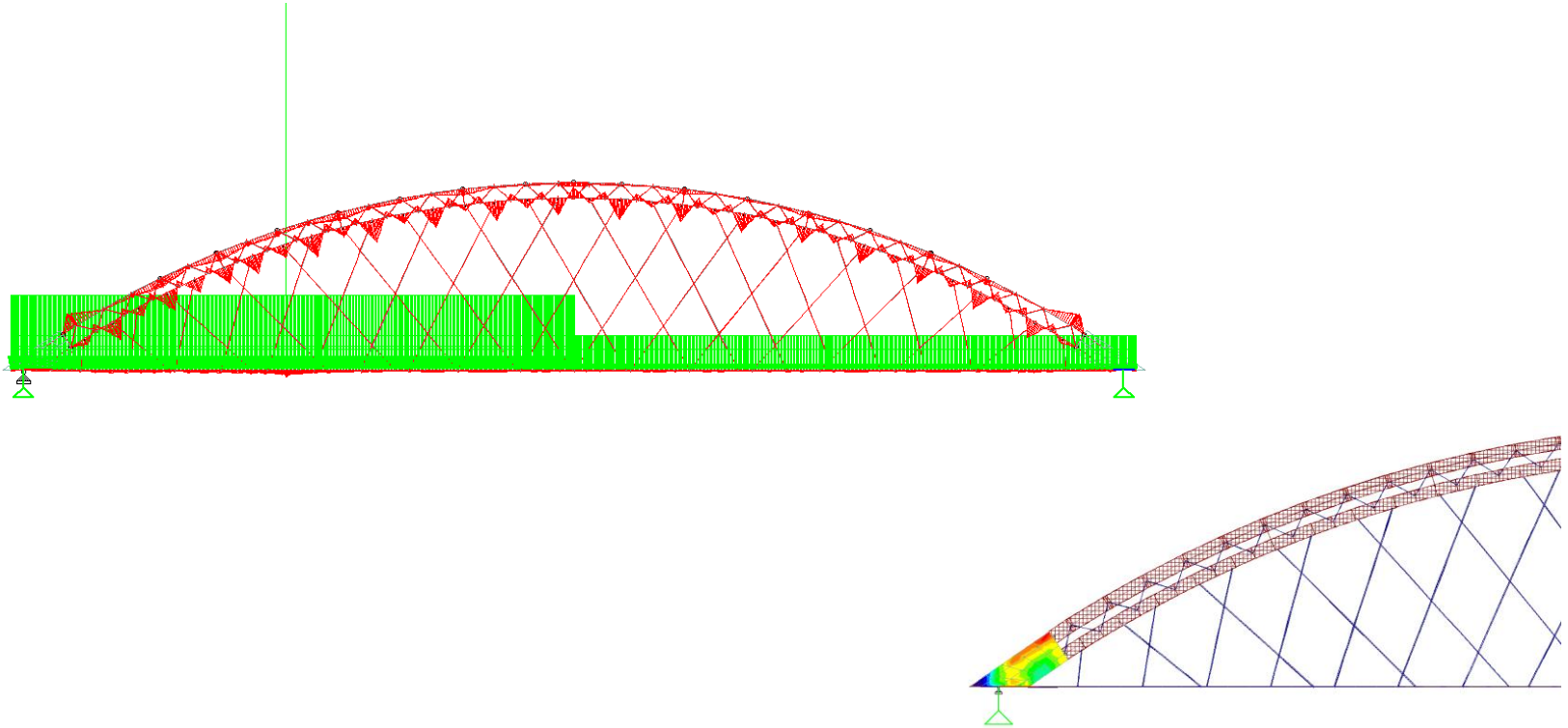
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Structural performance compared to a typical tied arch



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Distribution of moments and compressive forces due to asymmetric loading. Steien arch bridge





