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P A V E M E N T T E C H N O L O G Y

Field Evaluation of Elliptical Fiber Reinforced Polymer Dowel Performance

Final Report
June 2005

IOWA STATE UNIVERSITY

Sponsored by
the Federal Highway Administration,
U.S. Department of Transportation
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16. Abstract Fiber reinforced polymer (FRP) composite materials are making an entry into the construction market in both buildings and pavements. The application to pavements so far has come in the form of joint reinforcement (dowels and tie bars). FRP resistance to salt corrosion in dowels has made it an alternative to standard epoxy-coated steel dowels for pavements. Iowa State University has completed a large amount of laboratory research to determine the diameter, spacing, and durability of FRP dowels. This report documents the performance of elliptical FRP dowels installed in a field situation. Ten joints were monitored in three consecutive test sections, for each of three dowel spacings (10, 12, and 15 inches) including one instrumented dowel in each test section. The modulus of dowel bar support was determined using falling weight deflectometer (FWD) testing and a loaded crawl truck. FWD testing was also used to determine load transfer efficiency across the joint. The long-term performance and durability of the concrete was also evaluated by monitoring faulting and joint opening measurements and performing visual distress surveys at each joint. This report also contains similar information for standard round, medium elliptical, and heavy elliptical steel dowels in a portion of the same highway. In addition, this report provides a summary of theoretical analysis used to evaluate joint differential deflection for the dowels.					
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FIELD EVALUATION OF ELLIPTICAL FIBER REINFORCED POLYMER DOWEL PERFORMANCE

**Final Report
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1. INTRODUCTION

1.1. Background

Transverse joints are used in concrete paving to mitigate cracking effects caused by moisture infiltration, temperature changes, and concrete shrinkage. The joints purposely create weak areas in the concrete and, therefore, require the use of load transferring devices to maintain continuity in the pavement. The most common load transfer device currently in use is the epoxy-coated steel dowel. The dowel is usually round with a diameter of 1.25 or 1.5 inches, depending upon the slab thickness. The dowels present two main problems to the lifespan of the joint: corrosion and oblonging within the joint.

Corrosion occurs in the steel bar because of a chloride ion exchange caused by the environment and various salts applied to the roadway during adverse winter weather conditions. The corrosion weakens the dowel by causing a reduction in the effective load bearing area in the steel dowel. The corroded steel will also cause chipping and spalling in the surrounding concrete. The epoxy coating is designed to prevent the chloride from interacting with the steel. However, there are usually flaws in the epoxy coating caused by careless handling, storage, placement, or manufacturing, which in turn causes nicks, pin-holes, and scrapes. Moisture attacks the coating flaws and causes pitted corrosion beneath the surface of the coating [1].

Corrosion also causes the steel dowels to expand and thus freeze or lock the joints, preventing the intended normal slip required of a dowel bar within the joint. The dowel bar must slip to accommodate the expansion and contraction that results from temperature, shrinkage, and moisture changes in the slabs. A locked joint will cause cracking to occur outside of the intended doweled joint, resulting in pavement failure.

Oblonging occurs in the concrete around the dowel due to excessive bearing stresses between the bar and the concrete surface under repeated reversed loadings. The high stresses weaken the concrete and eventually loosen the connection between the dowel and the pavement.

To date, all fiber-reinforced polymer (FRP) dowel bar-related research in the United States has centered on the chemical makeup of materials in the bars and their laboratory strength evaluations. Iowa State University (ISU) has done much of this research [1-11]. Currently, research is underway to evaluate field installations for round dowels. A recent ISU study indicated that elliptical-shaped dowels could offer pavement performance benefits by reducing bearing stresses above and below the dowel [12-15]. This assertion is currently being tested further at ISU under the direction of Dr. Max Porter and Dr. James Cable. A field evaluation of the performance of elliptical-shaped steel and FRP dowels is being performed on U.S. Highway 330 near Melbourne, Iowa, in Marshall County.

Other FRP dowel bar research is being and has been conducted in Illinois, Ohio, Minnesota, and Wisconsin. Research in Iowa and Ohio has suggested that corrosion deterioration comparisons between FRP and steel dowels require longer-term evaluation. Research from these states has shown that steel generally provides a higher load transfer efficiency than FRP for round dowels of the same size and at the same spacing. Combinations of size, shape, and spacing affect this load transfer efficiency. Therefore, studies are needed of the performance of larger FRP dowels with smaller spacing between bars to improve load transfer efficiency. Studies conducted at ISU and in Illinois have recommended the testing the ability of elliptical-shaped dowels (both FRP and steel) to improve load transfer efficiency [16].

The research given in this report provides the opportunity to compare elliptical-shaped FRP bars in a roadway section immediately adjacent to (but separate in construction from) a roadway segment with round and elliptical-shaped steel bars (Federal Highway Administration, Project DTFH6103C00119) [12]. The advantage of this comparison on the same highway is that the same traffic will most likely use both segments of roadway and the environmental conditions will be very similar over the research period. This comparison can result in one measure of the relative stiffness, durability, cost, and strength of each material installed.

1.2. Research Objectives

The objective of this research is to evaluate the load transfer capabilities of elliptical-shaped FRP dowels and basket assemblies across pavement joints. The intent of this work is to estimate the performance of the individual dowel configurations in terms of stiffness, durability, modulus of dowel support, and deflection predictions. The following comparisons will be made after analyzing field data from Highway 330:

- Performance of elliptical FRP dowels versus that of conventional 1.5-inch diameter circular epoxy-coated steel dowels
- Performance of FRP versus conventional steel dowels with respect to long-term resistance to corrosion
- Effect of an elliptical versus circular shape in reducing the bearing contact stress between the concrete and the dowel bar

1.3. Research Approach

The life cycle of the project, as described in the proposal, lasts from September 30, 2002 through September 30, 2005. The investigators performed biannual testing. These tests were conducted once each spring and once each late summer. The objective of testing in the spring was to take advantage of a weaker subbase due to ground thaw. The late summer tests were conducted in hopes of having a very dry foundation. All tests were taken during similar times of day in order to best control the variance in temperature during the day to ensure comparable results from year to year. The tests consisted of the following procedures to monitor the pavement's performance:

- Falling weight deflectometer (FWD)
- Strain gage analysis under two conditions
- Load application with a standard Department of Transportation dump truck (crawl truck)
- Load application with FWD
- Joint faulting measurement
- Joint widening measurement
- Visual distress survey

The final report provides a comprehensive summary of the project's research, including installation, evaluation, and subsequent conclusions and recommendations.

2. THEORY

2.1 Joint Load Transfer

If dowel bars achieved 100% efficiency in load transfer, 50% of the wheel load would be transferred to the subgrade while the other 50% would be transferred through the dowels to the adjacent slab [2]. However, repetitive loading of the joint results in the creation of a void directly above or beneath the dowel at the face of the joint. According to Yoder and Witczak [17], a 5% to 10% reduction in load transfer occurs upon formation of this void. Therefore, a design load transfer of 45% of the applied wheel load is recommended.

$$P_t = 0.45P_w \quad (2-1)$$

Where,

P_t = load transferred across the joint (lbs)

P_w = applied wheel load (lbs)

Not all dowels are active in transferring the applied wheel load across the joint. Friberg [18] was the first to examine the distribution of transferred load to the dowels within a transverse joint. He assumed that dowel bars close to the load were more effective in transferring load than those farther away. For joints containing 0.75-inch or 0.875-inch diameter dowel bars spaced from 12 to 20 inches apart, Friberg postulated that only the dowels contained within a distance of $1.8l_r$ from the load are active in transferring the load, where l_r is the radius of relative stiffness, defined by Westergaard [19] as follows:

$$l_r = \sqrt[4]{\frac{E_c h^3}{12(1-\mu)^2 K}} \quad (2-2)$$

Where,

E_c = modulus of elasticity of the pavement concrete (psi)

h = pavement thickness (in.)

μ = poisson's ratio for the pavement concrete

K = modulus of subgrade reaction (pci)

Friberg also proposed a linear distribution of the load transferred across the joint as shown in Figure 2.1. For transverse joints containing dowel bars having a larger diameter or closer spacing, the stiffness of the joint increases and a distance of $1.8l_r$ is no longer applicable.

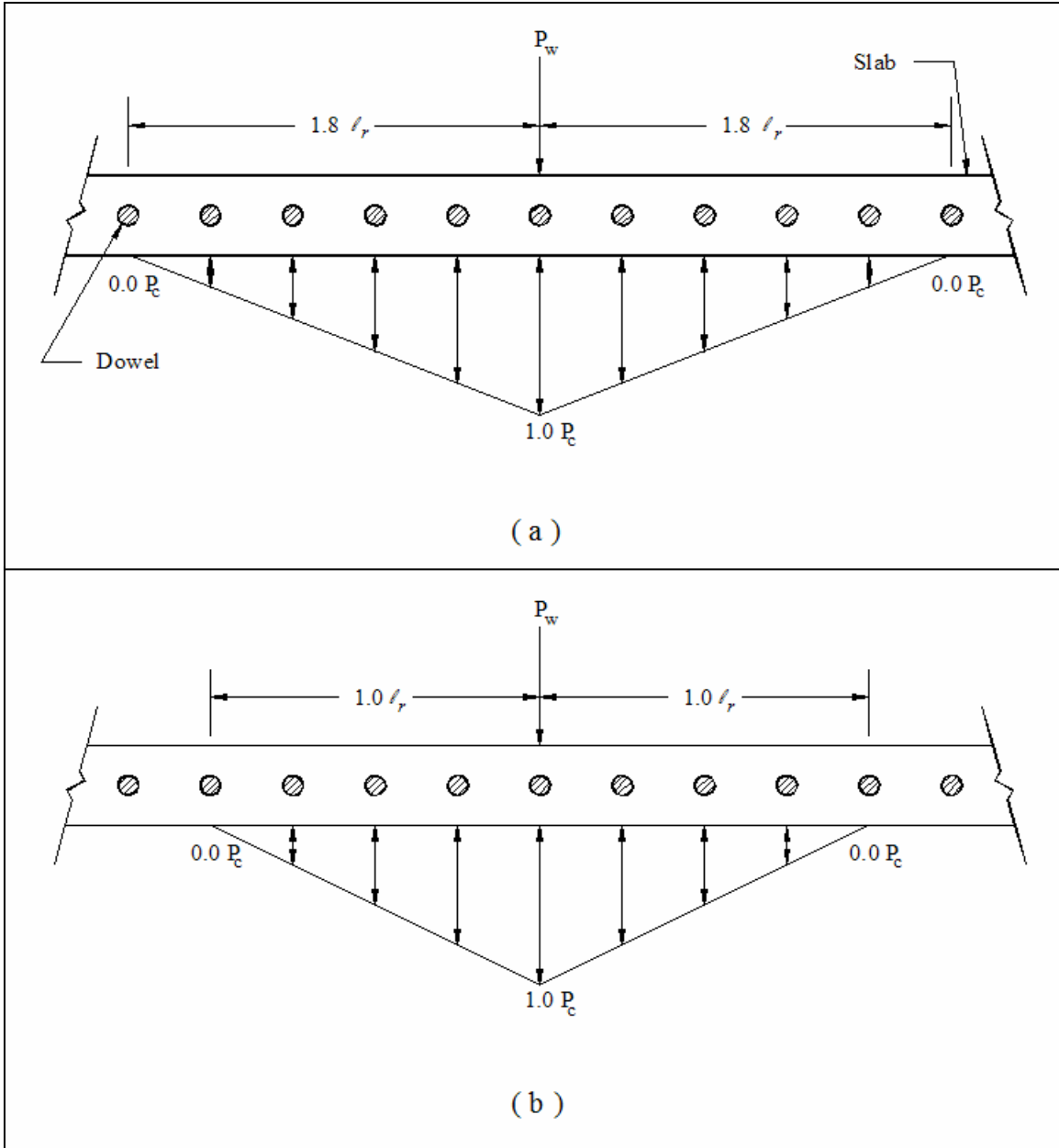


Figure 2.1. Load distribution model by Friberg (a), and Tabatabaie (b)

Finite element modeling of doweled joints by Tabatabaie [20] showed that an effective length of $1.01\ell_r$ from the applied wheel load is more appropriate for dowels used in practice today. A linear approximation was also shown to exist with the maximum dowel shear occurring directly beneath the load and decreasing to a value of zero at a distance of $1.01\ell_r$ from the load.

If the force transferred by a dowel located directly beneath the wheel load is designated as P_c , then the shear force in any other active dowel can be determined by multiplying the height of the triangle below that particular dowel by P_c . A value of 1.0 is assumed for the height of the triangle directly below the load as shown in Figure 2.1.

The shear force in the dowel directly under the load is obtained by dividing the transferred load, P_t , by the number of effective dowels, as shown by Equation 2-3.

$$P_c = \frac{P_t}{\# \text{ Effective Dowels}} \quad (2-3)$$

The sum of the heights of the triangle under each dowel gives the number of effective dowels.

2.2. Modulus of Dowel Support

The deflection of a dowel bar within pavement can be modeled using Timoshenko's model of a beam on an elastic foundation [21].

$$-ky = EI \frac{d^4 y}{dx^4} \quad (2-4)$$

Where,

k = Modulus of foundation (psi)

y = Vertical dowel deflection (in)

E = Young's modulus for dowel (psi)

I = Moment of inertia for dowel (psi)

The general solution of Timoshenko's differential equation is as follows in Equation 2-5.

$$y = e^{\beta x} (A \cos \beta x + B \sin \beta x) + e^{-\beta x} (C \cos \beta x + D \sin \beta x) \quad (2-5)$$

Where,

$$\beta = \text{Relative stiffness of beam on foundation} = \sqrt[4]{\frac{k}{4EI}}$$

When applying appropriate boundary conditions to Equation 2-5, the constants A, B, C, and D can be obtained. In the case of a semi-infinite beam with a point load, P, and moment, M_0 , Timoshenko's equation becomes the following:

$$y = \frac{e^{-\beta x}}{2\beta^3 EI} [P \cos \beta x - \beta M_0 (\cos \beta x - \sin \beta x)] \quad (2-6)$$

Equation 2-6 was applied by Friberg to evaluate a dowel with semi-infinite length and an elastic base. In order to calculate the deflection at the face, Equation 2-6 is applicable by setting $x=0$. Equation 2-6 then becomes the following:

$$y_0 = \frac{P_t}{4\beta^3 EI} (2 + \beta z) \quad (2-7)$$

and

$$\beta = \sqrt[4]{\frac{k_0 b}{4EI}} \quad (2-8)$$

Where,

k_0 = Modulus of dowel support (pci)

b = Dowel bar width (in.)

P_t = Load carried by dowel (lbs)

z = Joint width (in.)

Equations 2-7 and 2-8 can be solved by calculating a y_0 value from the data, solving for β using Equation 2-7, and finally obtaining k_0 from Equation 2-8.

The deflection of the dowel at the face of the joint can be calculated using the relative displacement between slabs and the joint width. A diagram of the interaction between the two slabs is shown in Figure 2.2.

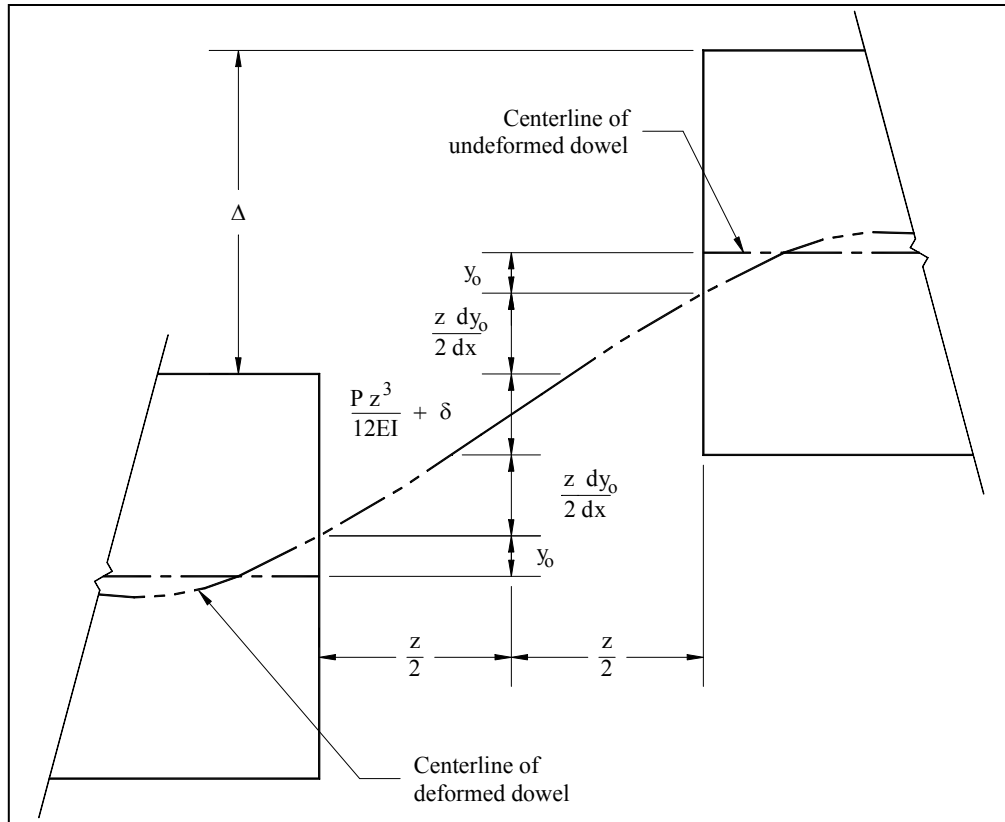


Figure 2.2. Relative deflection between slab sections

According to the above figure, the relative deflection, Δ , is dependent on four main components:

- Deflection at each joint face, y_0
- Deflection due to the slope of the dowel, $\frac{z dy_0}{dx}$
- Moment deflection, $\frac{Pz^3}{12EI}$
- Shear deflection, δ

The relative deflection, Δ , can be calculated by using Equation 2-9:

$$\Delta = 2y_0 + z \frac{dy_0}{dx} + \frac{Pz^3}{12EI} + \delta \quad (2-9)$$

Where,

$$\delta = \text{Shear deflection} = \frac{\lambda Pz}{AG}$$

P = Load carried by dowel (lbs)

A = Cross-sectional area of dowel (in.²)

λ = *Form Factor* = 10/9 (assumed) for elliptical dowels

G = Shear modulus (psi)

For this report, the joint widths are very narrow, roughly 0.125 inches. Due to the small differential displacement and joint width, both moment deflection and slope deflection were neglected. The authors assumed that the numbers would be insignificant due to the total deflection calculation. The following equation was used to calculate y_0 after making the appropriate changes to Equation 2-10:

$$y_0 = \frac{(\Delta - \delta)}{2} \quad (2-10)$$

3. TESTING PROGRAM

3.1. Project History

The project site for the elliptical FRP dowel bars is located just west of Melbourne, Iowa, on Iowa Highway 330. Field installation of these dowel bars was done as part of a 7.864-mile (12.656-km), four-lane divided-highway construction project. The project's pavement construction was completed using the metric system; therefore, all stationing is measured in meters (see Figure 3.1).

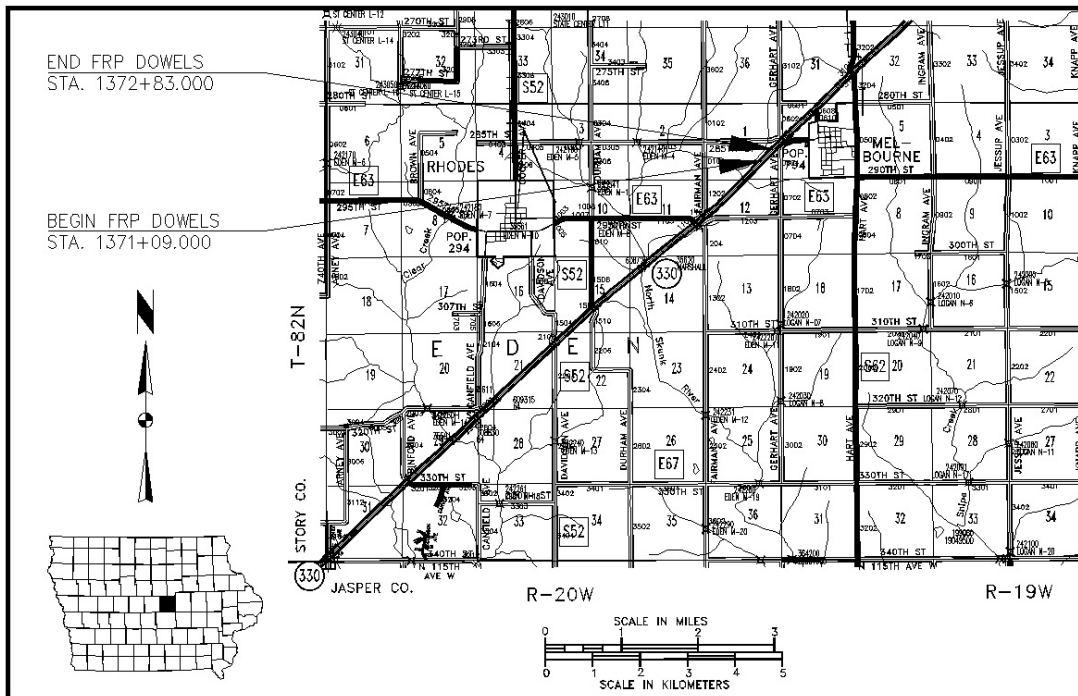


Figure 3.1. Project site map

3.1.1. Dowel Bar Locations

Placement of the dowel bars occurred in the northbound lanes at thirty joint locations beginning at Station 1371+09 and ending at Station 1372+83. The spacing between each joint is 19.69 feet (6 m) and all joints were constructed perpendicular to the edge of the concrete pavement. Spacing of the dowel bars within each joint was varied, with three different dimensions of 10, 12, and 15 inches (254, 305, and 381 mm). Table 3.1 and Figure 3.2 illustrate the layout and location of the elliptical FRP dowel bars installed for this project.