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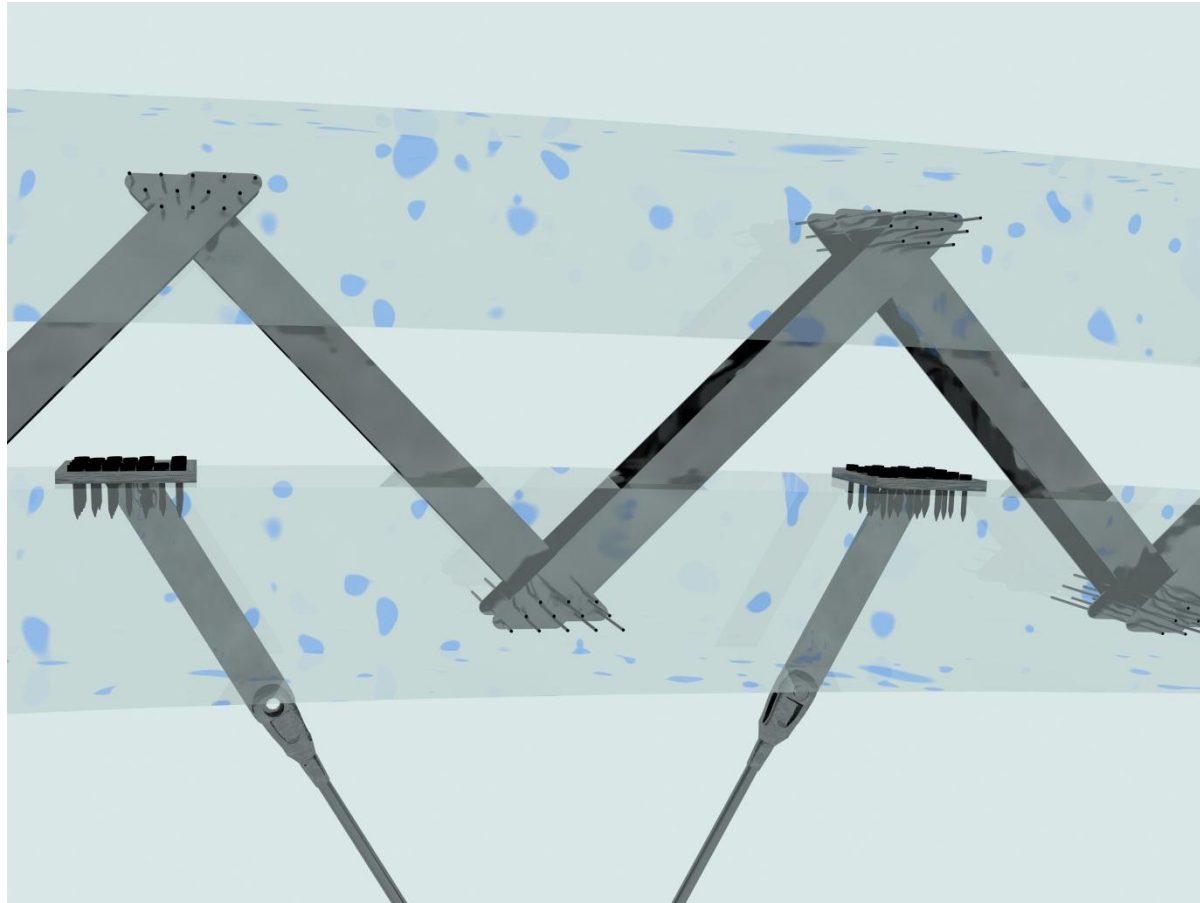
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Experience from other network arch bridges



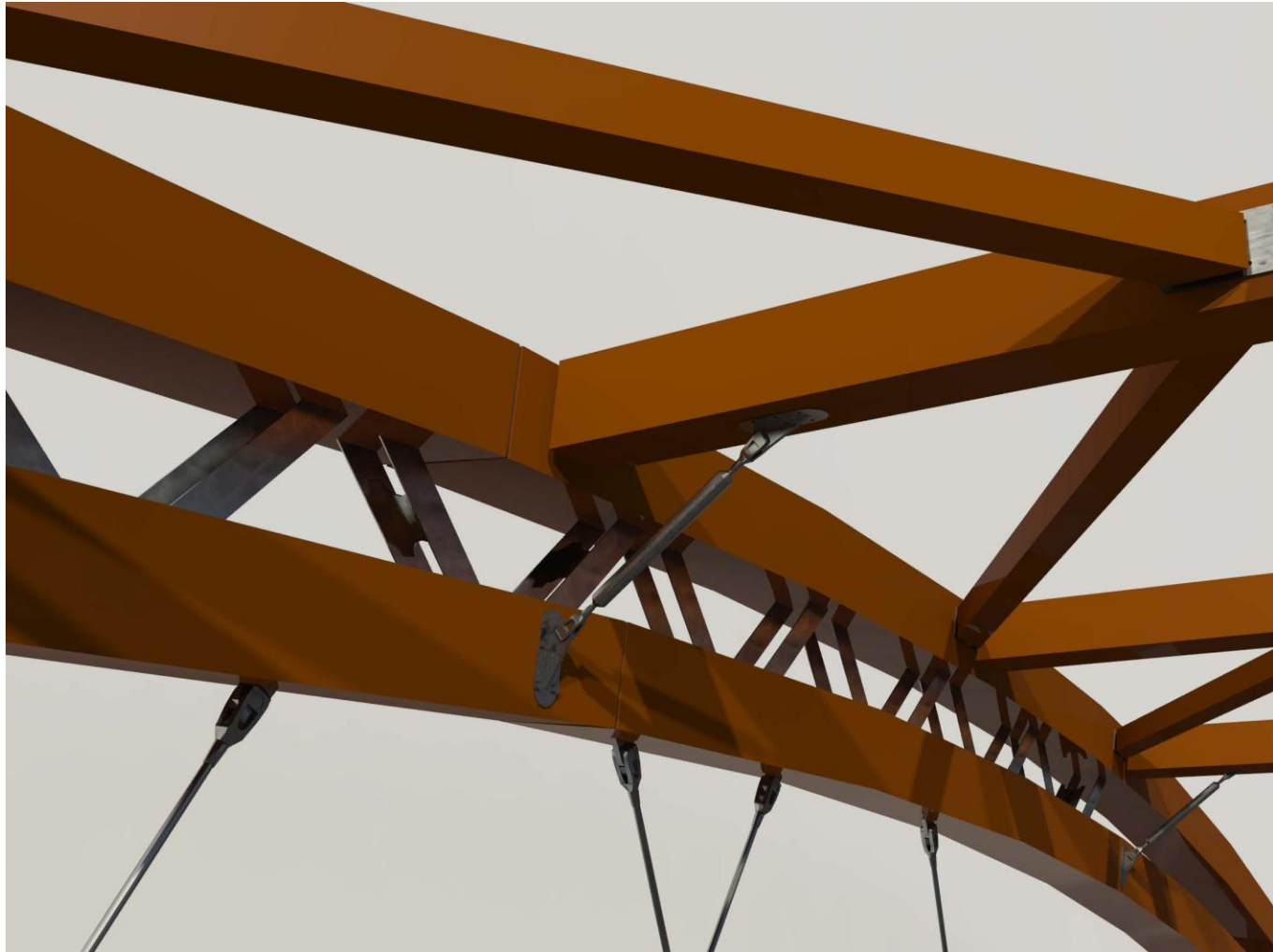


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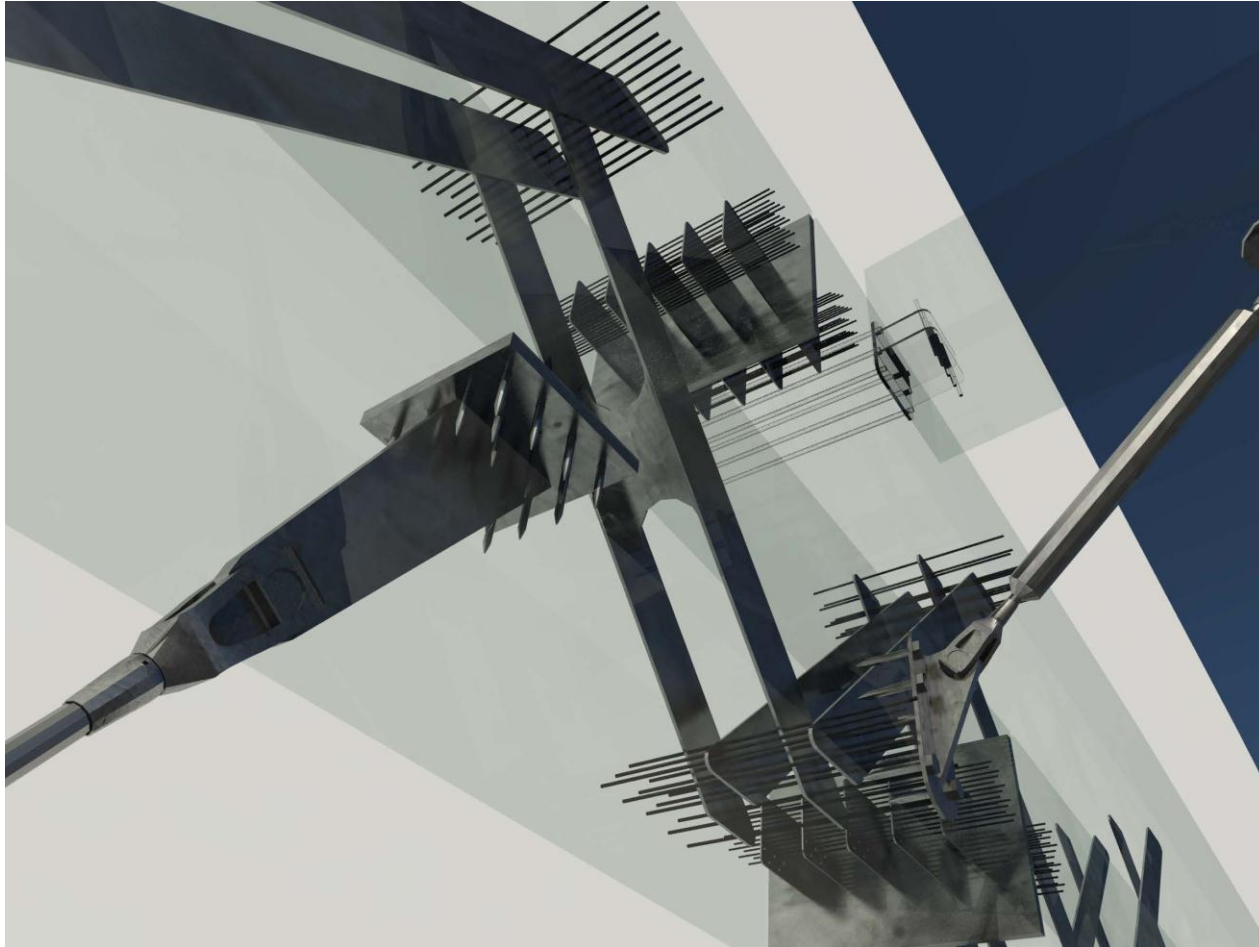


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DETAILS





ICTB 2013 DETAILS





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Construction of the bridge

- When the interim route is established the road bridge and footbridge are demolished.
- Abutments are established prior to or simultaneously with the framework for bridge deck being established.