Table 3.1. Stationing and spacing of elliptical FRP dowel bars

Begin Station	End Station	Number of Joints	Dowel Spacing, in. (mm)
1371+09	1371+61	10	10 (254)
1371+69	1372+23	10	12 (305)
1372+29	1372+83	10	15 (381)

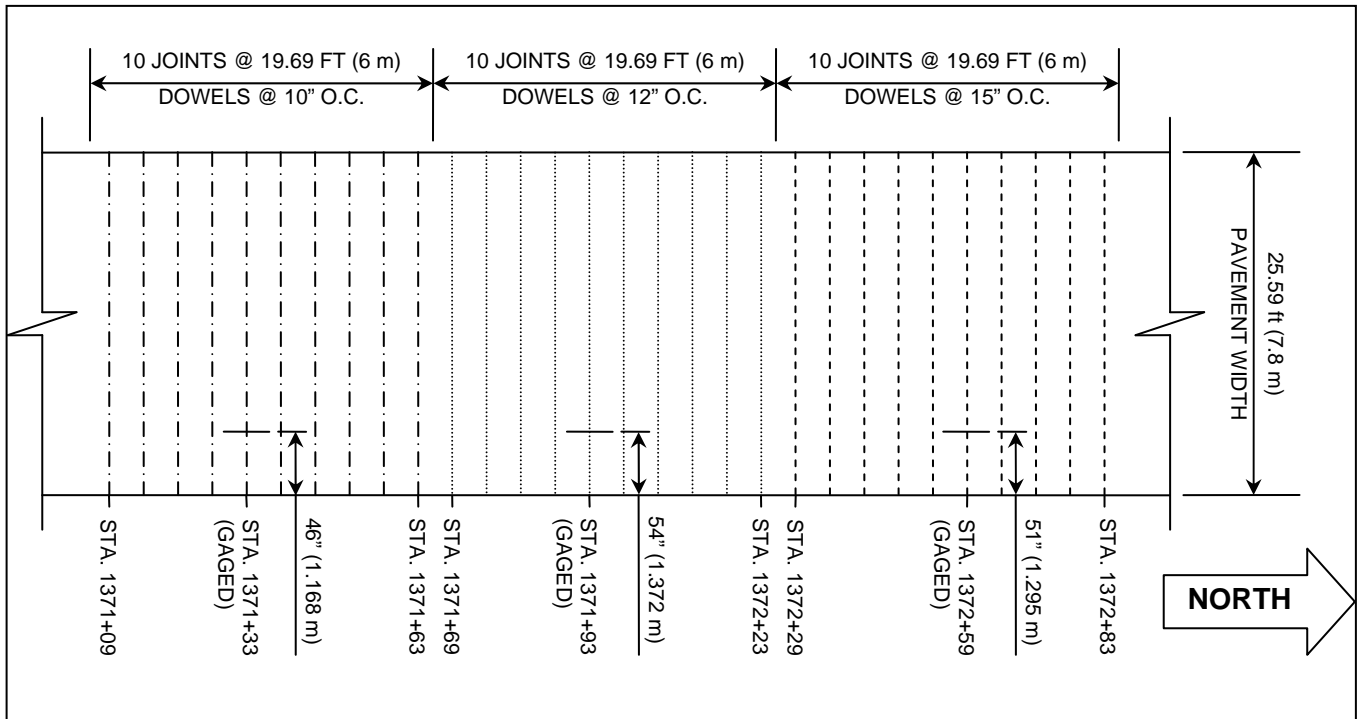


Figure 3.2. Stationing and spacing of elliptical FRP dowel bars

3.1.2. Construction History

Specially built elliptical dowel bar basket assemblies were used to install the dowel bars in this portion of the project in order to elevate the center of the bars 5 inches (127 mm) from the subgrade, placing them in the center of the 10-inch (254-mm) slab pavement. Figure 3.3 shows a photo of a typical dowel bar basket assembly. Conventional welding methods for attaching the dowel bars to the baskets, as used with steel dowel bars, could not be used with the FRP material. Therefore, plastic ties and epoxy were used to attach the FRP dowel bars to the baskets. Special care was taken to ensure that the epoxy was strong enough to hold the bars in place during concrete placement, yet brittle enough to crack and allow the bars to move in the longitudinal direction after the concrete had cured.



Figure 3.3. Dowel bar basket assembly (bars at 10-inch spacing)

Each of the basket assemblies were originally placed and staked at six inches (152 mm) from the proposed edge of the pavement. However, during the paving process, adjustments had to be made along the east edge of the northbound lane due to the discovery that some of the basket assemblies extended beyond the actual edge of the pavement. The eastern-most bar and basket end was removed from the dowel bar basket assemblies at Stations 1371+09, 15, 21, 87, and 1372+65 to prevent any contact between the basket assemblies and the paver.

Strain gage wires were buried just beneath the subgrade over the width of the shoulder to avoid interference with the pavement construction. After the paving was complete, the wires were uncovered and threaded through a protective PVC pipe and again buried under the shoulder. Strain gage wires for the dowel bars at Station 1371+33, which correspond to the 10-inch (254-mm) spacing, were destroyed during the shoulder construction process.

3.2. Test Descriptions

The testing for this project involved both mechanical and visual tests during the period of observation beginning in the fall of 2002. During the contract period, the following tests were conducted:

- Strain gages

- Falling weight deflectometer (FWD)
- Faulting
- Joint opening
- Visual distress surveys
- Laboratory tests

3.2.1. Strain Gages

In order to determine the stresses on the dowel bars at different spacings, one dowel bar from each of the 10-, 12-, and 15-inch (254-, 305-, and 381-mm) spacings was fitted with eight strain gages. The strain-gaged dowel bars were located as follows:

- 10-inch (0.254-meter) spacing: at Station 1371+33 on fifth bar in from right edge of pavement (46 inches [1.168 meters] from edge of pavement)
- 12-inch (0.305-meter) spacing: at Station 1371+93 on fifth bar in from right edge of pavement (54 inches [1.372 meters] from edge of pavement)
- 15-inch (0.381-meter) spacing: at Station 1372+59 on fourth bar in from right edge of pavement (51 inches [1.295 meters] from edge of pavement)

Four gages were placed on the top and bottom of each dowel bar. Strain gages were located at a distance of 1.5 and 4.5 inches (38 and 114 mm) from the centerline of the 18-inch (457-mm) long dowel bars. These distances were chosen to be the same as the strain gages placed on the coinciding elliptical steel dowel bar project so that a comparison between the two types of bars would be made easier. Gages were glued to the bars and strain gage wire was then soldered to each strain gage. The gage and wires were then covered to prevent damage before installation. Gages were labeled A through H, as listed in Figure 3.4.

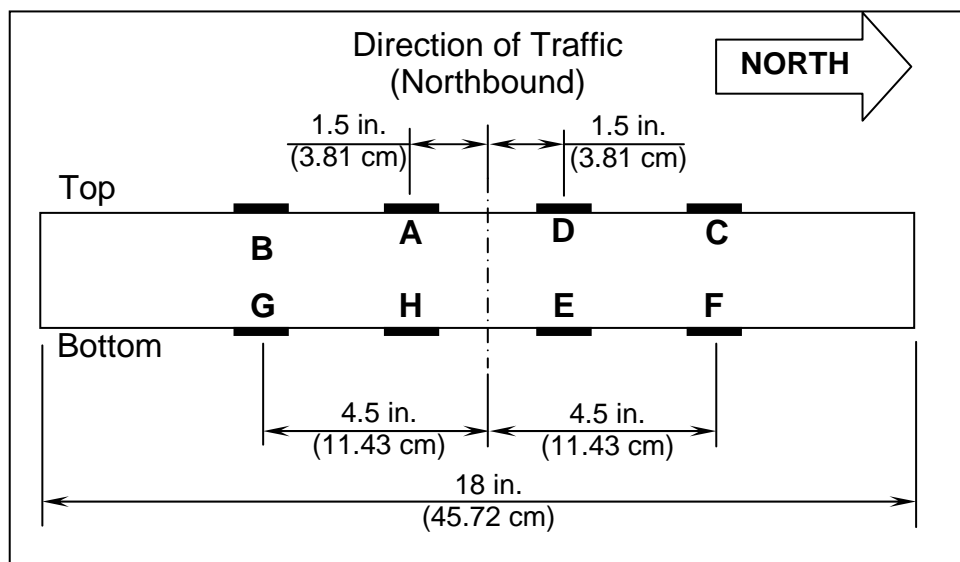


Figure 3.4. Location of strain gages on elliptical FRP dowel bars

Strain gage readings were taken twice, during each measurement period. One set of readings was taken during FWD testing, and the other set was taken while a loaded truck traversed the joints containing the gaged dowels at crawl speed (Figure 3.5) during each measurement period.



Figure 3.5. Loaded dump truck

Since not all strain gages were working properly, k_0 cannot be calculated directly; however, the deflected shape can be determined based on Friberg's semi-infinite beam theory, and y_0 can be found and directly compared to the y_0 value from FWD testing. The equation for the deflected shape of a dowel bar is given in Equation 2-6:

$$y(x) = \frac{e^{-\beta \cdot x}}{2 \cdot \beta^3 \cdot E \cdot I_z} [(V - M \cdot \beta) \cdot \cos(\beta \cdot x) + (M \cdot \beta) \cdot \sin(\beta \cdot x)] \quad (2-6)$$

Where,

$$\beta = \sqrt[4]{\frac{k_o \cdot b}{4 \cdot E \cdot I_z}} \quad (2-8)$$

To solve this equation, the moment, M , and shear, V , must be determined for any position across the length of the dowel. The moment at each strain gage can be determined using the following equation:

$$\sigma = \frac{M \cdot c}{I_z}$$

Where,

$$\sigma = \varepsilon \cdot E$$

Therefore,

$$M = \frac{\varepsilon \cdot E \cdot I_z}{c}$$

ε = strain from strain gages (microstrains)

σ = the stress based on the strain reading (psi)

E = the modulus of elasticity (psi)

I_z = the moment of inertia (in⁴)

c = the radius of the minor axis of the elliptical dowel bar (in.)

The moment for any given location on the bar can be interpolated from the moments determined from the strain gages and the following assumed boundary conditions:

- Shear is zero at each end of each dowel
- Moment is zero at each end of each dowel
- Moment is zero at the center of each dowel
- The inflection point occurs at the center of each dowel
- $k_0 = 939,000$ psi for an FRP elliptical dowel or $1,052,000$ psi for a steel elliptical dowel (both determined from current lab testing at ISU as discussed in Section 3.2.6)

The shear at any point on the dowel can be determined from [13]:

$$V(x) = -\frac{e^{-\beta \cdot x}}{2} \cdot [(P_c - M_o \cdot \beta) \cdot (2 \cdot \cos(\beta \cdot x) - 2 \cdot \sin(\beta \cdot x)) + M_o \cdot \beta \cdot (4 \cdot \sin(\beta \cdot x) + 2 \cdot \cos(\beta \cdot x))]$$

Where,

$$M_0 = \frac{P_c \cdot z}{2}$$

P_c = the load applied to the dowel determined by load distribution (see Section 2.2 and Figure 3.6)

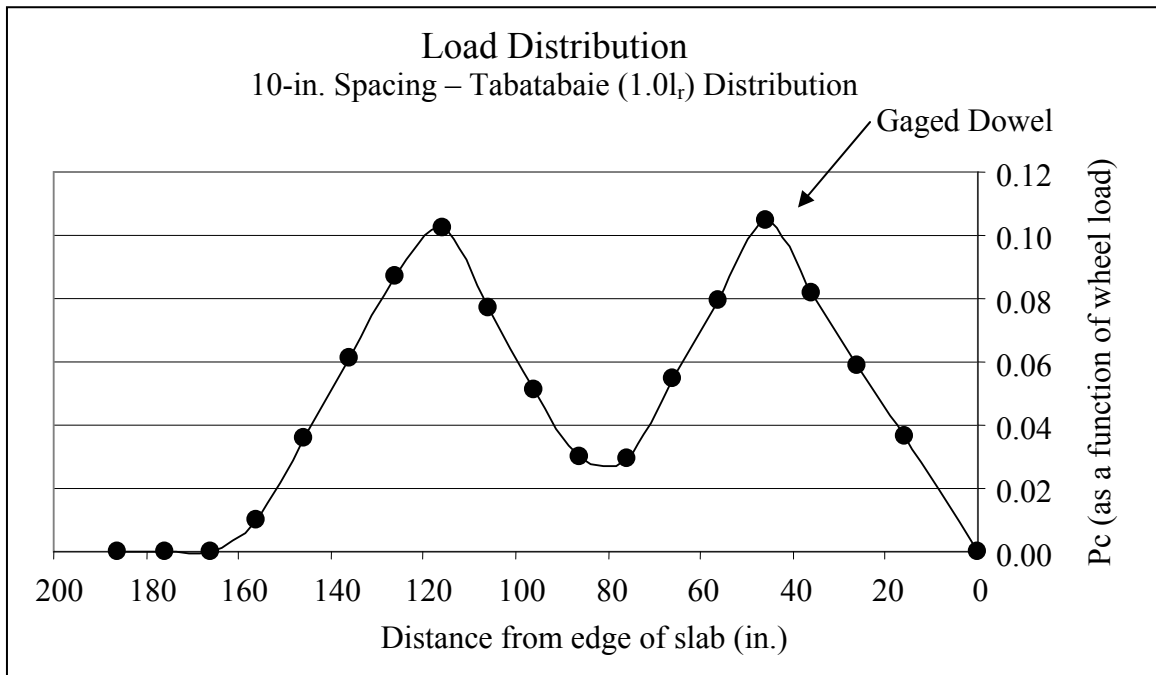


Figure 3.6. Load distribution

Once moment and shear are calculated from the strain gage readings and given boundary and loading conditions, deflection along the dowel, $y(x)$, can be plotted. See Figure 3.7 for an example plot of deflected shape. Note that this figure illustrates a general deflected shape for the dowel bars. Therefore, no values are given for the actual deflections. These deflections, however, typically have an order of magnitude of 1/10,000 of an inch for the tests included in this report.

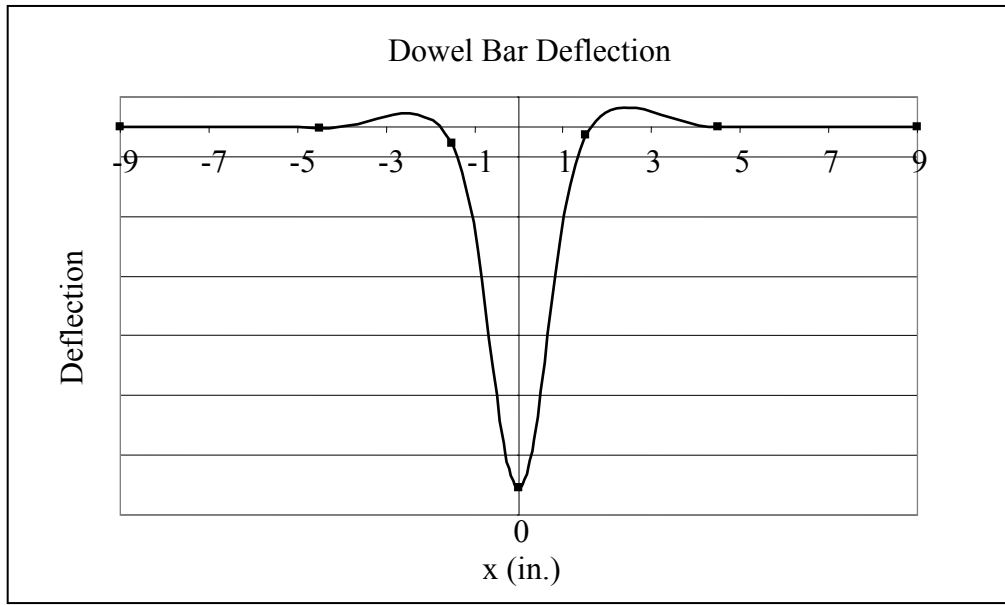


Figure 3.7. Deflected shape of dowel bar

3.2.2. *Falling Weight Deflectometer*

The FWD is a nondestructive test that involves applying a known load near a pavement joint. Loads and their corresponding deflections obtained from the FWD test were placed into a spreadsheet program. The deflections corresponding to each load were plotted with each sensor's distance from the load. The program was used to calculate a second-order equation relating downward deflection (in 0.001 inches) to distance from the load (in inches). The deflection equation was used to determine relative displacement between each slab surface at the joint.

The FWD tests were conducted by the Iowa Department of Transportation (see Figure 3.8).



Figure 3.8. Falling weight deflectometer

Tests were made on three transverse joints and three mid-panel locations per test section per lane. Testing was performed in the outside wheelpath, 2 feet (0.6 m) from the outer edge, in each lane.

FWD tests utilized nine deflection sensors placed at -4, 4, 12, 18, 24, 36, 48, and 60 inches (-102, 102, 305, 457, 610, 914, 1219, 1524 mm) from the center of the load plate (See Figure 3.9).

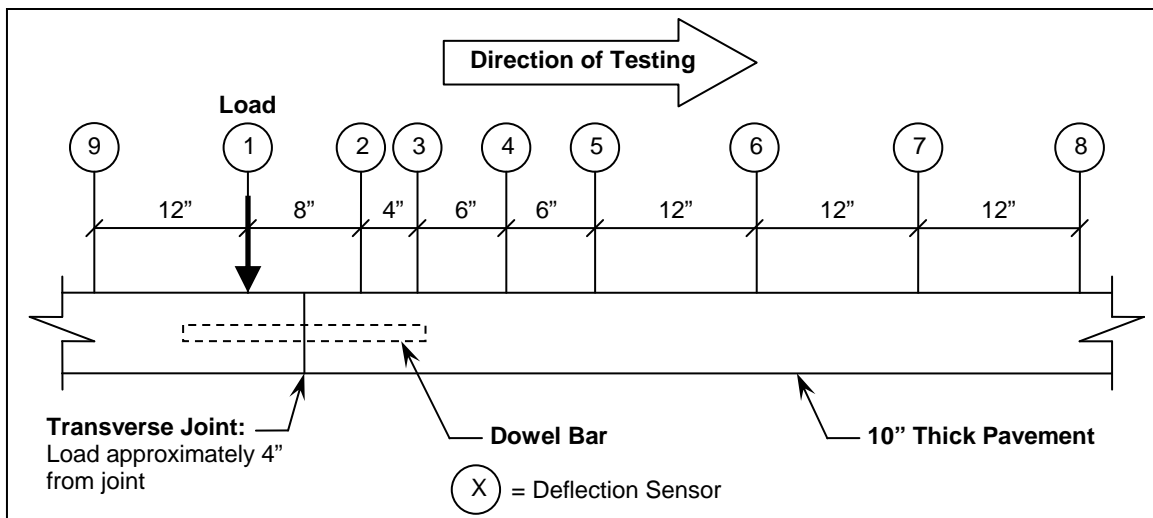


Figure 3.9. Location of FWD loading and deflection sensors

One seating drop and three separate load test drops were conducted at each test location with a target load of 9,000 force pounds (40.033 kN). Results from the FWD testing are discussed in the “Analysis and Results” portion of this report in Appendix A, with actual measurement data and graphs.

3.2.3. *Faulting*

The Georgia fault-meter was used to measure faulting at the inside and outside wheelpaths of the driving lane (see Figure 3.10).



Figure 3.10. Georgia fault meter

The digital readout of the fault meter indicates positive or negative faulting in millimeters. To obtain the readings, the fault meter was set on the pavement facing traffic, on the leave side of the joint, and the measuring probe was in contact with the approach slab. Movement of the probe was then transmitted to a linear variance displacement transducer to measure the difference in elevation between the two sides of the joint or the amount of faulting. A slab that is lower on the leave side of the joint indicates positive faulting, and a slab leaving the joint that is higher will register as a negative fault. Measurements are taken in the driving lane, outside wheelpath 30 inches (762 mm) from the edge of the pavement and in the passing lane, inside wheelpath some 18 inches (457 mm) from the edge of the pavement. Results of the faulting measurements are discussed under “Analysis and Results” in Appendix B, with actual measurement data [14].

3.2.4. *Joint Opening*

To monitor the transverse joint opening, surveyor mag nails were placed in the wet concrete (flush with the surface) on either side of the joints in the outside lane to serve as

a point of reference for measurement. Transverse joint movement was monitored at 10 consecutive joints in the middle of each test section. At these locations, nails were placed in the concrete within the first hour of paving 12 inches (305 mm) in from the edge of the slab with 10 inches (254 mm) between nails (5 inches [127 mm] offset either side of the joint).



Figure 3.11. Calipers and surveyor nails (nails not installed)

Figure 3.11 shows an example of the nails and calipers used. Initial measurements between the nails shortly after paving served as a benchmark for future joint movement. Joint opening measurements were made at the same time as faulting and visual distress surveys. Measurements from each joint opening survey can be found in Appendix B, and graphs displaying the trends are in Appendix C [14].

3.2.5. Visual Distress Surveys

Visual distress surveys were performed concurrently with the biannual joint opening and faulting measurements by ISU research staff. Completed in accordance with the Strategic Highway Research Program, the visual distress surveys consisted of a visual evaluation of the pavement surface for any signs of horizontal slab movement, spalling, or cracking. No signs of visual distress were recorded for the elliptical FRP dowel sections.

3.2.6. Laboratory Tests

Tests were performed at ISU in the structures laboratory located in Town Engineering Building. The tests are a part of ongoing research to investigate the current AASHTO T253-76 [22] testing method for dowel bars. The test specimens were constructed using concrete and various dowel shapes. Steel and glass fiber reinforced polymer (GFRP) dowels were tested. Each specimen consisted of three concrete blocks connected with two dowel bars (see Figure 3.12).

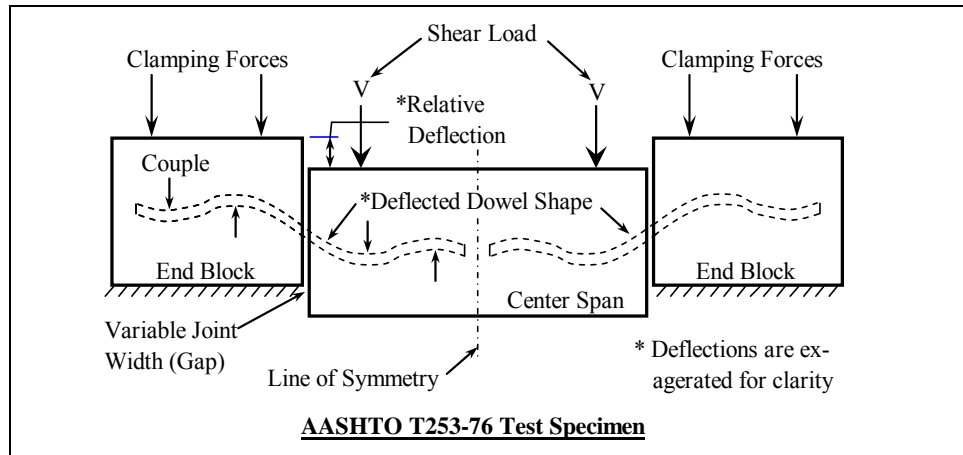


Figure 3.12. AASHTO T253-76 test diagram [13, 22]

The specimens featured in this report all contained 2.25 x 1.25-inch elliptical GFRP dowels. The GFRP test results are included in this report because there is insufficient data from previous research to compare k_0 values calculated using lab data and field data. Previous research involving k_0 for steel dowels was available for comparison in this report.