- Framework established on filling and / or temporary piles, optionally also using existing pillars.
- The slab is casted independent of the arches
- Each arch can be pre-assembled on factory and mounted on site in 4 segments.
- To compensate for the deflection the slab is casted with a camber. After stressing the slab will be jacked with an additional camber in order to ease the mounting of the hangers and reduce the need of hanger adjustments





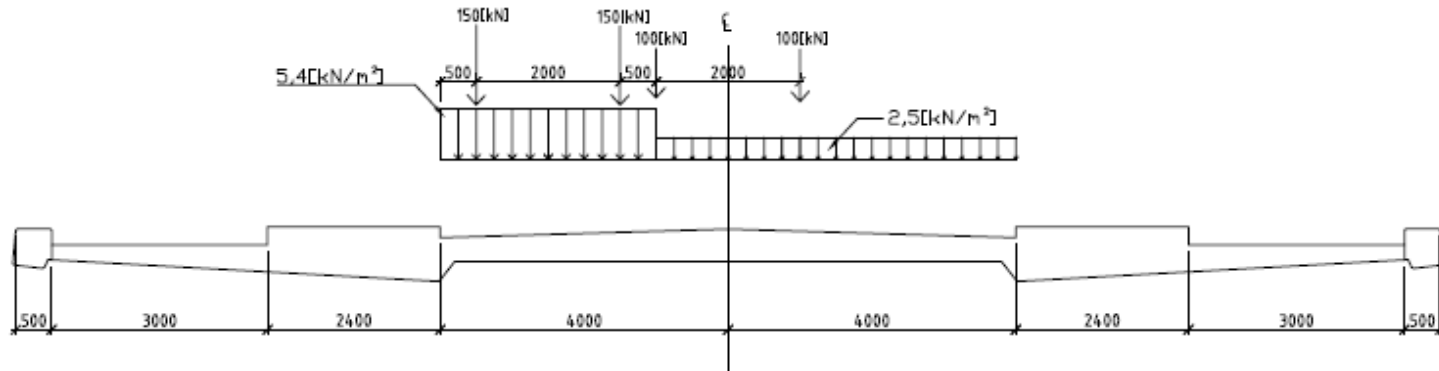
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Utilization of the arches

- Total weight of the superstructure: 2264 tons
- Total traffic loading: 495 tons
- Ratio between self-weight of the superstructure + traffic loading and self-weight alone:
$$2760 \text{ tonns} / 2264 \text{ tonns} = 1.22$$
- Knowing that the long term modification factor for strength is 0.6, and the same factor for combined loading of self-weight and traffic is 0.9, giving a ratio of 1.5, it is possible to explain why self-weight is governing the design.

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Traffic loading



Position	Double axel load (BL)	Equal Distributed load
	Axel load $\alpha_{Qi} \cdot Q_{ik}$ [kN]	$\alpha_{qi} \cdot q_{ik}$ [kN/m ²]
Loading area nr 1	1,0 • 300 = 300	0,6 • 9 = 5,4
Loading area nr 2	1,0 • 200 = 200	1,0 • 2,5 = 2,5

Loadmodel 1 according to NS-EN 1991-2:2003

Equally distributed load on the pedestrian carriageways are

$q=5,0$ kN/m²

without simultaneous traffic loading

$q=2,5$ kN/m²

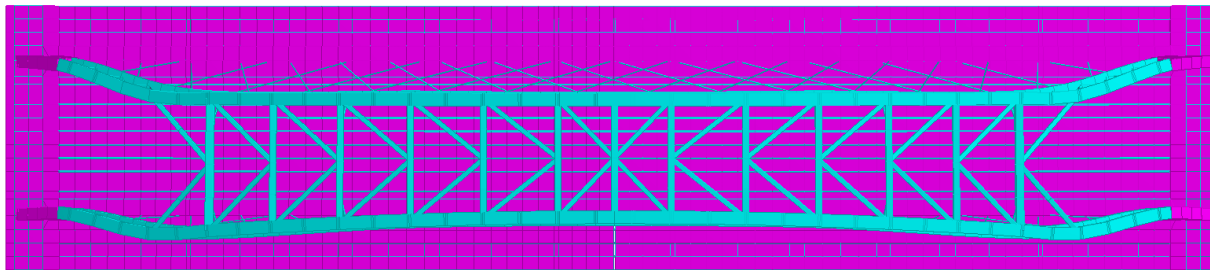
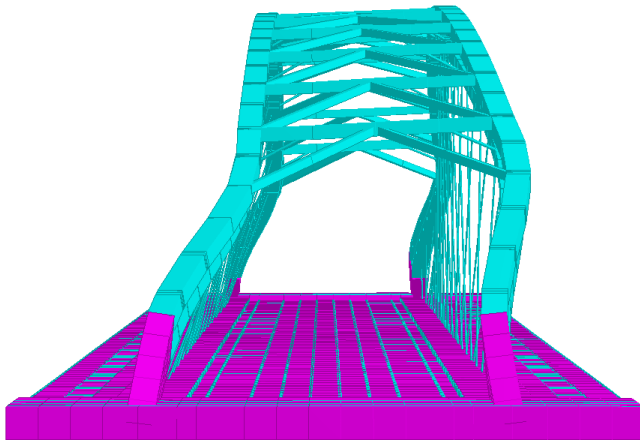
with simultaneous traffic loading



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1st buckling mode

Buckling factor = 8
Selfweight alone





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Thank you for your attention