Figure 3.13. Load test frame

The load frame used to test the lab specimens is shown in Figure 3.13. The vertical pipes supporting the top cross beam were post-tensioned to the structural tie-down floor using a 1.25-inch diameter steel Dywidag rod in each pipe. This was done to ensure smooth load transfer from the hydraulic actuator to the concrete test specimen. Downward load was transferred from the hydraulic jack to the test specimen by using a six-inch-deep wide flange steel beam with web stiffeners. Two 1.25-inch diameter solid steel bars were placed 3 inches from each end of the center block in order to transfer the downward load

from the beam to the concrete. Thin sheets of neoprene were placed beneath the loaded rollers to allow for an even transverse load application along each bar.

The end blocks of the specimen were clamped down to the lower steel support plates using high-strength Dywidag steel rods. The goal of each end support was to create a fixed-end condition on each side of the specimen. The bars were tightened to prevent end-block rotation. The clamping mechanisms were tightened using wrenches in lieu of using a hydraulic jack to avoid external stresses acting on the dowels and affecting the deflection behavior of the bar. The goal of the fixed-end conditions is to promote shear behavior in the sample dowel bars. Another reason for the fixed-end condition is to minimize the effect of bending forces on the dowel.

The specimens were instrumented with direct current deflection transducers (DCDTs). A total of eight DCDTs were used. Four were used to measure relative deflections on the right and left ends of the specimen. Two were placed at the far ends of the end blocks to monitor the movement in the restrained ends. Two more were placed on the base plates that support the specimen in order to monitor movement of the entire testing surface.

The procedure used to calculate k_0 with field data was also implemented with lab data. The force acting on each dowel was assumed to be half the total load acting on the apparatus. All deflections not pertaining to the relative deflection of the middle block were neglected due to their small magnitude.

4. ANALYSIS AND RESULTS

4.1. FRP Dowels

4.1.1. Falling Weight Deflectometer

The FWD test deflection readings (see Appendix A) can be used to determine k_0 . First the relative deflection, Δ_{REL} , is determined from the deflection readings (see Figure 2.2 and Section 2.3). Next, shear deflection, δ , is determined by the following:

$$\delta = \frac{\lambda \cdot P_c \cdot z}{A \cdot G}$$

Where,

$$\lambda = \frac{10}{9} \text{ (approximate) for ellipses}$$

P_c = the load applied to the dowel (lbs)

z = the width of the joint (in.)

A = the cross-sectional area of the dowel (in.²)

$$G = \frac{E}{2(1 + \nu)} = \text{the shear modulus (psi)}$$

E = the modulus of elasticity (psi)

ν = Poisson's ratio

Then, y_0 can be calculated:

$$y_0 = \frac{\Delta_{REL} - \delta}{2}$$

Finally, Equation 2-7 is solved for β and k_0 is determined. Figure 4.1 shows the average k_0 values for the three dowel bar spacings taken from various FWD testing dates.

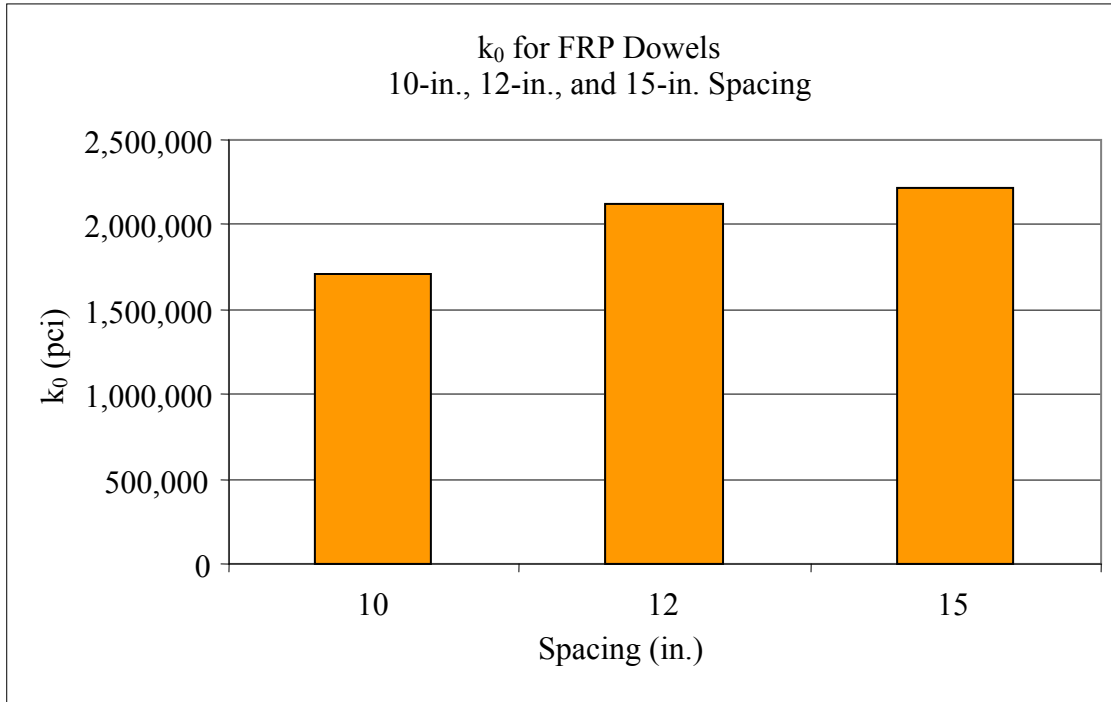


Figure 4.1. Average k_0 for each FRP dowel bar spacing

4.1.2. Strain Gages

Due to several malfunctioning strain gages, the results from the strain gages were limited. However, enough data was available to estimate the deflected shape of an FRP dowel for the 10-inch spacing. Figure 4.2 shows this deflected shape. In this case, the applied load on the dowel bar due to the crawl truck was 830 lbs. Using the method described in Section 3.2.1, the maximum deflection due to the crawl truck was determined to be 0.56 mils (0.014 mm) for the dowel placed directly under the wheelpath (i.e., the dowel that receives the greatest load due to the truck).

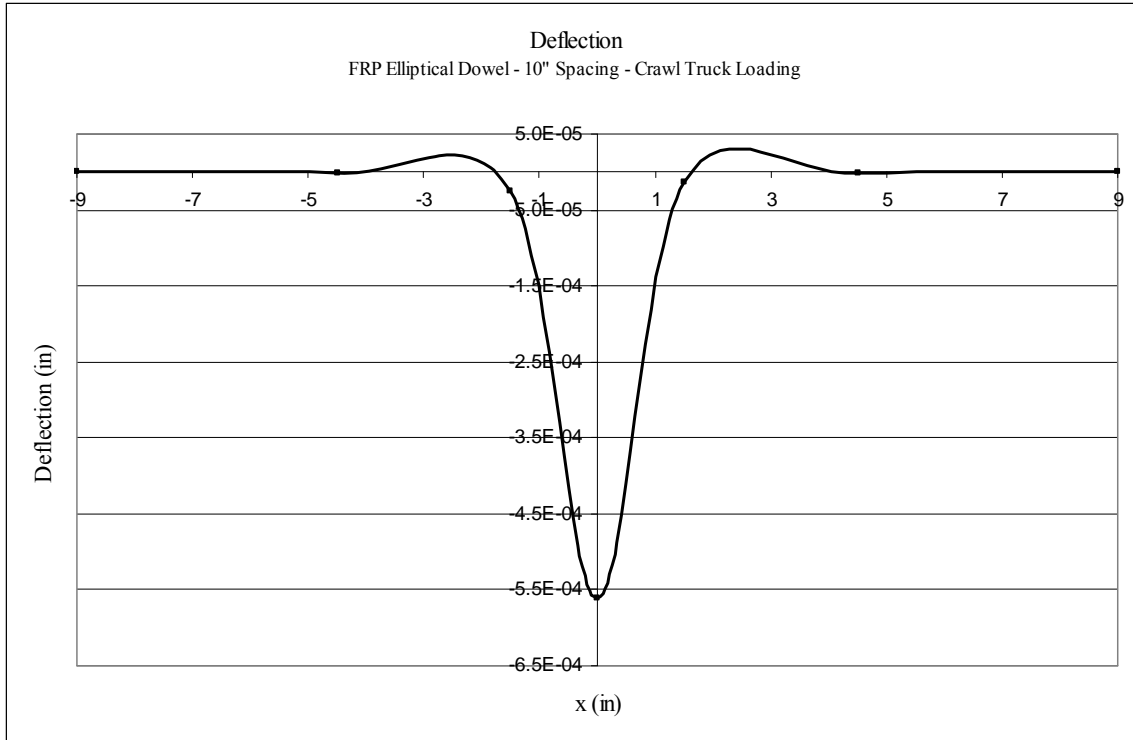


Figure 4.2. Deflected shape of an FRP dowel

4.1.3. Faulting

Analysis of the faulting data revealed no significant trends in the behavior of the elliptical FRP dowel bars between the variable spacings. Faulting measurements and graphs depicting the significance of these measurements are shown in Appendix B. Table B.1 lists the field measurements taken during each data collection period, along with the temperature of the pavement. Table B.2 lists the average faulting measurements calculated at each dowel spacing (10-, 12-, and 15-inch). Figures B.1 and B.2 display the average faulting in the driving and passing lanes, respectively, and Figure B.3 displays the average faulting across the entire section of pavement from each data collection period. No significant seasonal effects are shown in the faulting data between the spring and fall data collection periods. However, one item of note is that through the life of the project, average faulting measurements have shifted from negative to positive. Due to the small order of magnitude of these measurements, which ranged from 0.1 to 0.8 mm (0.0039 to 0.031 inches)^{*}, the accuracy of the measuring device, which was in 0.1-mm (0.0039-inch)^{*} increments, and the short life of the project, there is not enough detailed information to make a statistical relationship between these results, and no accurate conclusions can currently be made.

^{*} These measurements were taken using the metric system; therefore, the actual metric measurement is listed first and is shown for the true measurements in Appendices B and C.

4.1.4. Joint Opening

The change in joint opening data over the life of the project for the elliptical FRP dowel bars can be found in Appendix C. Table C.1 lists the field measurements taken during each data collection period. Table C.2 and corresponding Figure C.1 display the average joint opening for each dowel spacing. The change in joint opening generally relates to the change in temperature between the testing periods. Increased temperatures cause the pavement slabs to expand, thereby decreasing the joint opening. Decreased temperatures result in contraction of the pavement slab, which in turn increases the joint opening. Figure C.1 shows that the joints located in the sections of 10-inch and 12-inch dowel spacing performed about the same, with a change in opening of about 0.6 mm (0.024 inches)* whereas the joints with 15-inch dowel spacing underwent a change in joint opening of about 1.0 mm (0.039 inches)*. This indicates that the joints are operating properly by exhibiting free movement through the change in temperature, while on average the FRP dowels spaced at 15 inches are allowing more movement than the other dowel spacings.

4.2. Steel Dowels

4.2.1. Falling Weight Deflectometer

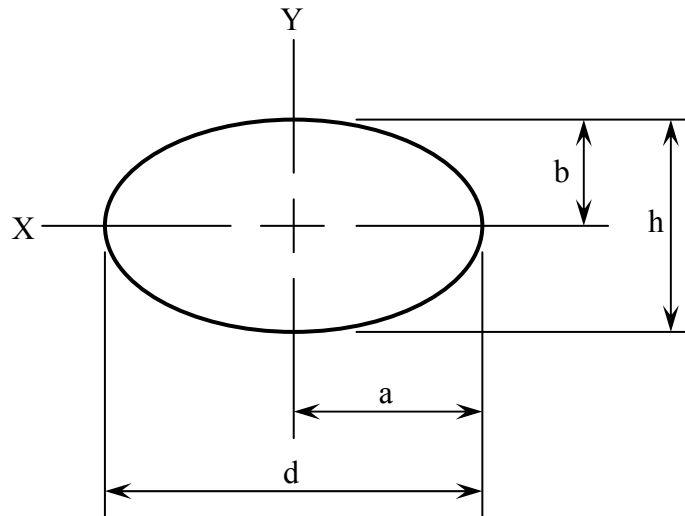


Figure 4.3. Steel dowel bar detail

The k_0 values for elliptical steel dowel bars from FWD testing were calculated in the same way as the values for elliptical FRP dowels, as outlined in Section 4.1.1. The elliptical steel dowels tested were not a part of this project, but part of a similar project on the same highway. That project included two elliptical steel sizes (in addition to 1.5-inch diameter standard round bars) with dimensions shown in Figure 4.1 and Table 4.1.

Table 4.1. Steel dowel bar dimensions

Dowel Type	a (in)	b (in)	d (in)	h (in)	A (in²)	I (in⁴)
Standard Round	0.75	0.75	1.5	1.5	1.767	0.2485
Medium Elliptical	0.827	0.558	1.654	1.115	1.473	0.1125
Heavy Elliptical	0.985	0.669	1.969	1.338	2.084	0.2315

These dowels were placed at 12-inch, 15-inch, and 18-inch spacings, respectively. Charts showing the k_0 values for the heavy elliptical, medium elliptical, and standard round dowels can be found in Appendix D.

4.2.2. Strain Gages

Strain gage readings were used as outlined in Section 3.2.1 to estimate the deflected shape, due to crawl truck loading, of the heavy elliptical (1.969-inch major axis and 1.338-inch minor axis) steel dowels for 12-, 15-, and 18-inch spacing. Figures of these deflected shapes can be found in Appendix D.

Table 4.2 summarizes the dowel loading and y_0 value determined using the strain gages for each spacing.

Table 4.2. Estimated y_0 from strain gage readings for heavy elliptical steel dowels

Spacing (in)	Dowel Load (lbs)	y_0 (mils)
12	1012	0.50
15	1196	0.59
18	1530	0.75

4.2.3. Faulting

Faulting data for standard round, medium elliptical, and heavy elliptical steel bars were compiled from a segment of the same highway. This information is tabulated and plotted in Appendix F. Table F.1 lists the field measurements taken during each data collection period, along with the temperature of the pavement. Table F.2 lists the average faulting measurements calculated at each test section, along with the respective dowel bar types and spacings. Average faulting values for the standard round dowel bars are listed in Table F.3 and plotted in Figures F.1, F.2, and F.3. Average faulting values for the medium elliptical dowel bars are listed in Table F.4 and plotted in Figures F.4, F.5, and F.6. Average faulting values for the heavy elliptical dowel bars are listed in Table F.5 and plotted in Figures F.7, F.8, and F.9. These tables and graphs display the average faulting

in the driving and passing lanes and also the average faulting across the entire section of pavement from each data collection period.

4.2.4. Joint Opening

Joint opening data were also compiled for standard round, medium elliptical, and heavy elliptical steel bars were compiled from a segment of the same highway. This information is tabulated and plotted in Appendix G. Table G.1 lists the field measurements taken during each data collection period. Table G.2 lists the average changes in joint opening calculated at each test section, along with the respective dowel bar types and spacings. Table G.3 and corresponding Figure G.1 display the average joint openings for each steel dowel type and spacing. Again, these results indicate that the joints are operating properly by exhibiting free movement through the change in temperature.

5. SUMMARY OF PERFORMANCE

The vertical dowel deflections, y_0 , calculated at the center of each joint in the FRP dowel sections for 10-inch, 12-inch, and 15-inch spacing from FWD testing averaged values less than 1 mil (0.0254 mm). Results obtained from strain gage data also displayed y_0 values of less than 1 mil (0.0254 mm). Additionally, the relative deflections associated with the FWD testing were less than 2 mils (0.0508 mm). Faulting data, representing the effects of repeated loading, subgrade conditions, and weather over time, give maximum displacements across the joint of 0.067 inches (1.7 mm) and an average of 0.020 inches (0.508 mm). These small deflections show that the FRP dowels at each spacing provide adequate load transfer across the joints. Furthermore, the deflections are of magnitudes small enough to provide adequate rider comfort as vehicles traverse the joints.

The average value for the modulus of dowel support, k_0 , calculated for elliptical FRP dowels from the field FWD testing was about 2,000,000 pci. This value was an average of all dowel spacings; however, the data showed a trend of an increased k_0 with increased spacing. Moreover, the steel data showed the same trend for medium elliptical dowels but the opposite trend for heavy elliptical dowels. Thus, no general conclusion can be made about the effect of spacing on the value of k_0 . Therefore, parameter testing is needed to learn more about the spacing effects. However, previous ISU research [2] arrived at preliminary effects. See the conclusions of Porter et al. (2001). The value of k_0 determined from the lab testing was about 939,000 pci. Previous research also indicates that k_0 values determined from lab testing tend to be less than k_0 values calculated from field results.

Overall, this study has shown that FRP dowel bars performed adequately, as demonstrated by this field application of over 700 FRP dowel bars in Iowa Highway 330. The overall small measured deflections demonstrated that the FRP dowel bars provided adequate load transfer across all of the joints. These deflections were small enough to provide adequate rider comfort for vehicles crossing joints containing FRP dowel bars. Faulting and joint opening measurements were similar and demonstrated that the joints were operating properly.

6. FUTURE RESEARCH NEEDS AND IMPLEMENTATION

Several problems exist with the current theory used here to determine the deflected shape of the dowel, including the following:

- Inoperative strain gages due to unforeseen field conditions
- Test loads provided by the FWD and crawl truck were not large enough to provide relative deflections of sufficient magnitude to calculate k_0 accurately
- Additional tests are needed to determine an appropriate location of the inflection point of the dowel within the joint
- Additional research is needed to verify the boundary conditions

In the future, more precautions and care should be taken during construction and when installing strain gages to ensure proper performance. Also, additional strain gages should be implemented at the ends and center of the dowel bars to better estimate boundary conditions. By obtaining these boundary conditions and by having properly functioning strain gages, Timoshenko's finite beam theory (Equation 2-6) can be applied to calculate the deflected shape of the dowel more accurately.

Faulting and joint opening is valuable in determining the long term performance of the dowel bars; therefore, more long term testing is needed to determine the true behavior of the FRP dowels more accurately. The use of more test sections would also be invaluable, in that it would create a wider range of data to be analyzed.

Corrosion and other long term effects may affect the performance of the FRP dowel bars through time and therefore should also be monitored and analyzed over a longer testing period.

Additionally, full-scale lab testing of slabs with multiple dowel bars needs to be performed to determine the effects of dowel spacing on load distribution more accurately. Along with the load distribution testing, fatigue testing is needed to better evaluate the long-term capabilities of the elliptical FRP dowels subjected to cyclical loadings.

Expansion joints are placed in roadways wherever pavement meets a fixed structure, and therefore additional analysis, design, and testing of FRP dowels within expansion joints is needed. Additional research is needed for all types of joints to determine the effects of gap sizes other than 0.125 inches. The additional effects of deflection due to flexure will be necessary for joints containing larger gaps.

The polymer matrix of a fiber composite is hydroscopic, which means that it can potentially absorb water. The absorption of water and subsequent swelling of FRP dowels could possibly be a concern for the slippage mechanism of concrete pavement joints over a period of time. Therefore, this phenomenon should be investigated more fully [2].

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APPENDIX A. FALLING WEIGHT DEFLECTOMETER DATA FOR FRP

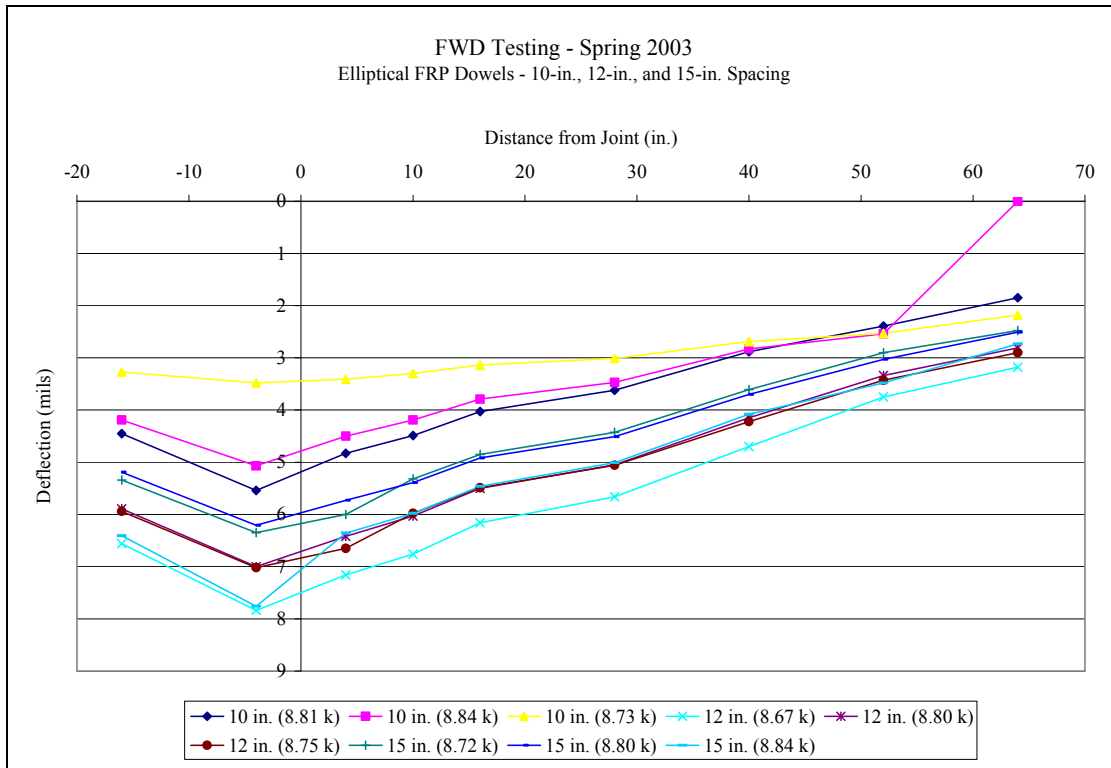


Figure A.1. Spring 2003 FWD testing: elliptical FRP

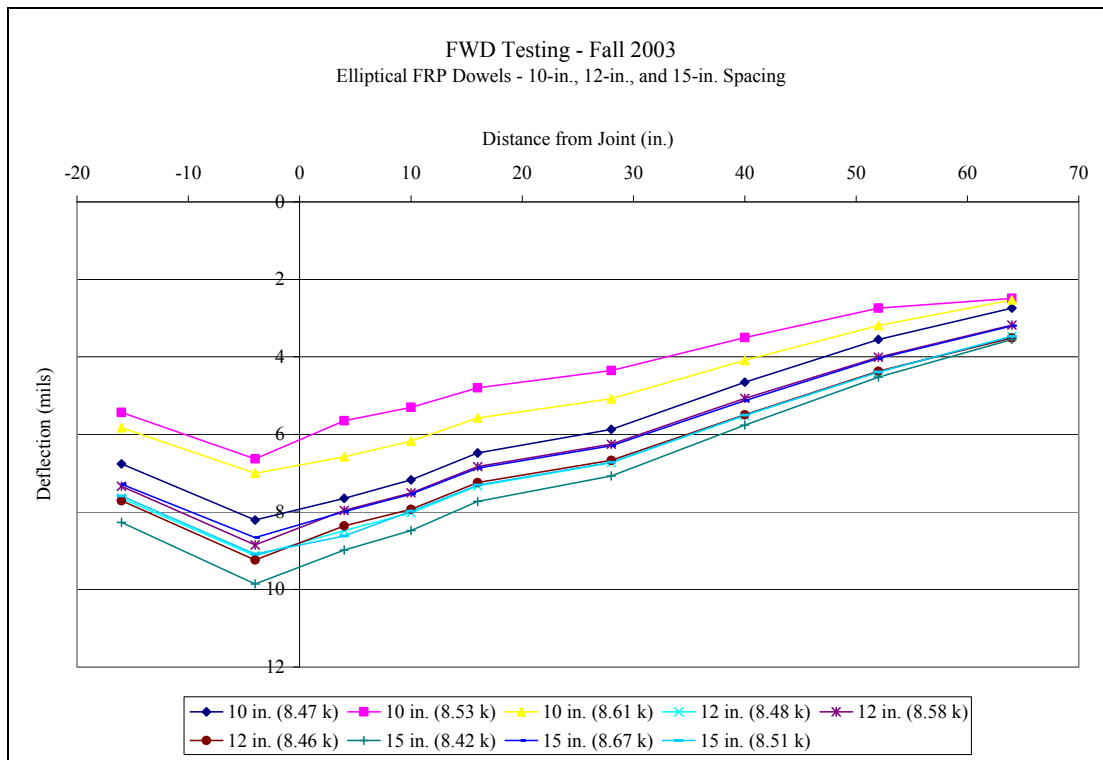


Figure A.2. Fall 2003 FWD testing: elliptical FRP

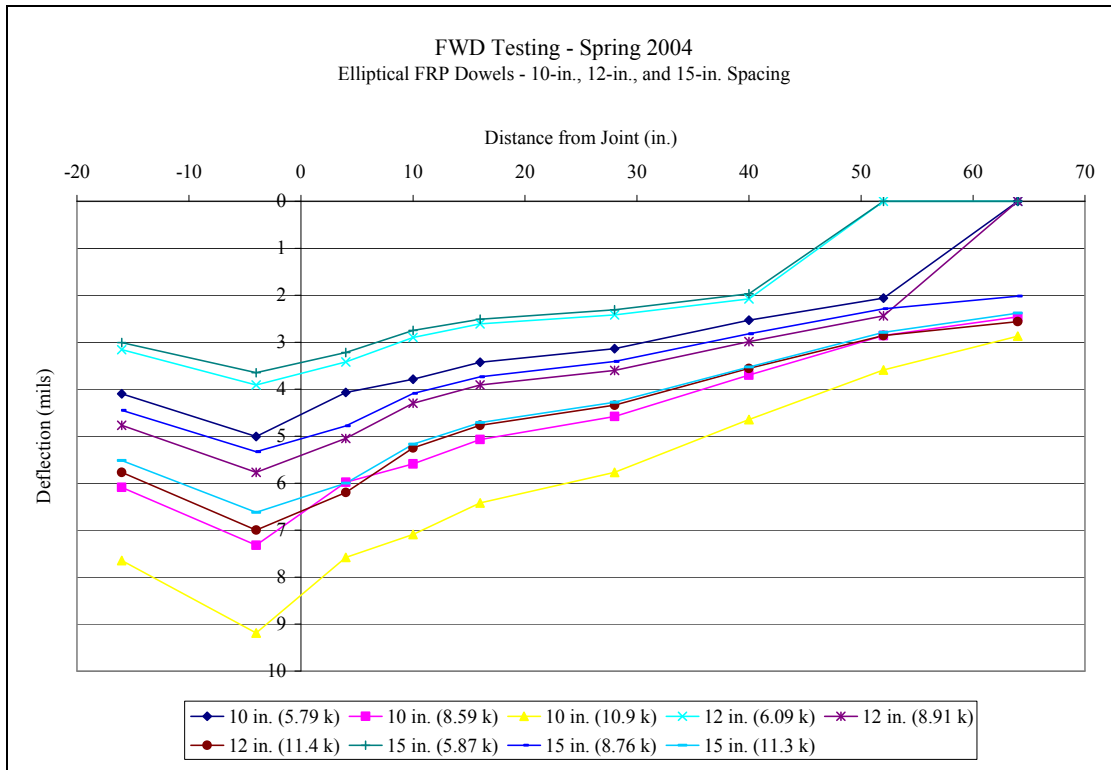


Figure A.3. Spring 2004 FWD testing: elliptical FRP

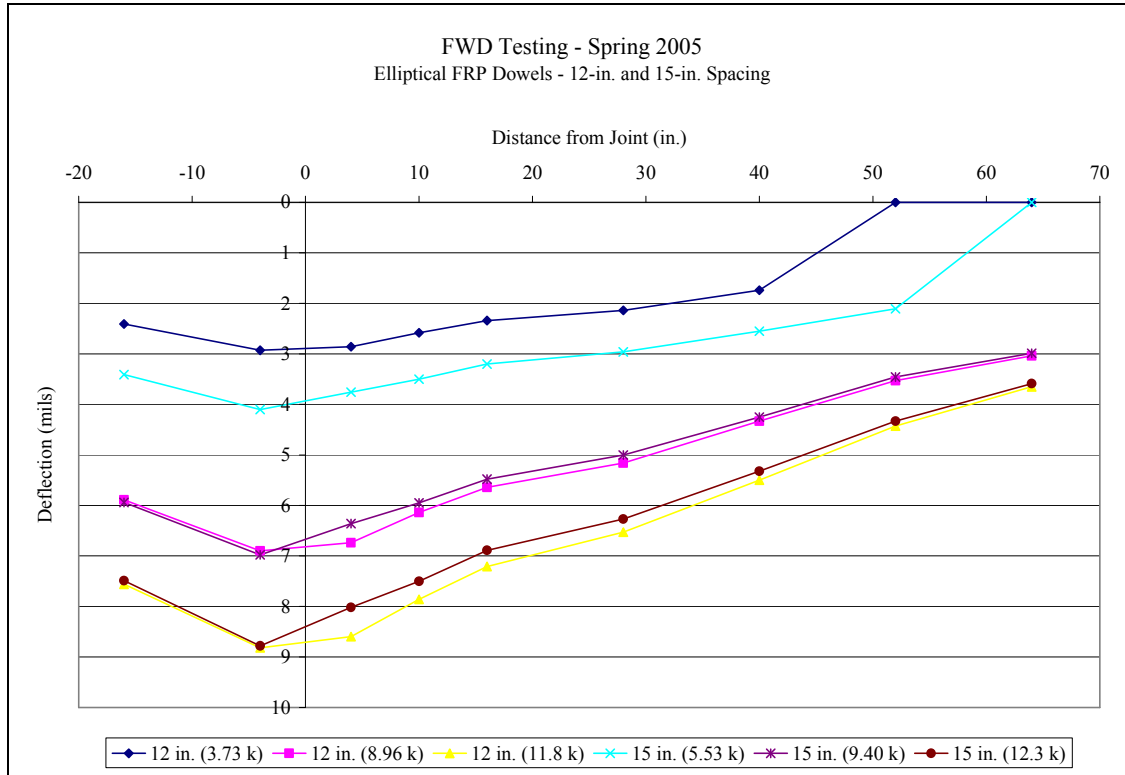


Figure A.4. Spring 2005 FWD testing: elliptical FRP

APPENDIX B. FAULTING DATA FOR FRP

In Table B.1, all tests were taken in the northbound (south) lane; tests were taken in the wheelpath four feet from the pavement edge in the driving lane and two feet from the pavement edge in the passing lane; the Georgia faultmeter was used for measurements; temperatures are measured in degrees Fahrenheit; and all dowels are manufactured by Hughes Brothers.

Table B.1. Elliptical FRP dowels: faulting field measurements

Test Sect.	Station (Metric)	Bar Size	Spacing (inches)	Faulting Measurements (mm)											
				4/5/2003			10/25/2003			4/10/2004			4/23/2005		
				Driving	Passing	Temp.	Driving	Passing	Temp.	Driving	Passing	Temp.	Driving	Passing	Temp.
EOP	1486+56 .225														
3	1371+09	1.33" x 2.25"	10	-0.6	0.0	35	-1.1	0.1	28.9	-0.1	-1.0	33	0.7	0.1	36
	1371+15	1.33" x 2.25"	10	-0.2	0.0	35	-0.2	-0.3	28.9	-0.7	-0.7	33	0.7	-0.6	36
	1371+21	1.33" x 2.25"	10	-0.5	-0.7	35	-0.3	0.2	28.9	-1.0	-1.5	33	0.3	1.2	36
	1371+27	1.33" x 2.25"	10	0.4	-0.3	35	-0.5	-0.3	28.9	0.0	-1.7	33	0.3	-0.1	36
	1371+33	1.33" x 2.25"	10	-0.3	0.5	35	-1.4	0.0	28.9	-0.2	-0.7	33	0.9	-0.1	36
	1371+39	1.33" x 2.25"	10	-0.5	-1.0	35	0.2	0.2	28.9	-0.8	-0.6	33	0.2	0.0	36
	1371+45	1.33" x 2.25"	10	-0.6	-0.3	35	-1.0	-0.1	28.9	-0.7	-0.2	33	0.1	0.5	36
	1371+51	1.33" x 2.25"	10	-1.3	-0.5	35	-1.4	0.0	28.9	-0.8	-0.7	33	0.1	0.5	36
	1371+57	1.33" x 2.25"	10	-0.8	0.5	35	-1.2	-0.4	28.9	-0.2	-0.3	33	1.0	-0.4	36
	1371+63	1.33" x 2.25"	10	-0.5	-0.8	35	-0.8	0.1	28.9	0.6	-1.6	33	1.0	0.0	36
2	1371+69	1.33" x 2.25"	12	-1.5	-0.3	35	-0.4	0.5	28.9	N/A	N/A	33	1.1	1.7	36
	1371+75	1.33" x 2.25"	12	-0.3	-0.2	35	0.1	0.5	28.9	-0.1	0.0	33	0.8	-0.7	36
	1371+81	1.33" x 2.25"	12	-0.8	0.0	35	-1.4	1.0	28.9	-0.1	-0.2	33	0.9	0.7	36
	1371+87	1.33" x 2.25"	12	-0.2	-0.5	35	-0.7	0.2	28.9	-1.0	-0.7	33	0.1	-0.3	36
	1371+93	1.33" x 2.25"	12	-1.0	-0.4	35	0.1	0.4	28.9	-0.1	-1.5	33	0.3	0.6	36
	1371+99	1.33" x 2.25"	12	-0.2	0.2	35	0.1	0.2	28.9	-0.2	-1.4	33	0.4	0.7	36
	1372+05	1.33" x 2.25"	12	-0.6	-0.7	35	-1.2	0.0	28.9	-0.1	-1.2	33	0.1	0.4	36
	1372+11	1.33" x 2.25"	12	-0.8	-0.8	35	-0.3	-0.5	28.9	-0.3	-0.8	33	0.4	0.5	36
	1372+17	1.33" x 2.25"	12	-0.4	0.4	35	-0.4	-0.2	28.9	-0.7	-0.5	33	0.3	0.7	36
	1372+23	1.33" x 2.25"	12	0.0	0.0	35	-1.2	0.2	28.9	-0.8	-1.5	33	0.3	-0.1	36
1	1372+29	1.33" x 2.25"	15	-0.3	-0.3	35	-1.3	0.3	28.9	-1.0	-1.4	33	0.2	-0.4	36
	1372+35	1.33" x 2.25"	15	-0.3	-0.3	35	-1.0	-0.3	28.9	-0.3	-1.2	33	0.6	-0.3	36
	1372+41	1.33" x 2.25"	15	0.4	-0.7	35	-0.9	0.3	28.9	-0.1	-0.8	33	0.0	0.1	36
	1372+47	1.33" x 2.25"	15	-0.5	0.1	35	-0.7	1.0	28.9	-0.7	-1.4	33	0.2	0.5	36
	1372+53	1.33" x 2.25"	15	0.5	-0.6	35	-0.5	0.2	28.9	0.3	-1.4	33	1.2	-0.4	36
	1372+59	1.33" x 2.25"	15	-0.3	0.0	35	-1.4	-0.4	28.9	-0.9	-0.7	33	0.4	-0.4	36
	1372+65	1.33" x 2.25"	15	-0.8	-0.7	35	-1.2	0.9	28.9	-0.4	-1.2	33	0.3	0.7	36
	1372+71	1.33" x 2.25"	15	-0.3	0.5	35	-1.2	-0.3	28.9	-0.1	-0.7	33	0.3	0.5	36
	1372+77	1.33" x 2.25"	15	-0.2	-0.2	35	-0.5	1.1	28.9	-0.6	-1.4	33	-0.5	-0.5	36
	1372+83	1.33" x 2.25"	15	-0.6	-0.3	35	-1.2	0.3	28.9	-1.4	-1.4	33	0.8	-0.8	36
BOP	1360+00														

Table B.2. FRP elliptical dowels: faulting averages

Test Date	Faulting Averages (mm)								
	10-in. spacing			12-in. spacing			15-in. spacing		
	Driving	Passing	Average	Driving	Passing	Average	Driving	Passing	Average
Spring 2003	-0.5	-0.3	-0.4	-0.6	-0.2	-0.4	-0.2	-0.3	-0.2
Fall 2003	-0.8	-0.1	-0.4	-0.5	0.2	-0.2	-1.0	0.3	-0.3
Spring 2004	-0.4	-0.9	-0.6	-0.4	-0.9	-0.6	-0.5	-1.2	-0.8
Spring 2005	0.5	0.1	0.3	0.5	0.4	0.4	0.4	-0.1	0.1

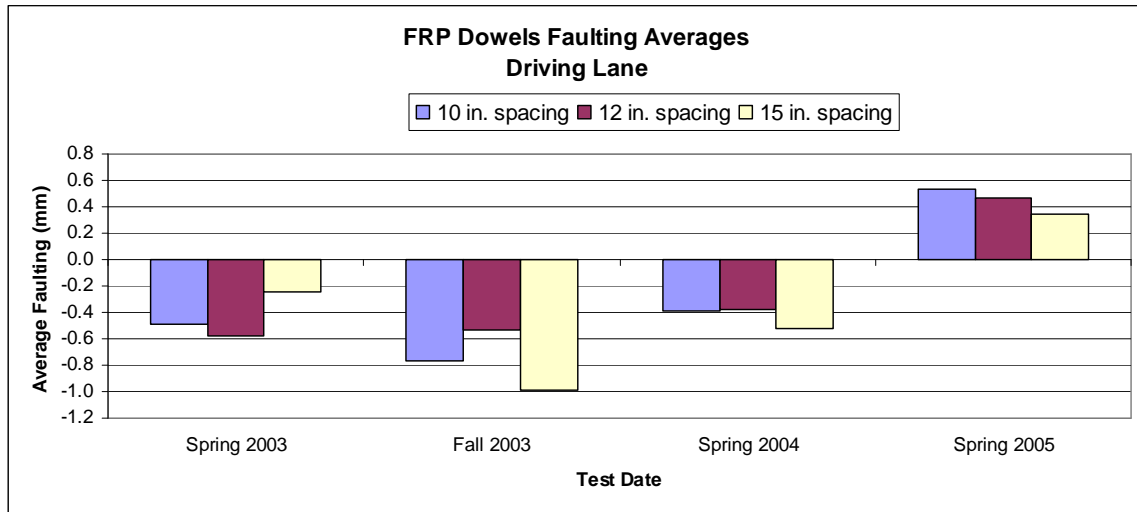


Figure B.1. Faulting: FRP dowels, driving lane

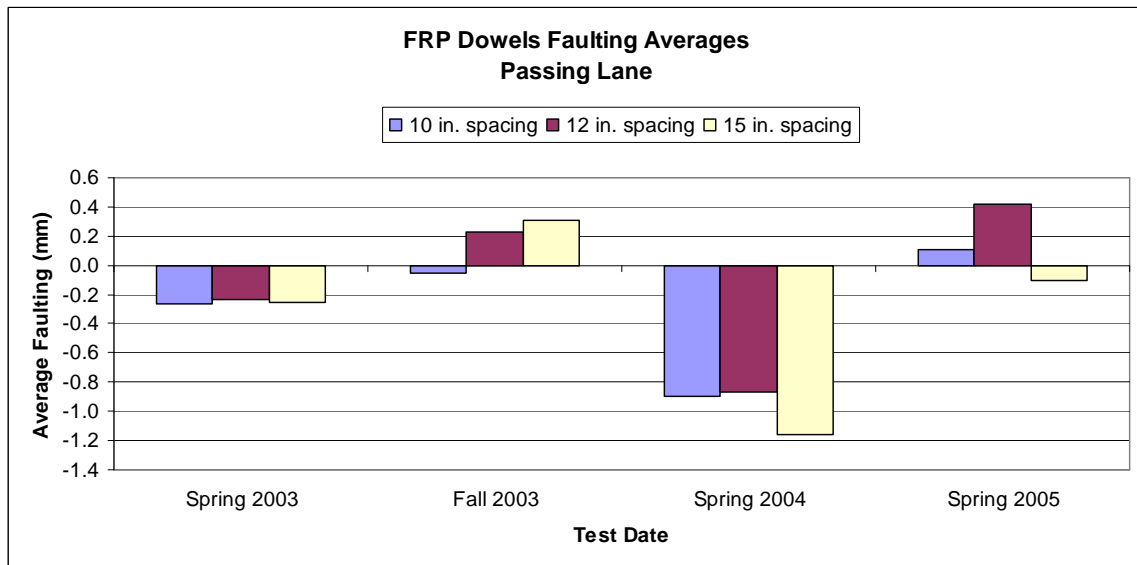


Figure B.2. Faulting: FRP dowels, passing lane

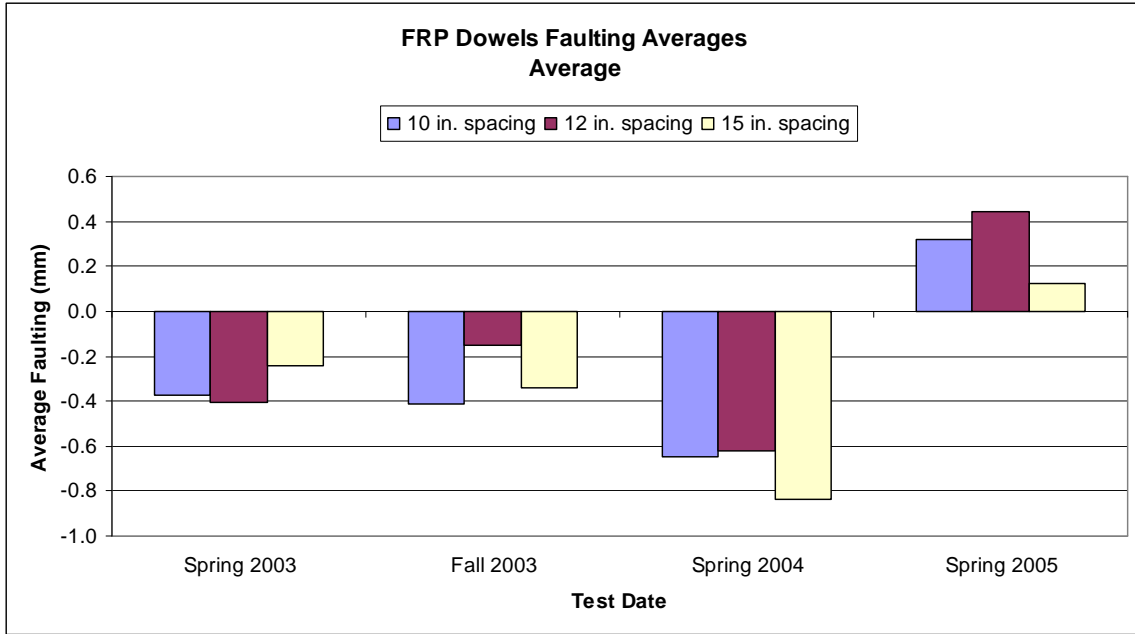


Figure B.3. Faulting: FRP dowels, averages

APPENDIX C. JOINT OPENING DATA FOR FRP

In Table C.1, note that a negative (-) value for "Change in Joint Opening" indicates joint expansion. A positive (+) value for "Change in Joint Opening" indicates joint contraction.

Table C.1. FRP elliptical dowels: joint opening field measurements

Test Sect.	Station (Metric)	Bar Shape	Bar Size	Spacing (inches)	Joint Opening Measurements (mm)				Change in Joint Opening (mm)		
					8/28/2002 (35° F)	9/21/2002 (35° F)	10/1/2002 (35° F)	4/23/2005 (34.5° F)	9/21/2002 (35° F)	10/1/2002 (35° F)	4/23/2005 (34.5° F)
EOP	1486+56.225										
3	1371+09	Elliptical	1.33" x 2.25"	10	264	264	264	266	0.3	0.3	2.4
	1371+15	Elliptical	1.33" x 2.25"	10	246	246	246	247	-0.2	-0.1	1.1
	1371+21	Elliptical	1.33" x 2.25"	10	249	249	250	250	-0.2	0.6	0.9
	1371+27	Elliptical	1.33" x 2.25"	10	249	248	248	249	-0.3	-0.2	0.3
	1371+33	Elliptical	1.33" x 2.25"	10	250	250	251	251	0.1	0.6	1.0
	1371+39	Elliptical	1.33" x 2.25"	10	257	257	257	257	0.0	0.0	0.1
	1371+45	Elliptical	1.33" x 2.25"	10	252	252	252	253	-0.2	0.0	0.7
	1371+51	Elliptical	1.33" x 2.25"	10	253	253	253	253	-0.3	-0.2	-0.3
	1371+57	Elliptical	1.33" x 2.25"	10	252	252	253	253	-0.2	0.2	0.7
1371+63	Elliptical	1.33" x 2.25"	10	249	249	250	250	0.1	0.8	1.1	
2	1371+69	Elliptical	1.33" x 2.25"	12	268	268	268	269	0.0	-0.1	0.9
	1371+75	Elliptical	1.33" x 2.25"	12	260	260	260	261	-0.2	0.0	1.1
	1371+81	Elliptical	1.33" x 2.25"	12	249	249	249	250	-0.2	-0.3	0.8
	1371+87	Elliptical	1.33" x 2.25"	12	245	245	245	246	0.1	0.1	0.7
	1371+93	Elliptical	1.33" x 2.25"	12	256	257	256	257	0.3	0.2	0.8
	1371+99	Elliptical	1.33" x 2.25"	12	258	257	257	258	-0.2	-0.1	0.5
	1372+05	Elliptical	1.33" x 2.25"	12	255	255	255	256	-0.8	-0.5	0.5
	1372+11	Elliptical	1.33" x 2.25"	12	272	272	272	272	0.0	-0.2	-0.2
	1372+17	Elliptical	1.33" x 2.25"	12	256	256	257	256	0.1	0.6	-0.1
1372+23	Elliptical	1.33" x 2.25"	12	271	272	271	272	1.5	0.7	1.2	
1	1372+29	Elliptical	1.33" x 2.25"	15	255	255	255	No nails	0.6	0.1	
	1372+35	Elliptical	1.33" x 2.25"	15	263	262	262	263	-0.4	-0.6	0.2
	1372+41	Elliptical	1.33" x 2.25"	15	258	258	258	No nails	0.4	-0.4	
	1372+47	Elliptical	1.33" x 2.25"	15	248	248	248	249	0.0	0.1	1.2
	1372+53	Elliptical	1.33" x 2.25"	15	262	263	262	263	0.1	0.1	0.6
	1372+59	Elliptical	1.33" x 2.25"	15	263	263	262	264	0.3	-0.6	1.5
	1372+65	Elliptical	1.33" x 2.25"	15	260	260	260	261	0.1	0.3	1.5
	1372+71	Elliptical	1.33" x 2.25"	15	262	262	262	263	-0.2	0.1	1.3
	1372+77	Elliptical	1.33" x 2.25"	15	290	291	291	291	0.3	0.3	0.7
1372+83	Elliptical	1.33" x 2.25"	15	275	275	275	277	0.1	0.2	1.9	
BOP	1360+00										

Also note that for the data in Table C.1, all tests were taken in the northbound (south) lane; measurements were made between nails installed 12 inches from the edge of pavement; temperatures are measured in degrees Fahrenheit; and all dowels are manufactured by Hughes Brothers.

Table C.2. FRP elliptical dowels: change in joint opening averages

Bar Type	Spacing (inches)	Change in Joint Opening Averages (mm)	
		Fall 2002	Spring 2005
FRP-Elliptical	10	0.20	0.80
FRP-Elliptical	12	0.05	0.62
FRP-Elliptical	15	-0.05	1.10

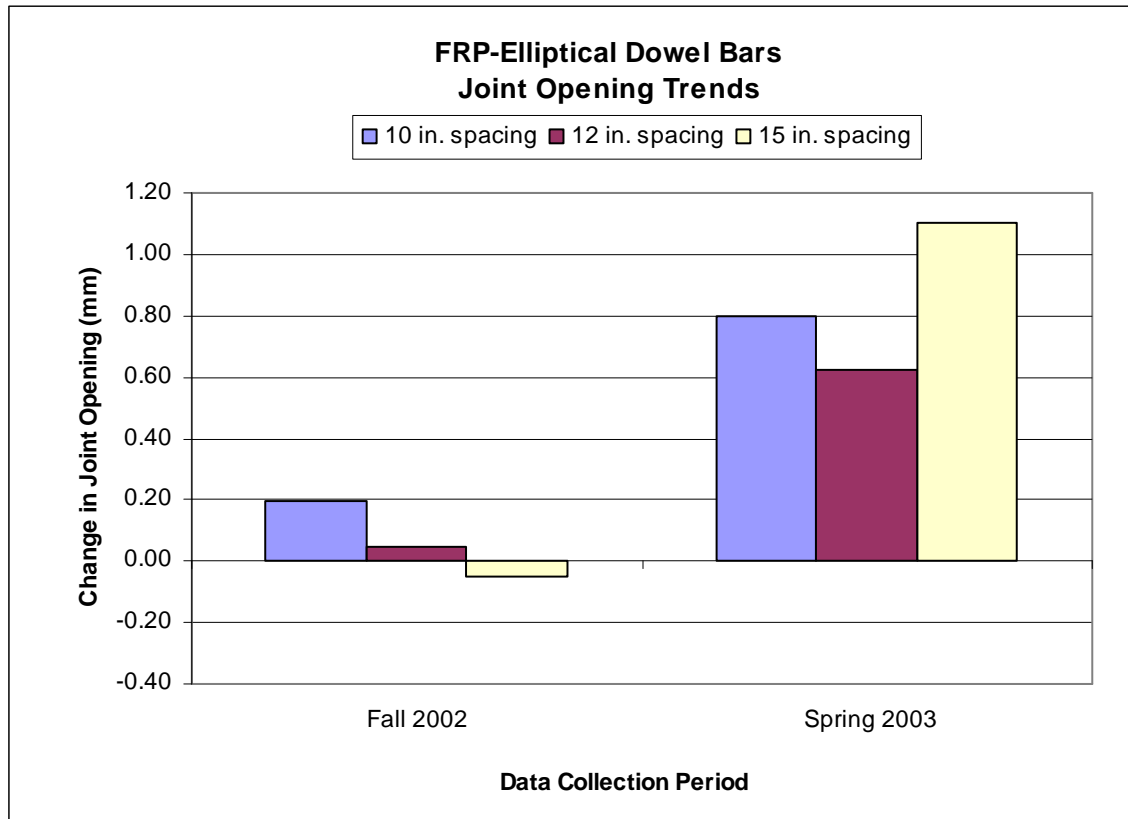


Figure C.1. Joint Opening - FRP Dowels

APPENDIX D. FALLING WEIGHT DEFLECTOMETER DATA FOR STEEL

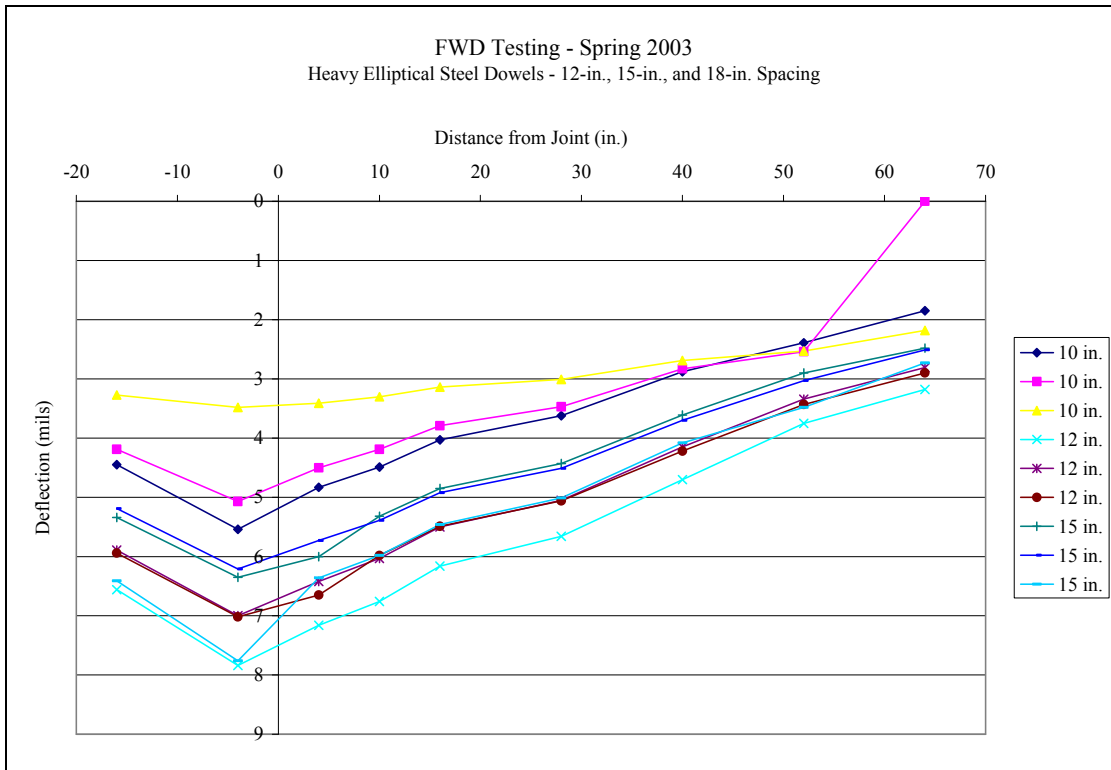


Figure D.1. Spring 2003 FWD testing: heavy elliptical steel

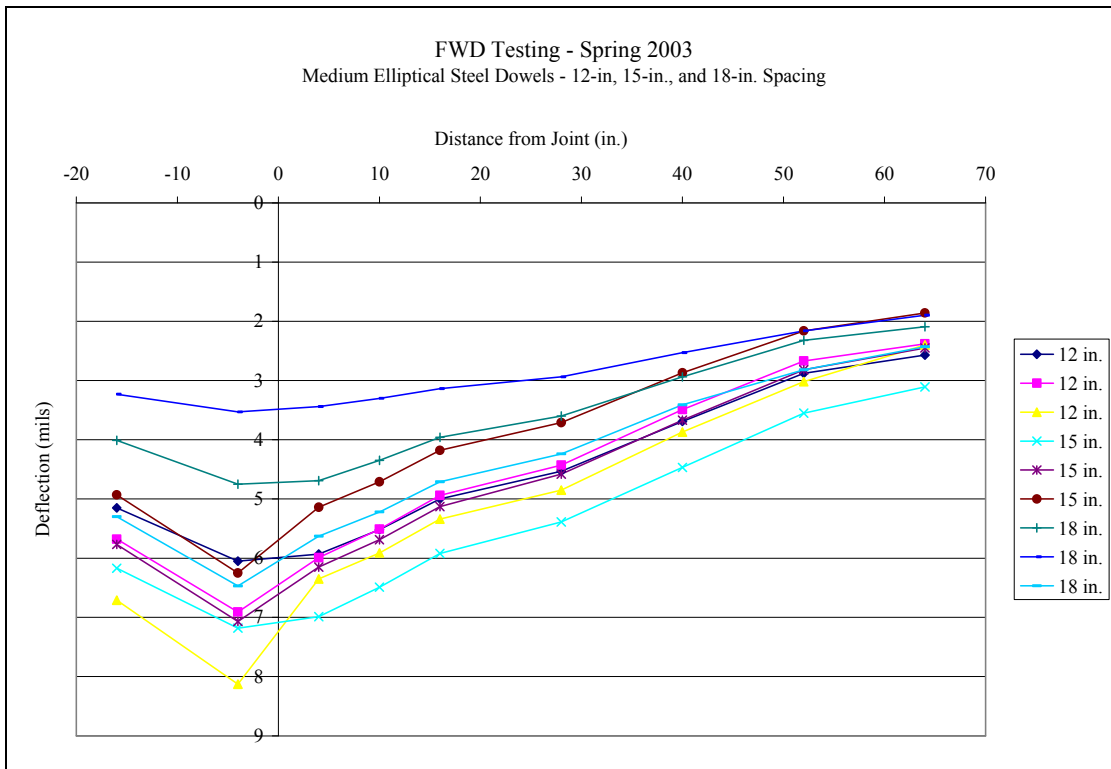


Figure D.2. Spring 2003 FWD testing: medium elliptical steel

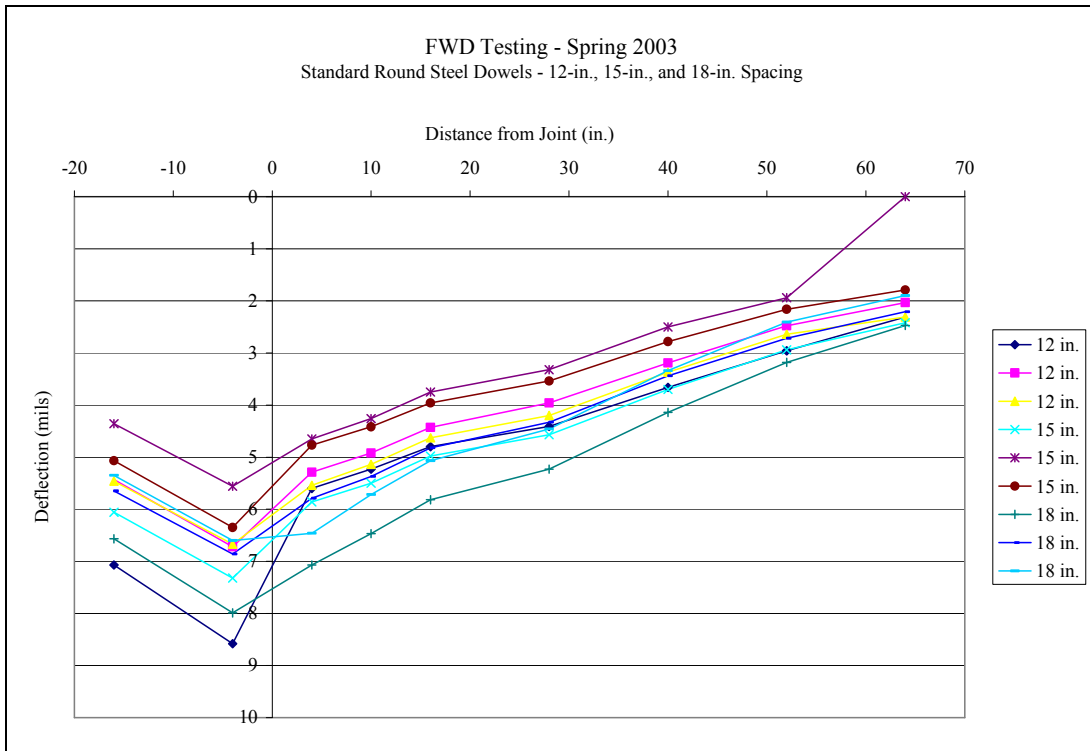


Figure D.3. Spring 2003 FWD testing: standard round steel

Figures D.4 to D.6 illustrate the average modulus of dowel support, k_0 , for the heavy elliptical, medium elliptical, and standard round steel dowels at various dowel spacings.

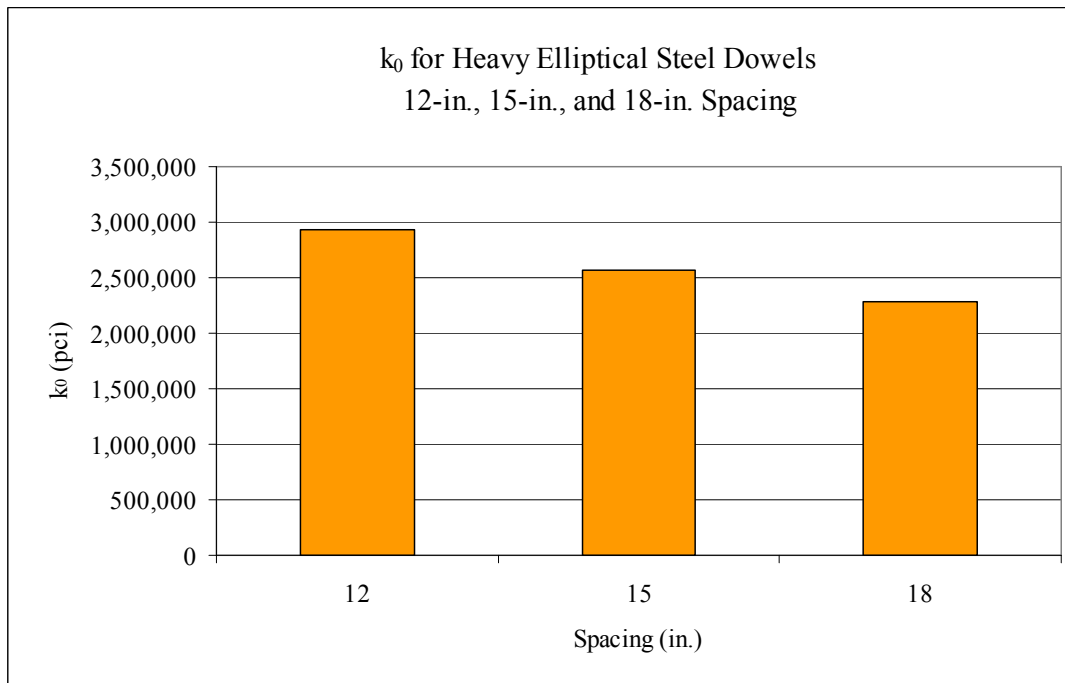


Figure D.4. Average k_0 for heavy elliptical steel dowels

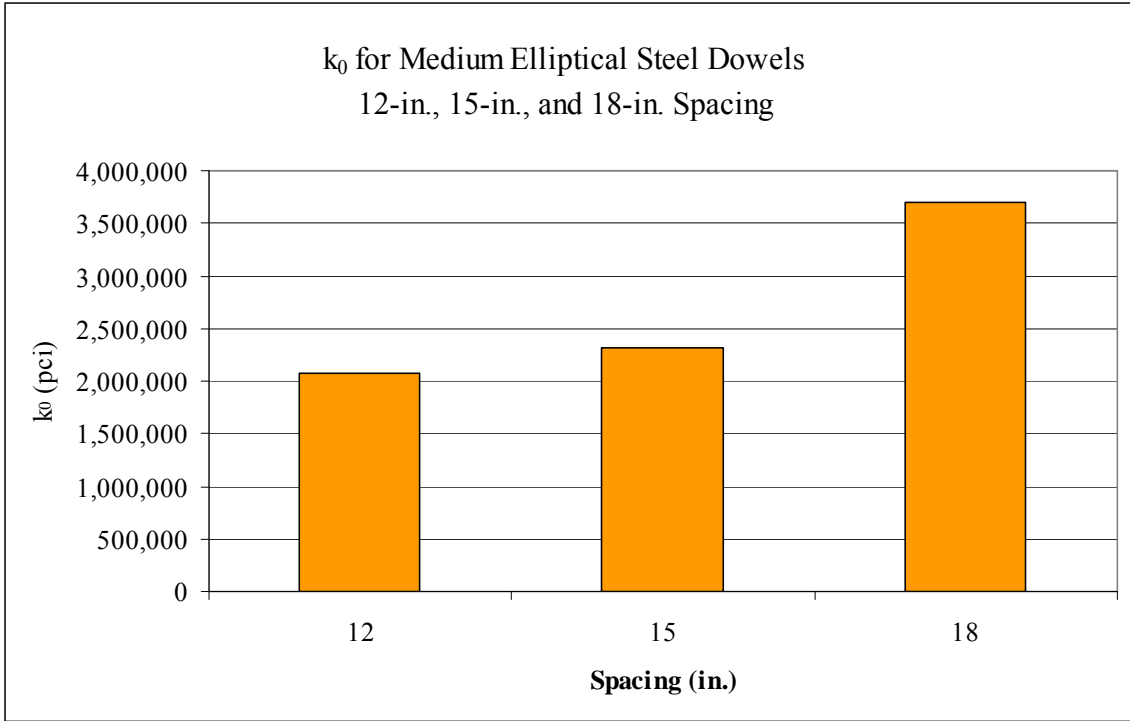


Figure D.5. Average k_0 for medium elliptical steel dowels

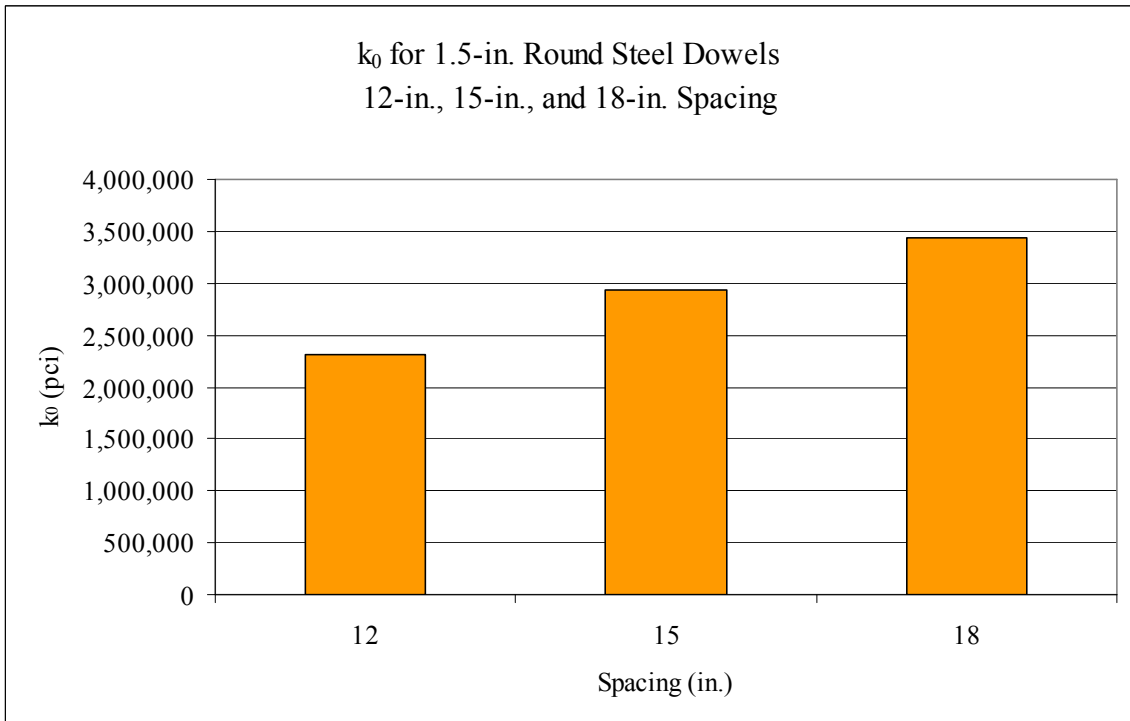


Figure D.6. Average k_0 for standard round steel dowels

APPENDIX E. STRAIN GAGE RESULTS FOR STEEL

Figures E.1 to E.3 show the estimated deflected shape from strain gage data for heavy elliptical steel dowels (major axis is 1.969 inches and minor axis is 1.338 inches) for 12-, 15-, and 18-inch spacing.

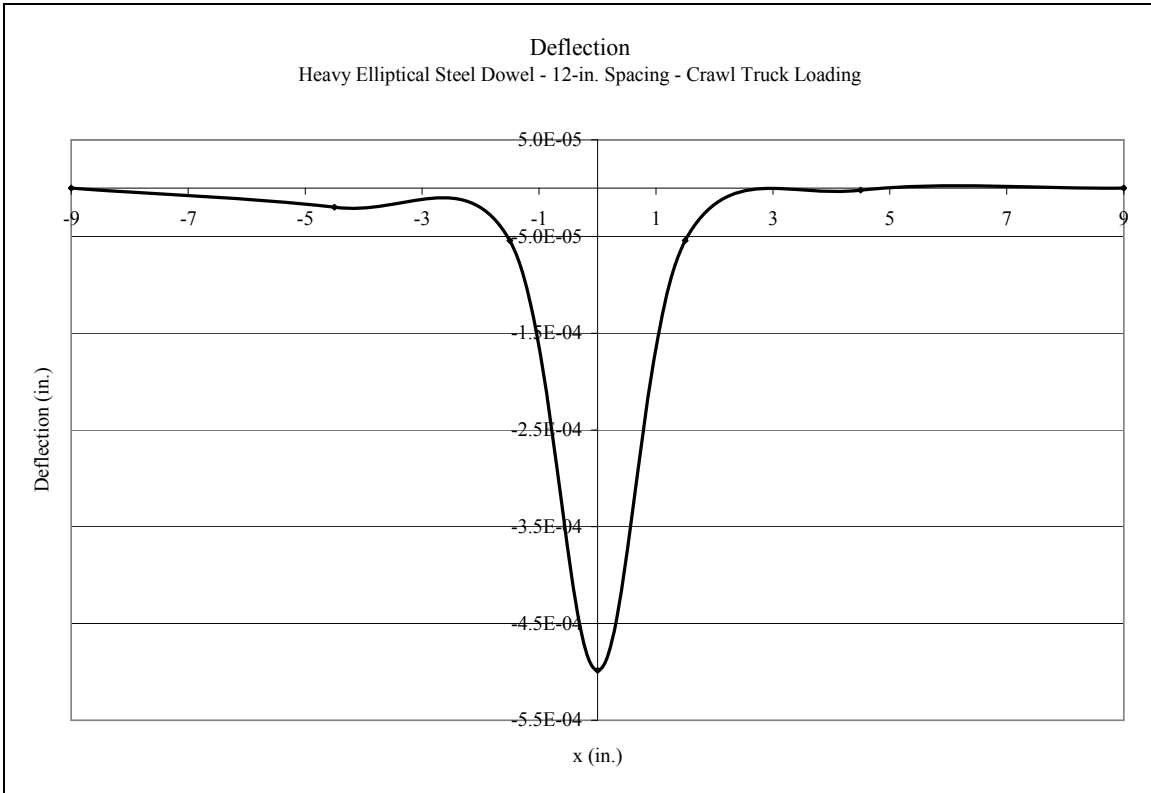


Figure E.1. Deflection of heavy elliptical steel dowel, 12-in. spacing

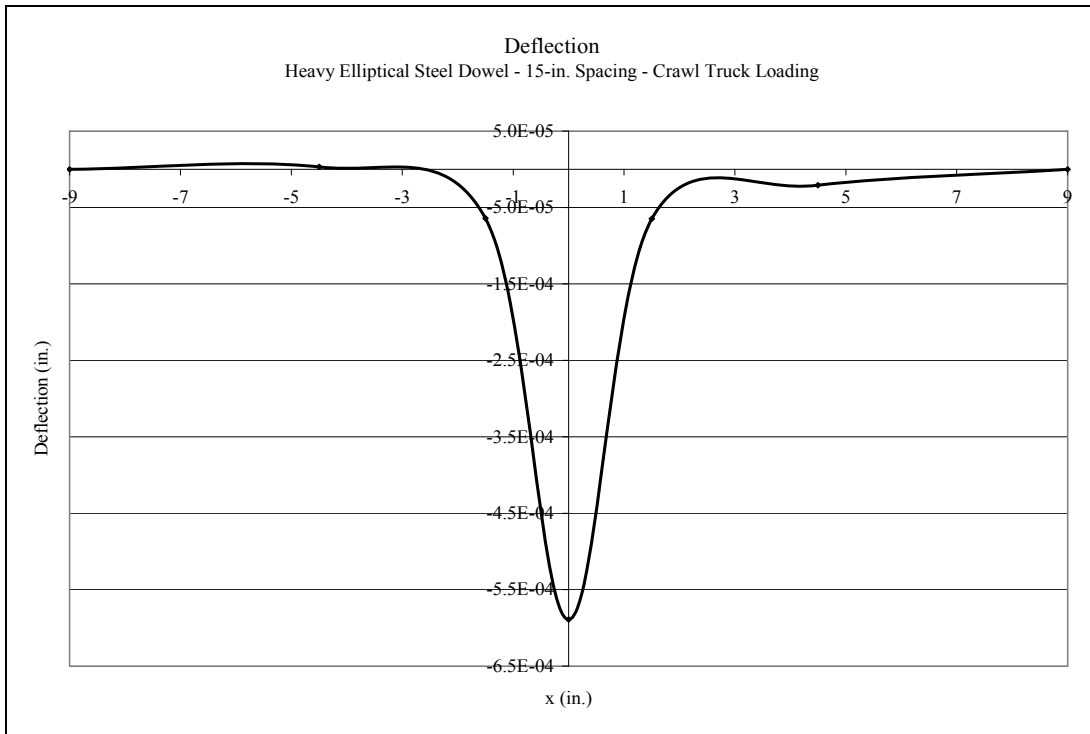


Figure E.2. Deflection of heavy elliptical steel dowel, 15-in. spacing

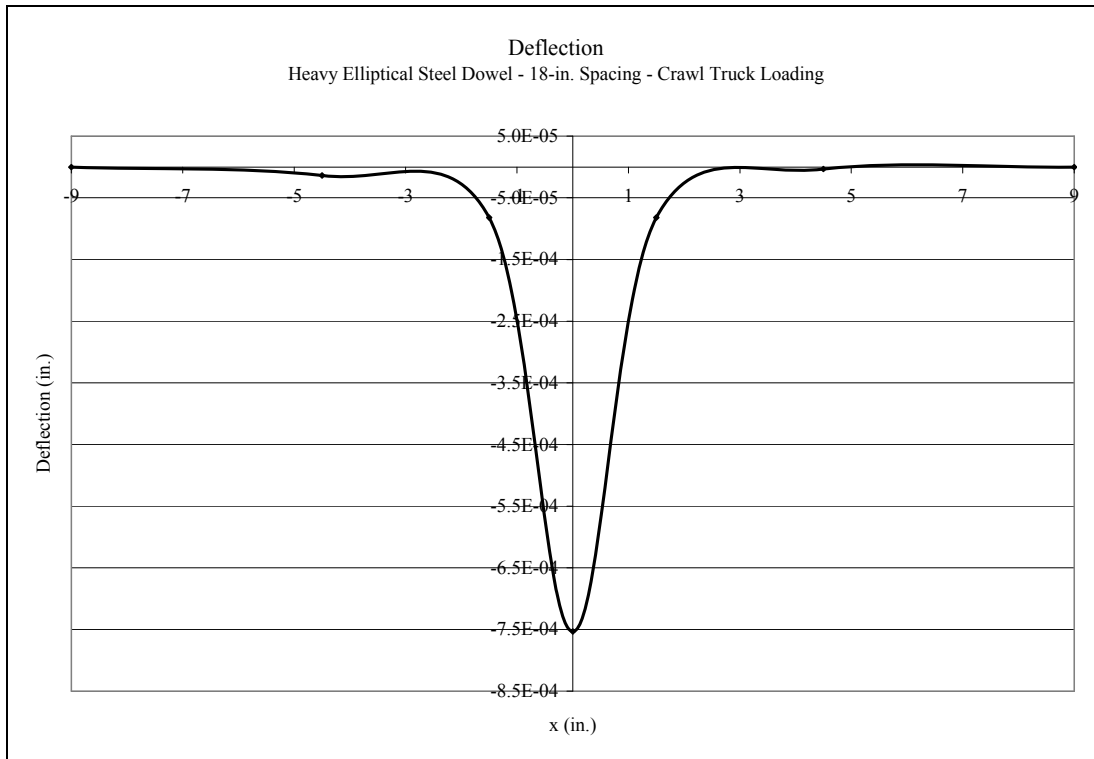


Figure E.3. Deflection of heavy elliptical steel dowel, 18-in. spacing

APPENDIX F. FAULTING DATA FOR STEEL

Table F.1. Steel dowels, faulting field measurements

Notes:
 1. All tests were taken in the northbound (south) lane.
 2. Tests were taken in the wheelpath; 4 ft from the edge of pavement in the driving lane and 2 ft from the edge of pavement in the passing lane.
 3. Georgia Faultmeter was used. For all measurements.
 4. Temperatures are measured in Degrees Fahrenheit.

Test Sect. Station Ref. EOP	Station Offset	Bar Shape	Bar Size	Spacing Inches	Faulting Measurements (mm)															
					9/21/2002		4/5/2003		10/25/2003		4/22/2004		4/22/2005							
					Driving	Passing	Temp.	Driving	Passing	Temp.	Driving	Passing	Temp.	Driving	Passing	Temp.				
128 1346+20	1345+89	Elliptical	Medium	18	-0.4	-0.3	0.0	0.0	32	0.2	0.9	27.1	0.1	-1.3	33	0.7	68	0.8	0.3	40
	1345+93	Elliptical	Medium	18	0.5	-0.5	-0.1	0.1	32	-1.4	1.1	27.1	-1.1	-1.3	33	-0.6	68	0.5	0.7	40
	1345+97	Elliptical	Medium	18	-0.2	0.4	0.0	0.4	32	-1.5	1.0	27.1	-1.0	-1.2	33	0.0	68	0.0	1.5	40
	1345+71	Elliptical	Medium	18	-0.3	0.1	-0.3	0.0	32	-1.4	0.9	27.1	-1.2	-2.0	33	-0.5	68	-0.5	1.0	40
	1345+65	Elliptical	Medium	18	-1.3	-0.3	0.0	-0.3	32	-1.4	0.3	27.1	-0.3	-1.3	33	0.5	68	0.4	0.7	40
	1345+59	Elliptical	Medium	18	-1	-0.8	-0.2	-1.2	32	-1.6	1.0	27.1	-0.6	-1.5	33	0.6	68	0.6	1.0	40
	1345+53	Elliptical	Medium	18	-1	-0.2	-0.3	-0.4	32	-1.6	-0.2	27.1	-0.6	-0.6	33	0.5	68	0.5	0.0	40
	1344+47	Elliptical	Medium	18	-0.2	-0.3	-0.7	-0.2	32	-0.1	1.0	27.1	0.0	-1.8	33	-0.3	68	-0.3	0.4	40
	1345+41	Elliptical	Medium	18	-0.8	-0.1	-0.5	-0.3	32	-0.1	1.0	27.1	-1.1	-1.3	33	0.5	68	-0.3	0.4	40
	1345+35	Elliptical	Medium	18	0	-0.3	-0.5	-0.3	32	-1.2	0.2	27.1	-0.2	-1.5	33	0.8	68	0.2	0.6	40
126 1344+70	1344+40	Elliptical	Medium	18	0.1	0.5	0.6	0.5	32	-1.4	-0.5	27.1	-0.1	-0.6	33	0.1	68	0.6	0.8	40
	1344+34	Elliptical	Medium	18	0.2	0	-0.3	-0.1	32	-0.9	0.1	27.1	-1.0	-0.9	33	0.7	68	0.6	0.1	40
	1344+28	Elliptical	Medium	18	-0.9	-0.2	-0.5	-1.4	32	-0.6	-0.1	27.1	-0.1	-0.9	33	0.2	68	0.1	0.2	40
	1344+22	Elliptical	Medium	18	0.3	0.4	0.3	0.4	32	-0.2	0.0	27.1	-0.5	0.0	33	0	68	0.1	0.4	40
	1344+16	Elliptical	Medium	18	-0.5	-0.4	-0.7	-0.1	32	-1.1	0.5	27.1	-1.0	-0.6	33	0.5	68	-0.2	1.3	40
	1344+10	Elliptical	Medium	18	-0.7	0	-0.2	-0.1	32	-0.9	0.9	27.1	-1.0	-0.6	33	0.7	68	0.5	0.7	40
	1344+04	Elliptical	Medium	18	-0.5	-0.4	0.3	-0.2	32	0.5	-0.1	27.1	-0.8	-0.1	33	0.7	68	0.6	0.1	40
	1343+98	Elliptical	Medium	18	-1	-0.3	0.0	-0.3	32	-1.2	0.9	27.1	-1.0	-0.6	33	0.2	68	0.5	0.1	40
	1343+92	Elliptical	Medium	18	-0.9	0.3	-0.5	-0.3	32	-0.8	0.2	27.1	-1.0	-0.6	33	0.5	68	0.4	0.9	40
	1343+86	Elliptical	Medium	18	-0.2	0.1	-0.4	-0.7	32	-0.9	0.1	27.1	-0.5	-1.4	33	-0.6	68	0.6	0.2	40
124 1340+20	1339+90	Elliptical	Medium	18	-1.9	-1	0.2	-1.3	44	1.0	0.2	25.5	-0.8	-0.5	33	0	69	2.8	0.5	40
	1339+84	Elliptical	Medium	18	0.5	-0.8	-0.4	-1.9	44	-0.2	0.9	25.5	-1.1	-0.7	33	0.7	69	0	1.2	40
	1339+78	Elliptical	Medium	18	-0.3	0	-0.5	0.3	44	-1.0	0.7	25.5	-0.1	-0.5	33	-0.8	69	-0.2	1.6	40
	1339+72	Elliptical	Medium	18	-0.5	-0.3	-0.6	-0.1	44	-1.4	0.4	25.5	-0.1	-1.8	33	-0.3	69	-0.1	0.5	40
	1339+66	Elliptical	Medium	18	-0.8	-0.5	0.0	0.0	44	-0.9	0.9	25.5	-0.6	-1.4	33	-0.8	69	0.7	0.0	40
	1339+60	Elliptical	Medium	18	-0.1	0	0.2	-0.4	44	-0.6	0.0	25.5	-0.2	-1.5	33	-0.9	69	-0.3	1.0	40
	1339+54	Elliptical	Medium	18	0	-0.6	-0.1	-0.4	44	-1.0	0.2	25.5	-1.0	-1.3	33	-0.6	69	0.5	1.2	40
	1339+48	Elliptical	Medium	18	0.5	0	-0.5	-0.3	44	-1.4	0.0	25.5	-0.3	-1.5	33	-0.7	69	-0.4	0.1	40
	1339+42	Elliptical	Medium	18	0.3	-0.6	-0.3	0.9	44	-0.7	0.9	25.5	0.6	-0.8	33	-0.4	69	-0.3	0.5	40
	1339+36	Elliptical	Medium	18	0.4	0.2	-0.2	-0.5	44	-0.4	0.2	25.5	-0.7	-0.6	33	0	69	0.6	0.2	40
122 1333+70	1333+36	Elliptical	Medium	15	-0.4	-0.6	-1.0	0.1	44	0.2	0.5	25.5	-1.1	0.3	33	0.7	69	-0.3	0.7	40
	1333+30	Elliptical	Medium	15	-0.3	-0.6	-0.4	0.2	44	-0.2	0.0	25.5	-2.2	0.0	33	0	69	1.7	0.3	40
	1333+24	Elliptical	Medium	15	-0.5	-0.4	-0.5	0.7	44	-1.4	-0.5	25.5	-1.5	-0.2	33	-0.9	69	0.4	0.4	40
	1333+18	Elliptical	Medium	15	0.6	0	-0.8	0.0	44	-0.6	-0.1	25.5	0.3	-1.5	33	-0.9	69	0.0	1.5	40
	1333+12	Elliptical	Medium	15	-0.6	-0.3	-1.3	-1.0	44	-1.3	-0.1	25.5	-1.3	-1.8	33	-0.6	69	0.7	1.0	40
	1333+06	Elliptical	Medium	15	-0.6	-0.3	-1.1	-1.0	44	-1.4	1.0	25.5	-0.1	-1.3	33	-0.7	69	1.2	0.6	40
	1333+00	Elliptical	Medium	15	0	0.5	0.2	-0.8	44	-1.2	-0.4	25.5	-0.1	-1.6	33	-0.1	69	0.7	0.6	40
	1332+94	Elliptical	Medium	15	-0.7	-0.3	-0.7	-0.5	44	-0.4	-0.2	25.5	-0.6	-0.6	33	1	69	0.5	-0.1	40
	1332+88	Elliptical	Medium	15	-0.8	-0.3	-0.8	0.0	44	-1.2	-0.1	25.5	-0.4	-1.1	33	0.1	69	-0.6	-0.6	40
	1332+82	Elliptical	Medium	15	-0.7	0.7	0.3	0.1	44	-1.5	0.2	25.5	-0.1	-1.8	33	-0.2	69	-0.6	0.1	40
120 1332+20	1331+84	Elliptical	Medium	15	-1	0.2	0.0	-0.2	38	-0.4	0.3	26.8	-0.3	-0.5	33	0.1	70	1.2	0.8	40
	1331+78	Elliptical	Medium	15	-0.3	0.2	0.2	-0.6	38	-1.0	0.9	26.8	-0.4	-1.0	33	0.2	70	0.5	0.1	40
	1331+72	Elliptical	Medium	15	-1.3	0.6	-0.9	-1.1	38	-0.9	0.3	26.8	-0.7	-1.3	33	-0.9	70	0.7	0.0	40
	1331+66	Elliptical	Medium	15	-0.4	0.1	-0.5	-0.6	38	-0.1	0.1	26.8	0.4	-1.1	33	0.3	70	0.5	1.3	40
	1331+60	Elliptical	Medium	15	-0.4	-0.2	-1.1	-0.6	38	-0.1	0.2	26.8	-0.3	-1.3	33	0.8	70	1.2	0.1	40
	1331+54	Elliptical	Medium	15	-0.5	-0.5	-1.5	-0.3	38	-1.0	0.1	26.8	0.2	-0.7	33	0.5	70	0.5	0.6	40
	1331+48	Elliptical	Medium	15	-0.2	0	-0.3	-0.5	38	0.3	1.0	26.8	0.2	-0.1	33	0.3	70	1.2	0.9	40
	1331+42	Elliptical	Medium	15	-0.5	-0.5	-0.3	-0.8	38	-0.1	1.5	26.8	-0.5	0.0	33	0.1	70	0.6	2.1	40
	1331+36	Elliptical	Medium	15	-0.1	-0.3	0.5	-0.8	38	-0.1	0.3	26.8	-0.9	-1.5	33	0.8	70	0.4	1.3	40
	1331+30	Elliptical	Medium	15	-1.2	0.1	-0.2	-0.2	38	-1.0	0.9	26.8	0.0	-0.1	33	0.4	70	0.6	0.1	40
118 1328+20	1327+88	Standard	Round	12	-0.7	-0.5	-0.2	0.7	38	-0.5	0.4	26.8	-0.9	-1.3	33	0	70	-0.5	0.0	40
	1327+82	Standard	Round	12	0.5	-1	0.2	0.2	38	-0.6	0.0	26.8	-0.1	0.0	33	0.7	70	1.2	1.0	40
	1327+76	Standard	Round	12	0.6	-0.2	-1.2	-0.2	38	-0.6	0.8	26.8	-0.2	-1.0	33	0	70	-0.3	1.0	40
	1327+70	Standard	Round	12	-0.5	-0.2	-1.2	-0.2	38	-1.2	0.8	26.8	0.5	-1.3	33	0.2	70	0.5	1.0	40
	1327+64	Standard	Round	12	0	-0.1	0.0	0.0	38	-0.2	-0.1	26.8	-0.1	-0.5	33	0.7	70	0.5	0.2	40
	1327+58	Standard	Round	12	-1.1	0	-0.2	-1.0	38	-1.4	0.0	26.8	-0.1	-0.7	33	-0.3	70	-0.3	0.3	40
	1327+52	Standard	Round	12	-0.3	-0.2	-0.5	-0.5	38	-0.1	0.8	26.8	-0.8	-0.6	33	0.7	70	1.0	1.5	40
	1327+46	Standard	Round	12	0.3	-0.7	0.0	0.1	38	-1.2	1.6	26.8	-0.5	-1.3	33	1	70	0.4	1.0	40
	1327+40	Standard	Round	12	-0.8	0	-0.1	0.5	38	-0.9	0.1	26.8	1.2	-1.6	33	0.5	70	-0.3	0.7	40
	1327+34	Standard	Round	12	-1.4	-0.6	-0.6	-0.1	38	-0.3	0.8	26.8	0.0	-0.1	33	1	70	-0.8	-0.5	-0.5

1320+89	15	Medium	Elliptical	0	-0.3	-0.2	41	-0.3	-0.3	26.8	-0.2	0.0	36	0.4	-0.4	70	0.6	1.4	40
1320+83	15	Medium	Elliptical	0	0.3	0.2	41	-0.6	0.2	26.8	-1.1	-0.7	36	0.2	0.2	70	0.6	0.1	40
1320+77	15	Medium	Elliptical	0.2	-0.2	0.0	41	-1.2	0.1	26.8	-0.7	-1.3	36	0.4	0.6	70	0.6	1.0	40
1320+71	15	Medium	Elliptical	-0.2	-0.7	-0.7	41	-0.8	1.6	26.8	-0.4	-0.4	36	0.4	-0.4	70	0.2	0.2	40
1320+65	15	Medium	Elliptical	-0.3	0.5	0.0	41	-0.5	1.2	26.8	-0.5	-1.3	36	1.4	-0.1	70	-0.3	1.3	40
1320+59	15	Medium	Elliptical	-1.4	0.0	0.0	41	-1.4	0.2	26.8	-0.8	-1.5	36	1	-0.2	70	-0.5	0.1	40
1320+53	15	Medium	Elliptical	0.6	0.0	-0.2	41	-0.5	0.0	26.8	-0.3	-1.6	36	0.2	0.5	70	0.1	0.1	40
1320+47	15	Medium	Elliptical	-0.3	0.1	0.1	41	-0.1	-0.1	26.8	-0.3	-0.3	36	-0.3	-0.1	70	-0.3	0.2	40
1320+41	15	Medium	Elliptical	0	-0.5	0.4	41	-1.1	0.5	26.8	-0.4	-1.5	36	0.4	-0.1	70	-0.2	1.1	40
1320+35	15	Medium	Elliptical	-0.7	-0.8	-0.8	41	-1.4	0.3	26.8	-0.8	-0.7	36	0.3	0.3	70	1.2	0.1	40
1319+38	12	Medium	Elliptical	0.4	0.0	-0.3	41	-1.3	0.0	26.8	-0.8	-0.5	36	1.1	-0.3	70	0.5	0.1	40
1319+32	12	Medium	Elliptical	-0.5	0.0	-0.9	41	0.1	-0.1	26.8	0.5	-0.5	36	1	-0.5	70	1.1	1.0	40
1319+26	12	Medium	Elliptical	-0.1	-0.5	0.2	41	-0.1	0.9	26.8	0.3	-1.8	36	0.5	0.7	70	1.2	0.8	40
1319+20	12	Medium	Elliptical	0.5	-0.2	-1.0	41	0.1	0.2	26.8	-0.3	-0.5	36	0.7	0.7	70	0.6	0.2	40
1319+14	12	Medium	Elliptical	0.3	0.3	-0.3	41	-0.6	0.3	26.8	-1.1	-1.6	36	-0.3	-0.8	70	0.5	1.0	40
1319+08	12	Medium	Elliptical	0	0.2	-0.2	41	-1.4	0.8	26.8	0.4	-0.7	36	0.5	-0.8	70	0.1	1.0	40
1319+02	12	Medium	Elliptical	-0.6	0.1	-0.3	41	0.0	1.6	26.8	0.4	0.0	36	1.3	0.4	70	1.2	0.1	40
1318+96	12	Medium	Elliptical	-0.5	-0.2	-1.2	41	0.3	0.5	26.8	-0.3	-0.6	36	1.5	-0.6	70	0.2	1.4	40
1318+90	12	Medium	Elliptical	-1	0.5	-0.3	41	-0.1	-0.2	26.8	-1.0	-0.1	36	1	-0.8	70	0.6	1.0	40
1318+84	12	Medium	Elliptical	-0.4	-1.3	-0.7	41	-1.7	0.1	26.8	-0.5	-0.7	36	1	-0.8	70	1.2	0.3	40
1317+78	12	Medium	Elliptical	0.2	-0.5	-0.5	40	-0.5	1.6	28	-0.4	-2.0	37	0.3	1.1	69	-0.3	1.0	40
1317+71	12	Medium	Elliptical	-0.8	-0.3	0.0	40	-0.5	0.2	28	-0.8	-0.6	37	0.4	0.7	69	0.5	0.1	40
1317+65	12	Medium	Elliptical	-0.5	-0.3	0.0	40	-1.4	0.4	28	-1.0	-1.7	37	0.6	-0.3	69	-0.3	0.2	40
1317+59	12	Medium	Elliptical	0.2	-0.8	-0.5	40	-0.1	0.3	28	-0.4	0.0	37	-0.6	1	69	0.6	0.7	40
1317+53	12	Medium	Elliptical	-0.1	0.1	-0.4	40	0.8	0.2	28	-0.5	-2.0	37	1	-0.3	69	0.9	0.1	40
1317+47	12	Medium	Elliptical	-0.9	-1.1	-0.3	40	0.3	0.9	28	-0.4	-2.0	37	-0.4	1.1	69	1.2	0.9	40
1317+41	12	Medium	Elliptical	-0.5	-1.0	-1.6	40	-0.1	1.2	28	1.0	-0.7	37	0	69	1.2	0.4	40	
1317+35	12	Medium	Elliptical	0.2	-0.8	-0.9	40	-0.8	0.9	28	0.3	-0.9	37	0.2	0.8	69	0.5	0.5	40
1317+29	12	Medium	Elliptical	0.3	-0.3	-0.3	40	-0.9	0.7	28	-0.1	-1.3	37	-0.8	0.2	69	0.6	1.4	40
1317+23	12	Medium	Elliptical	-1.1	-1.5	-0.4	40	-0.1	1.0	28	0.4	-0.4	37	1.1	1	69	1.1	1.2	40
1301+85	12	Standard	Round	-0.4	0.6	-0.7	40	-1.3	-0.4	28	-0.6	-0.7	37	0.3	1.4	69	0.5	0.6	40
1301+79	12	Standard	Round	-0.4	-0.5	-0.9	40	0.1	0.2	28	-0.8	-0.7	37	0.7	0.2	69	0.5	0.1	40
1301+73	12	Standard	Round	0.2	-0.2	-1.0	40	-1.0	0.2	28	-0.8	-0.2	37	-0.9	-0.2	69	0.7	0.4	40
1301+67	12	Standard	Round	0.5	-0.3	-0.3	40	0.1	0.3	28	-0.3	0.5	37	-0.6	0.7	69	0.8	1.4	40
1301+61	12	Standard	Round	-0.4	-0.2	-0.7	40	-0.9	0.7	28	0.5	-0.5	37	0.7	1.3	69	0.8	1.4	40
1301+55	12	Standard	Round	-0.4	0.2	0.4	40	-1.0	0.2	28	-0.9	-1.7	37	-0.7	0	69	0.1	0.9	40
1301+49	12	Standard	Round	-0.5	-0.6	-0.3	40	-1.1	0.9	28	1.0	-0.4	37	0.9	-0.5	69	1.2	0.1	40
1301+43	12	Standard	Round	-0.5	-0.4	-1.1	40	-0.1	-0.3	28	-1.0	0.0	37	-0.3	0.7	69	0.5	0.3	40
1301+37	12	Standard	Round	0	0.3	-1.1	40	-1.4	1.0	28	-0.3	0.0	37	0.6	1.5	69	-0.4	0.1	40
1301+31	12	Standard	Round	-0.8	-0.1	-0.5	40	-0.1	-0.5	28	-0.4	0.0	37	1.1	0.2	69	0.7	1.0	40
1290+87	12	Medium	Elliptical	0.4	-0.8	-0.7	43	-0.9	-0.4	30.8	0.5	-0.7	37	0.3	-0.4	70	0.5	0.6	43
1290+81	12	Medium	Elliptical	-0.6	0.5	0.0	43	-1	-0.3	30.8	-0.1	-0.7	37	0.6	0.5	70	0.6	0.8	43
1290+75	12	Medium	Elliptical	-0.3	-0.9	-0.3	43	-0.5	-0.2	30.8	0.2	-0.4	37	-0.1	0.2	70	-0.3	0.1	43
1290+69	12	Medium	Elliptical	-0.6	0.1	-0.2	43	-0.8	0.2	30.8	-0.4	-0.6	37	0.8	0.4	70	0.7	0.6	43
1290+63	12	Medium	Elliptical	-0.2	0.3	-0.6	43	-0.8	0.2	30.8	-0.4	-0.6	37	-0.8	0.7	70	0.2	0.6	43
1290+57	12	Medium	Elliptical	-1.3	0.3	-0.8	43	-0.8	0.2	30.8	-1.0	-1.3	37	-0.8	0.6	70	1.2	0.2	43
1290+51	12	Medium	Elliptical	-0.5	0.3	-0.5	43	-0.8	0.2	30.8	-1.0	-1.3	37	0.7	0.9	70	1.2	0.3	43
1290+45	12	Medium	Elliptical	-0.7	0.8	-0.5	43	-0.9	0.2	30.8	-0.8	-0.5	37	-0.3	0.2	70	1.2	0.8	43
1290+39	12	Medium	Elliptical	-0.4	-1.0	-0.5	43	-1.3	-0.3	30.8	-0.8	-0.9	37	0.3	0.4	70	1.6	1.6	43
1290+33	12	Medium	Elliptical	-0.7	-1.0	-1.5	43	0.1	0.4	30.8	-1.1	-0.7	37	-0.2	0.7	70	0.6	0.6	43
1279+38	18	Standard	Round	-0.5	0.0	-0.5	43	0.2	0.0	30.9	-0.5	-0.5	37	0.4	-0.3	70	1.2	0.0	43
1279+32	18	Standard	Round	0.1	0.8	-0.2	43	-0.8	0.9	30.9	-1.0	-0.5	37	0.8	1.1	70	0.6	1.4	43
1279+26	18	Standard	Round	0.5	-0.4	0.0	43	-0.1	0.0	30.9	-0.9	-0.4	37	-0.4	0.7	70	0.6	0.6	43
1279+20	18	Standard	Round	-0.8	-0.6	-0.2	43	0.2	-0.1	30.9	-0.5	0.0	37	0.8	0.3	70	1.2	1.0	43
1279+14	18	Standard	Round	-1.5	0.0	-0.8	43	-1.5	0.3	30.9	-1.1	-1.5	37	-0.4	1	70	1.0	-0.1	43
1279+08	18	Standard	Round	-0.7	0.0	-0.6	43	0.1	0.2	30.9	0.2	-0.7	37	0.6	0.2	70	1.1	1.4	43
1279+02	18	Standard	Round	-0.5	0.1	-0.5	43	0.0	0.0	30.9	-0.1	-0.5	37	0.3	0.2	70	0.6	0.2	43
1278+96	18	Standard	Round	0.7	-0.9	-1.1	43	-0.3	0.5	30.9	-0.6	-0.7	37	0.1	-0.1	70	0.5	1.4	43
1278+90	18	Standard	Round	-0.7	-0.8	-1.0	43	0.6	1.0	30.9	-1.0	-0.5	37	0.1	-0.3	70	0.9	0.7	43
1278+84	18	Standard	Round	-0.9	-0.8	-1.0	43	0.2	1.2	30.9	-0.8	0.0	37	0.7	-0.3	70	1.1	0.2	43
1277+89	18	Standard	Round	-0.1	-0.2	-1.2	41	-1.2	1.0	33	-1.0	-0.8	38	-0.4	0.7	70	-0.3	1.5	43
1277+83	18	Standard	Round	-0.5	0.1	-1.0	41	-0.1	0.9	33	-1.0	-0.7	38	0.6	0.6	70	1.1	1.6	43
1277+77	18	Standard	Round	-0.2	-1.3	-0.5	41	-0.1	0.4	33	-0.5	-0.5	38	1.1	0.1	70	0.6	0.7	43
1277+71	18	Standard	Round	0	-0.3	0.2	41	-0.8	-0.1	33	-0.4	-1.3	38	-0.8	0.5	70	0.5	1.0	43
1277+65	18	Standard	Round	-1	0.2	0.5	41	-1.4	0.2	33	-1.3	0.2	38	-0.3	0	70	1.5	1.3	43
1277+59	18	Standard	Round	0.3	0.2	0.1	41	0.7	1.0	33	-1.8	-1.0	38	0.2	0.7	70	0.2	1.4	43
1277+53	18	Standard	Round	-1.2	-0.7	-0.6	41	-0.8	1.6	33	0.2	-1.2	38	0.3	1.7	70	0.5	1.9	43
1277+47	18	Standard	Round	-0.3	-0.1	-0.5	41	-1.4	0.4	33	-0.3	-1.4	38	0.2	0	70	1.1	0.9	43
1277+41	18	Standard	Round	-0.2	0	0.0	41	-1.3	-0.3	33	-0.7	-1.8	38	-0.1	-0.1	70	-0.6	1.0	43
1277+35	18	Standard	Round	0	-0.5	-0.7	41	0.0	0.1	33	-1.0	0.3	38	1	0.6	70	1.2	1.0	43

91 1260+20	1256+87	Round	Standard	12	-0.7	-0.5	-0.6	0.2	0.4	-0.9	1.1	33.6	0.8	-1.4	43	0.5	0.5	0.5	0.5	0.5	-0.3	70	-0.3	1.7	50		
	1256+81	Round	Standard	12	1	-0.5	-1.2	-0.5	-0.4	-0.9	1.5	33.6	0.4	-0.5	43	1	0.3	0.3	0.3	0.3	0.3	0	70	-0.6	0.6	50	
	1256+75	Round	Standard	12	-0.3	-0.8	-0.4	-0.2	-0.2	-0.4	1.6	33.6	-0.8	-0.6	43	0.6	0.3	0.3	0.3	0.3	0.3	0	70	0.5	0.5	50	
	1256+69	Round	Standard	12	-1.1	-0.9	-0.4	-1.6	-0.3	-1.0	0.4	33.6	0.0	-1.8	43	-0.3	0.6	0.6	0.6	0.6	0.6	0	70	-0.1	0.8	50	
	1256+63	Round	Standard	12	0.1	-0.4	-0.2	-1.3	0.1	-1.2	0.4	33.6	-0.3	-1.7	43	1.5	-0.7	0.7	0.7	0.7	0.7	0	70	0.5	1.3	50	
	1256+57	Round	Standard	12	0.3	-0.1	0.2	-1.3	-0.1	-1.3	0.4	33.6	-0.3	-1.7	43	1.5	-0.7	0.7	0.7	0.7	0.7	0	70	0.5	1.3	50	
	1256+51	Round	Standard	12	-0.5	-0.2	0.2	-0.8	-0.5	-0.5	-0.3	33.6	-0.8	-0.8	43	0.7	0.2	0.2	0.2	0.2	0.2	0	70	0.5	1.7	50	
	1256+45	Round	Standard	12	0.6	0.6	-0.2	-0.1	0.4	-1.4	0.6	33.6	-1.0	-1.0	43	0	0.5	0.5	0.5	0.5	0.5	0	70	-0.4	1.0	50	
	1256+39	Round	Standard	12	0	-0.3	-0.3	0.2	0.2	-0.6	0.2	33.6	-0.3	-0.3	43	1.3	0.3	0.3	0.3	0.3	0.3	0	70	-0.1	0.1	50	
	1256+33	Round	Standard	12	0	-0.3	-0.3	0.2	0.2	-0.6	0.2	33.6	-0.3	-0.3	43	1.3	0.3	0.3	0.3	0.3	0.3	0	70	-0.1	0.1	50	
89 1257+20	1256+88	Elliptical	Medium	12	0.2	-0.3	-0.5	-0.5	-0.5	-0.2	1.5	33.6	0.5	-0.6	43	1	0.8	0.8	0.8	0.8	0.8	0	70	0.5	0.7	50	
	1256+82	Elliptical	Medium	12	0.1	-0.5	-0.5	-0.5	-0.5	-0.1	0.1	33.6	0.1	-1.2	43	0.6	-0.9	-0.9	-0.9	-0.9	-0.9	0	70	0.2	0.1	50	
	1256+76	Elliptical	Medium	12	0.5	-0.3	-0.4	0.7	0.7	-1.4	1.5	33.6	0.1	-0.6	43	1.5	0.3	0.3	0.3	0.3	0.3	0	70	0.5	0.1	50	
	1256+70	Elliptical	Medium	12	0.1	0.1	0.2	1.0	0.3	-1.4	0.2	33.6	-0.8	-1.8	43	0.2	0.8	0.8	0.8	0.8	0.8	0	70	0.1	0.1	50	
	1256+64	Elliptical	Medium	12	-0.3	0.2	0.1	-1.3	0.3	-1.0	0.3	33.6	0.0	-0.7	43	0.7	-0.8	-0.8	-0.8	-0.8	-0.8	0	70	0.8	0.4	50	
	1256+58	Elliptical	Medium	12	-0.3	-0.3	0.1	-1.3	0.3	-1.0	0.3	33.6	0.0	-0.7	43	0.7	-0.8	-0.8	-0.8	-0.8	-0.8	0	70	0.8	0.4	50	
	1256+52	Elliptical	Medium	12	0	-0.2	-0.2	-0.2	-0.2	-0.4	0.3	33.6	-0.7	-1.5	43	0.5	0.5	0.5	0.5	0.5	0.5	0	70	0.5	1.2	50	
	1256+46	Elliptical	Medium	12	-0.4	0	-0.4	-0.4	-0.4	-0.4	-0.4	0.3	33.6	-0.7	-1.5	43	0.5	0.5	0.5	0.5	0.5	0	70	0.5	1.2	50	
	1256+40	Elliptical	Medium	12	0.2	0.4	0.4	-0.4	-0.4	-0.8	-0.1	33.6	1.2	-0.6	43	0.6	0.8	0.8	0.8	0.8	0.8	0	70	0.0	1.7	50	
	1256+34	Elliptical	Medium	12	0	0.2	0.1	-0.5	0.4	-1.4	1.0	33.6	1.2	-0.6	43	0.6	0.8	0.8	0.8	0.8	0.8	0	70	-0.2	1.0	50	
87 1258+70	1256+86	Elliptical	Medium	12	-0.2	0.2	-0.6	-0.5	-0.5	-0.3	0.2	33.6	-0.6	-0.3	43	-0.1	-0.4	-0.4	-0.4	-0.4	-0.4	0	70	-0.5	0.3	50	
	1255+84	Elliptical	Medium	12	-0.5	-0.1	-0.3	-0.6	-0.6	-1.0	1.0	34.4	0.3	-0.5	43	0.5	-0.8	-0.8	-0.8	-0.8	-0.8	0	71	0.7	1.2	55	
	1255+78	Elliptical	Medium	12	-1.3	-0.1	-0.5	-0.3	-0.3	-1.2	0.3	34.4	-1.0	-1.4	43	0.3	0.7	0.7	0.7	0.7	0.7	0	71	0.6	0.2	55	
	1255+72	Elliptical	Medium	12	0.2	-1.7	-1.0	-0.3	-0.3	-0.8	0.1	34.4	-0.5	-1.4	43	0	-0.7	-0.7	-0.7	-0.7	-0.7	0	71	0.0	0.6	55	
	1255+66	Elliptical	Medium	12	0.1	0.2	-0.7	-0.3	-0.3	0.1	0.2	34.4	0	-0.5	43	0.7	-0.8	-0.8	-0.8	-0.8	-0.8	0	71	-0.1	0.1	55	
	1255+60	Elliptical	Medium	12	-0.3	-0.4	-0.5	-0.3	-0.3	0.1	0.1	34.4	0.1	-1.3	43	1	-0.9	-0.9	-0.9	-0.9	-0.9	0	71	1.0	-0.3	55	
	1255+54	Elliptical	Medium	12	-0.9	-0.3	-0.9	-0.6	-0.6	-0.6	-0.4	0.3	34.4	-0.6	-0.6	43	0.5	0.5	0.5	0.5	0.5	0	71	-0.7	-0.3	55	
	1255+48	Elliptical	Medium	12	0.2	0.0	0.0	-0.8	-0.8	-1.2	0.4	34.4	0.4	-0.7	43	0.2	-0.9	-0.9	-0.9	-0.9	-0.9	0	71	-0.1	-1.0	55	
	1254+92	Elliptical	Medium	12	0.4	0.2	0.0	-0.8	-0.8	-1.2	0.4	34.4	0.4	-0.7	43	0.2	-0.9	-0.9	-0.9	-0.9	-0.9	0	71	-0.1	-1.0	55	
	1254+86	Elliptical	Medium	12	0.9	0	-0.8	0.1	0.1	-0.7	0.4	34.4	-0.1	-0.7	43	0.7	-0.7	-0.7	-0.7	-0.7	-0.7	0	71	0.5	0.5	55	
85 1254+20	1254+80	Elliptical	Medium	12	0.2	-0.9	0.2	1.2	1.2	-0.8	0.0	34.4	-1.0	-0.8	43	-0.5	0.1	0.1	0.1	0.1	0.1	0	71	0.6	0.6	55	
	1252+84	Elliptical	Medium	12	0.3	-0.8	-0.2	-1.8	-1.8	-0.7	1.0	34.4	-0.3	-1.5	43	1	0.2	0.2	0.2	0.2	0.2	0	71	-0.5	0.4	55	
	1252+78	Elliptical	Medium	12	0.3	-1.5	-1.0	-0.5	-0.5	0.1	1.4	34.4	-0.4	-0.0	43	1	0.2	0.2	0.2	0.2	0.2	0	71	1.1	0.8	55	
	1252+72	Elliptical	Medium	12	-0.3	-0.7	-0.4	-0.8	-0.8	0.1	-1.4	34.4	-1.0	-0.2	43	1.4	-0.8	-0.8	-0.8	-0.8	-0.8	0	71	1.1	0.2	55	
	1252+66	Elliptical	Medium	12	0.3	-1.2	-1.0	-0.3	-0.3	-0.6	1.1	34.4	-0.7	-0.7	43	0.7	1.1	1.1	1.1	1.1	1.1	0	71	0.6	0.7	55	
	1252+60	Elliptical	Medium	12	0.3	-0.2	-0.5	0.2	0.2	-0.2	0.3	34.4	-0.8	-0.6	43	0.4	-0.3	-0.3	-0.3	-0.3	-0.3	0	71	0.8	1.1	55	
	1252+54	Elliptical	Medium	12	-0.9	-1	0.2	-1.0	-1.0	-1.4	0.5	34.4	0.1	-1.4	43	0.5	0.5	0.5	0.5	0.5	0.5	0	71	0.6	0.3	55	
	1252+48	Elliptical	Medium	12	-0.2	-0.4	-0.3	-0.2	-0.2	0.1	-0.2	0.4	34.4	0.0	-1.4	43	1	-0.8	-0.8	-0.8	-0.8	-0.8	0	71	0.5	1.4	55
	1253+42	Elliptical	Medium	12	0.1	0.4	-0.3	-0.8	-0.8	-1.0	-0.8	-0.8	34.4	-0.6	-0.6	43	1	-0.8	-0.8	-0.8	-0.8	-0.8	0	71	0.7	0.0	55
	1253+36	Elliptical	Medium	12	1.3	-0.3	-0.9	-0.8	-0.8	-1.3	-1.0	34.4	-0.4	-1.3	43	0.8	-0.6	-0.6	-0.6	-0.6	-0.6	0	71	0.4	-0.1	55	
83 1252+70	1252+84	Elliptical	Heavy	18	-0.3	-1.1	-0.3	-0.8	-0.8	-1.1	1.2	35.8	0.3	-1.5	46	0.5	0.8	0.8	0.8	0.8	0.8	0	72	-0.4	1.4	52	
	1252+78	Elliptical	Heavy	18	0.3	0.4	-1	-0.6	-0.6	-0.2	0.0	35.8	0.3	-0.3	46	0.7	0.8	0.8	0.8	0.8	0.8	0	72	-0.3	0.8	52	
	1252+72	Elliptical	Heavy	18	0.4	-0.3	0	-0.6	-0.6	-0.2	0.0	35.8	-0.8	-1.3	46	1.2	-0.2	-0.2	-0.2	-0.2	-0.2	0	72	0.7	-0.8	52	
	1252+66	Elliptical	Heavy	18	0.4	-0.3	-1.0	-0.5	-0.5	-0.8	0.4	35.8	-0.8	-0.7	46	0.4	-0.9	-0.9	-0.9	-0.9	-0.9	0	72	0.7	0.3	52	
	1252+60	Elliptical	Heavy	18	-0.7	-0.7	-0.2	-0.2	-0.2	-0.2	0.5	35.8	0.0	0.1	46	0.4	-0.9	-0.9	-0.9	-0.9	-0.9	0	72	0.6	-0.1	52	
	1252+54	Elliptical	Heavy	18	0.1	-1.7	0.2	-0.2	-0.2	0.1	1.3	35.8	0.3	0.2	46	1.7	0.2	0.2	0.2	0.2	0.2	0	72	1.5	1.0	52	
	1252+48	Elliptical	Heavy	18	0.1	-1.7	0.2	-0.2	-0.2	0.1	1.3	35.8	0.3	0.2	46	1.7	0.2	0.2	0.2	0.2	0.2	0	72	1.5	1.0	52	
	1251+92	Elliptical	Heavy	18	0.2	-1.0	-1.0	-1.0	-1.0	-0.6	0.2	35.8	0.6	-1.2	46	1.3	-0.9	-0.9	-0.9	-0.9	-0.9	0	72	0.8	0.6	52	
	1251+86	Elliptical	Heavy	18	-1.1	0.2	0.5	-0.8	-0.8	-1.2	-0.8	35.8	0.6	-1.2	46	0.5	0.9	0.9	0.9	0.9	0.9	0	72	-0.5	1.4	52	
	1251+80	Elliptical	Heavy	18	0.2	-0.3	0.2	0.1	0.1	-0.3	0.9	35.8	0.3	-0.6	46	0.2	-0.3	-0.3	-0.3	-0.3	-0.3	0	72	1.0	1.4	52	
81 1251+20	1250+84	Elliptical	Medium	12	-0.9	-0.7	-0.5	-0.6	-0.6	-1.4	0.3	35.9	-0.3	-0.7	46	0.5	-0.1	-0.1	-0.1	-0.1	-0.1	0	72	-0.4	0.6	52	
	1250+78	Elliptical	Medium	12	-0.8	-0.6	-0.3	-0.4	-0.4	-0.5	0.3	35.9	0.1	0.0													

	1233+31	Heavy	15	-1	-1.3	-0.5	-0.3	39	-0.8	-0.2	39.3	-0.5	-0.7	48	-0.8	1	70	-0.6	1.5	50
	1233+31	Heavy	15	-0.8	0.8	0.4	-0.6	39	-0.8	0.2	39.3	-0.1	-0.5	48	0.3	0.6	70	0.5	-0.1	50
	1233+25	Heavy	15	-0.3	-0.4	0.0	0.2	39	-0.2	0.2	39.3	-0.6	-0.8	48	-0.3	0.5	70	-0.2	0.6	50
	1233+19	Heavy	15	-0.3	-0.5	-0.1	0.0	39	0.2	0.3	39.3	-0.8	-0.2	48	0.4	0.7	70	-0.8	0.0	50
	1233+13	Heavy	15	-0.7	0	-0.7	-1.2	39	-0.3	1.6	39.3	0.6	-1.7	48	-0.7	1	70	-0.7	-0.1	50
	1233+07	Heavy	15	0	0	-0.5	-0.6	39	-0.2	-0.2	39.3	0.8	-1.8	48	-0.8	1	70	-0.1	1.0	50
	1233+01	Heavy	15	-0.8	-0.4	-0.7	-0.9	39	-1.3	1.0	39.3	0.2	-0.7	48	0.1	1.3	70	-0.3	1.2	50
	1232+95	Heavy	15	0.4	0.2	-0.3	-0.3	39	-0.5	0.2	39.3	-0.9	-0.7	48	0.2	0	70	-0.5	0.8	50
	1232+89	Heavy	15	0	-1	-0.3	-0.5	39	-1.4	0.5	39.3	-1.4	-1.8	48	0.1	1.0	70	-0.2	0.3	50
	1232+83	Heavy	15	-1.5	-0.3	0.5	2.5	39	-1.2	0.9	39.3	-0.6	-1.3	48	-0.3	1.7	70	-0.1	1.3	50
	1231+87	Heavy	15	-0.4	-0.2	-0.1	0.4	39	-0.2	-0.1	39.3	-0.1	-0.7	48	0.4	0.5	70	-0.9	0.0	50
	1231+81	Heavy	15	-0.1	-0.2	-0.5	-0.9	39	-1.0	1.0	39.3	-0.7	0.0	48	0.2	1.5	70	-0.1	1.2	50
	1231+75	Heavy	15	-0.8	-0.1	0.3	-0.8	39	-1.4	1.1	39.3	-0.4	-1.5	48	-0.5	1	70	-0.2	1.2	50
	1231+69	Heavy	15	-1.1	-0.7	-1.1	-0.8	39	0.4	1.5	39.3	0.5	-0.8	48	0.0	0.0	70	0.0	0.0	50
	1231+63	Heavy	15	-0.8	0.1	-0.3	-0.8	39	-0.8	0.7	39.3	-0.9	-1.4	48	0.8	1	70	-1.2	0.0	50
	1231+57	Heavy	15	-0.5	0.6	0.2	0.2	39	-1.4	0.5	39.3	-0.7	-1.3	48	-0.5	0.2	70	-1.4	0.8	50
	1231+51	Heavy	15	0.9	0	-0.9	-0.9	39	-1.2	0.2	39.3	-1.0	-0.5	48	0.1	0.9	70	-0.8	0.8	50
	1231+45	Heavy	15	0.9	-0.3	-0.2	-0.4	39	-0.8	0.3	39.3	-0.3	-1.8	48	0.5	-0.2	70	-0.2	0.7	50
	1231+39	Heavy	15	0.5	0	-0.8	-0.9	39	-0.8	0.2	39.3	0.1	-0.5	48	0.3	0.7	70	0.0	0.6	50
	1231+33	Heavy	15	0.5	-0.8	-0.6	-0.4	39	-1.2	0.2	39.3	0.3	-1.7	48	-0.8	0.4	70	-0.9	0.0	50
	1230+36	Heavy	15	-0.2	-0.4	0.3	0.3	43	-0.8	1.0	44.4	-0.3	-0.7	48	0.4	0.8	70	0.0	0.6	47
	1230+30	Heavy	15	0.8	-0.5	-0.3	0.2	43	0.1	0.8	44.4	-1.0	-0.4	48	0.3	0.8	70	-0.5	0.9	47
	1230+24	Heavy	15	0.7	-0.5	-0.3	-1.0	43	-0.1	1.0	44.4	-0.2	-1.4	48	0.3	1.1	70	-0.8	0.1	47
	1230+18	Heavy	15	0.1	-0.2	-0.4	-1.0	43	-0.2	0.7	44.4	0.2	-0.8	48	-0.2	1.1	70	-0.9	-0.1	47
	1230+12	Heavy	15	0.3	1.3	-0.9	-1.0	43	-0.2	0.5	44.4	-1.0	-1.3	48	-0.4	1	70	-0.9	0.3	47
	1230+06	Heavy	15	0.5	0	-0.8	-1.0	43	-0.1	0.0	44.4	0.7	-1.8	48	-0.4	1.4	70	-1.2	-0.1	47
	1230+00	Heavy	15	-0.4	-0.1	0.2	-1.1	43	-3.0	0.4	44.4	0.4	-1.2	48	-0.4	1.6	70	-0.2	-0.1	47
	1229+94	Heavy	15	-0.1	-0.2	-0.2	-0.3	43	0.2	0.7	44.4	-0.6	-0.7	48	-0.4	1.3	70	-0.2	0.7	47
	1229+88	Heavy	15	-0.7	0.2	-1.9	-0.8	43	-0.1	-0.1	44.4	-0.8	-0.7	48	-0.8	0.7	70	0.5	0.4	47
	1229+82	Heavy	15	-0.4	0.4	-0.1	-0.2	43	-1.4	0.5	44.4	-0.3	-1.2	48	0.2	0.5	70	-0.2	1.0	47
	1228+85	Heavy	18	-0.1	-0.2	-0.7	-0.3	43	0.0	-0.3	44.4	-0.7	-0.6	48	-0.8	1	70	0.2	1.7	47
	1228+79	Heavy	18	0	-0.3	-0.4	-0.4	43	-0.4	1.0	44.4	0.2	-1.3	48	-0.9	1	70	-1.0	0.4	47
	1228+73	Heavy	18	-0.3	0.2	-0.4	-0.4	43	-0.4	-0.1	44.4	-0.1	-1.1	48	0.8	1.4	70	-1.3	1.3	47
	1228+67	Heavy	18	-0.3	0.8	-0.1	-0.8	43	-0.4	0.7	44.4	-0.8	-0.5	48	1	-0.8	70	-0.8	-0.1	47
	1228+61	Heavy	18	-0.3	0.8	-0.3	-0.6	43	-0.4	-0.2	44.4	0.4	-0.8	48	-0.4	-1.6	70	-0.5	1.2	47
	1228+55	Heavy	18	0.2	0.1	-0.3	-0.5	43	-0.1	-0.1	44.4	0.0	-1.4	48	-0.8	1.2	70	-0.1	1.0	47
	1228+49	Heavy	18	0.2	0.3	-0.9	-0.5	43	-0.8	1.0	44.4	0.2	-0.9	48	-1.9	1	70	-0.4	-0.4	47
	1228+43	Heavy	18	-0.3	0.2	-0.9	-1.0	43	-0.8	0.9	44.4	0.4	-1.6	48	-0.8	1.2	70	-0.9	0.5	47
	1228+37	Heavy	18	-0.3	-0.5	-0.3	0.5	43	0.0	0.3	44.4	-0.1	-0.7	48	-0.6	1.2	70	-0.9	0.5	47
	1228+31	Heavy	18	0	-0.5	-0.5	-0.9	43	-1.0	0.4	44.4	-0.5	-0.9	48	-0.3	0.8	70	0.0	0.2	47
	1227+35	Heavy	12	-0.1	-0.3	0.8	-1.5	40	-0.6	0.8	44.4	1.2	0.1	55	-0.1	1.4	72	-0.8	1.4	55
	1227+29	Heavy	12	-0.4	-0.2	-0.8	0.6	40	-0.6	0.2	44.4	-0.6	-1.2	55	0.0	1.3	72	-0.8	1.5	55
	1227+23	Heavy	12	-0.3	-0.6	-0.8	-1.0	40	-1.2	0.5	44.4	-0.2	-1.3	55	-0.1	0.9	72	-0.9	0.3	55
	1227+17	Heavy	12	-0.3	-0.6	0.2	-0.9	40	-1.4	0.2	44.4	0.2	-1.3	55	0.1	0.9	72	-0.9	0.3	55
	1227+11	Heavy	12	-0.3	-1.1	0.7	-0.9	40	-0.1	0.9	44.4	-0.3	-1.3	55	-0.8	0.2	72	-1.3	0.9	55
	1227+05	Heavy	12	-0.6	-1	0.7	-1.5	40	-0.1	0.4	44.4	0.2	-1.3	55	-0.3	1.2	72	-0.8	1.2	55
	1226+99	Heavy	12	-0.4	0.2	0.2	-1.5	40	-1.3	1.5	44.4	0.6	-1.3	55	-0.3	1.2	72	-0.8	1.4	55
	1226+93	Heavy	12	-0.3	0.2	-1.6	-0.8	40	-0.7	0.9	44.4	-0.8	-1.3	55	-0.2	1.3	72	-1.3	1.0	55
	1226+87	Heavy	12	-0.1	-0.3	-1.1	-0.6	40	-0.3	0.7	44.4	-0.9	-0.6	55	-0.8	0.9	72	-1.1	1.7	55
	1226+81	Heavy	12	-0.4	-0.4	0.1	-0.8	40	-1.3	1.7	44.4	-1.0	-1.8	55	-0.1	1.4	72	-0.2	1.4	55
	1225+85	Heavy	18	-0.8	-0.5	-0.5	-0.8	40	-0.6	0.9	44.4	0.1	-0.9	55	-0.6	0.2	72	0.0	0.0	55
	1225+79	Heavy	18	-0.5	0.2	-0.6	-0.7	40	-0.6	1.1	44.4	0.4	-0.7	55	-0.8	1	72	-0.1	1.4	55
	1225+73	Heavy	18	-0.9	-0.3	-0.3	-1.1	40	-0.5	1.4	44.4	0.3	-1.3	55	0.1	1.5	72	-0.1	1.7	55
	1225+67	Heavy	18	-0.9	-0.6	-1.0	-0.8	40	-0.2	1.6	44.4	0.9	-0.6	55	0.1	1.3	72	-0.1	1.7	55
	1225+61	Heavy	18	0.1	-0.4	-0.5	0.2	40	-0.1	-0.2	44.4	-1.0	-0.5	55	0.3	0.9	72	0.5	0.3	55
	1225+55	Heavy	18	0.2	-0.4	-0.5	0.2	40	-0.2	0.2	44.4	-0.5	-1.8	55	0.3	0	72	-0.2	0.6	55
	1225+49	Heavy	18	0.2	-1.0	0.4	0.4	40	-0.3	-0.3	44.4	-0.5	-1.4	55	0.3	0.2	72	-0.9	0.2	55
	1225+43	Heavy	18	-0.5	-0.5	-1.1	0.1	40	-0.1	0.9	44.4	0.8	-0.6	55	0.3	1.2	72	0.5	0.3	55
	1225+37	Heavy	18	-0.1	-0.2	-1.3	-0.5	40	-0.8	-0.2	44.4	0.4	-0.7	55	0.4	0.5	72	0.1	0.4	55
	1225+31	Heavy	18	-0.9	-0.1	-0.4	0.2	40	-0.2	0.4	44.4	-0.8	0.0	55	0	0.6	72	-0.1	1.0	55
	1224+25	Heavy	12	0	0.1	-0.5	-0.4	43	-0.2	0.2	45.5	-0.6	-0.5	54	-0.4	1	73	-0.3	1.0	56
	1224+19	Heavy	12	0.5	-1.0	-2.0	-0.4	43	0.3	1.4	45.5	0.6	-1.5	54	-0.3	1.2	73	-0.8	1.0	56
	1224+13	Heavy	12	-1	-0.2	-0.3	-0.4	43	0.1	0.5	45.5	0.1	-0.7	54	-0.8	1.3	73	-0.6	0.9	56
	1224+07	Heavy	12	-0.2	-0.5	0.4	-0.7	43	0.3	0.9	45.5	-1.0	0.5	54	0.6	1.1	73	-0.2	0.3	56
	1223+95	Heavy	12	-0.3	-1.1	-2.0	-0.1	43	-1.3	1.0	45.5	0.2	-1.3	54	-0.6	1.1	73	-0.9	0.7	56
	1223+89	Heavy	12	-0.8	-1.1	-0.7	-0.5	43	-0.8	1.0	45.5	-0.4	-1.7	54	-0.8	1.1	73	-0.9	0.9	56
	1223+83	Heavy	12	-0.8	1.2	-1.0	-0.7	43	-0.8	1.2	45.5	-0.3	-1.2	54	-0.4	1.7	73	-0.8	0.6	56
	1223+77	Heavy	12	-0.3	-0.5	-0.7	-0.8	43	-0.2	0.4	45.5	-0.1	-1.0	54	-0.8	1.4	73	-0.8	1.5	56
	1223+71	Heavy	12	-1	-0.3	0.0	-1.2	43	-1.0	0.5	45.5	-1.0	-1.3	54	-0.1	1	73	-1.0	-0.1	56

35 1210+20	1209+86	Elliptical	Medium	15	-0.6	-0.7	-0.4	0.1	39	0.3	0.7	48.7	0.0	-1.5	60	0.9	-0.3	84	0.0	0.6	55	
	1209+80	Elliptical	Medium	15	1.2	1	-0.2	-0.3	39	-0.8	0.9	48.7	0.0	-0.7	60	0	-0.2	84	0.0	0.6	55	
	1209+74	Elliptical	Medium	15	-1	-0.2	-0.2	-1.2	39	-0.1	-0.1	48.7	-0.6	-1.5	60	0.1	0.8	84	0.9	0.9	55	
	1209+68	Elliptical	Medium	15	-0.6	0.6	2.6	-1.4	39	-1.3	1.2	48.7	0.3	-0.5	60	1	0.8	84	0.9	1.4	55	
	1209+62	Elliptical	Medium	15	-0.6	0.6	-0.7	-0.6	39	-1.4	1.5	48.7	0.5	-1.7	60	1	-0.3	84	-0.2	-1.4	55	
	1209+56	Elliptical	Medium	15	0.1	-0.1	-1.3	-0.2	39	-0.1	0.3	48.7	0.6	-0.5	60	1.1	0.2	84	1.1	-1.0	55	
	1209+50	Elliptical	Medium	15	-0.1	-0.3	-0.4	1.1	39	-0.2	0.8	48.7	1.1	-1.7	60	0	0.8	84	0.0	0.0	55	
	1209+44	Elliptical	Medium	15	-0.6	-0.1	-0.5	0.5	39	-0.3	0.2	48.7	-1.0	-1.3	60	0.5	0.9	84	-0.1	-0.8	55	
	1209+38	Elliptical	Medium	15	-0.4	0.3	-0.4	0.3	39	-0.3	1.0	48.7	0.8	-1.5	60	0.8	0.3	84	0.0	-1.6	55	
	1209+32	Elliptical	Medium	15	-0.5	1.1	0.4	0.3	39	-1.3	0.2	48.7	-1.0	-0.7	60	1	-0.4	84	0.2	-1.3	55	
	33 1207+20	1206+85	Elliptical	Medium	15	0.1	0.5	0.1	-1.7	39	-1.0	1.5	48.7	1.0	-0.7	60	0.9	0.9	84	0.3	-0.1	55
		1206+79	Elliptical	Medium	15	-0.8	0.2	-0.9	-0.5	39	-1.3	0.9	48.7	0.7	-1.8	60	0.6	0.8	84	0.0	0.0	55
		1206+73	Elliptical	Medium	15	-0.8	0.5	-0.3	-0.9	39	-1.1	1.0	48.7	-0.8	-1.5	60	0.6	0.8	84	0.0	-1.7	55
		1206+67	Elliptical	Medium	15	-0.5	-0.4	-0.3	-0.3	39	-1.1	-0.4	48.7	-0.6	0.0	60	0.8	-0.6	84	0.3	-0.1	55
		1206+61	Elliptical	Medium	15	-0.5	0.3	0.0	-1.5	39	-0.6	1.6	48.7	-0.3	-1.1	60	0.3	0.9	84	0.1	-1.0	55
1206+55		Elliptical	Medium	15	-0.5	-0.5	-0.6	-0.8	39	-0.8	0.3	48.7	-0.8	-1.6	60	0.4	-1	84	-0.1	-1.7	55	
1206+49		Elliptical	Medium	15	-1.4	-0.5	-0.6	-0.5	39	-0.9	1.0	48.7	0.8	-1.0	60	1.1	-0.9	84	0.9	-1.7	55	
1206+43		Elliptical	Medium	15	-1.4	-0.7	-1.4	-0.8	39	-1.1	0.2	48.7	0.1	-1.3	60	0.9	-0.2	84	0.2	-0.8	55	
1206+37		Elliptical	Medium	15	-0.5	0.1	-0.8	0.1	39	-0.1	-0.3	48.7	0.8	-1.8	60	0.9	-0.3	84	1.5	-0.8	55	
1206+31		Elliptical	Medium	15	-0.5	-0.1	-0.2	-0.9	39	-1.3	1.1	48.7	-0.2	-0.4	60	1.6	-0.2	84	1.5	-0.8	55	
31 1205+70		1205+39	Elliptical	Heavy	15	0.3	1.1	-0.7	-1.5	38	-0.4	1.5	57.4	0.8	-1.0	54	0.5	0.9	85	0.5	0.6	53
		1205+33	Elliptical	Heavy	15	0.3	-0.2	-0.8	-2.0	38	-0.8	0.5	57.4	-0.8	-1.3	54	0.9	0	85	0.3	-1.1	53
		1205+27	Elliptical	Heavy	15	-0.4	0	-0.8	-1.0	38	-0.1	0.2	57.4	-0.8	-0.8	54	0.9	-0.8	85	1.5	-1.0	53
		1205+21	Elliptical	Medium	12	-0.5	-0.5	-0.3	-0.8	38	-0.3	-0.3	57.4	-1.0	-0.3	54	1.1	0.6	85	1.2	-1.2	53
		1205+15	Elliptical	Heavy	15	-0.5	-0.5	-0.7	-0.5	38	-0.9	0.1	57.4	-1.0	-0.6	54	1.2	-0.3	85	-2.3	-1.3	53
	1205+09	Elliptical	Heavy	15	-0.5	-0.8	-0.4	-0.7	38	-0.2	0.2	57.4	0.5	0.0	54	1.6	0.8	85	0.1	-0.2	53	
	1205+03	Elliptical	Heavy	15	-0.4	-0.2	-0.4	-0.9	38	-1.4	1.2	57.4	0.8	-0.9	54	1.3	0.7	85	0.5	-0.5	53	
	1204+97	Elliptical	Heavy	15	-0.6	-0.1	-0.8	-0.2	38	-1.3	0.0	57.4	0.3	-1.5	54	1.7	0.3	85	0.9	-1.7	53	
	1204+91	Elliptical	Heavy	15	0	-0.3	-0.1	-1.1	38	-0.5	0.8	57.4	0.3	-0.7	54	1.3	0.2	85	1.1	-0.7	53	
	1204+85	Elliptical	Heavy	15	0.5	0.1	-1.0	-0.6	38	-0.8	0.2	57.4	-0.8	-1.7	54	0	-0.6	85	0.2	-1.2	53	
	29 1202+70	1202+39	Elliptical	Medium	12	-0.2	0.7	-0.2	-1.3	38	-1.3	1.5	57.4	1.2	-1.3	54	0.2	0.7	85	-0.3	0.3	53
		1202+33	Elliptical	Medium	12	-0.6	-0.2	0.0	-0.5	38	-0.7	1.6	57.4	0.5	0.0	54	1.7	0.8	85	0.9	0.0	53
		1202+27	Elliptical	Medium	12	0.6	-0.4	-1.3	0.2	38	-0.7	-0.2	57.4	-0.3	-1.8	54	1.5	1	85	0.8	-1.8	53
		1202+21	Elliptical	Medium	12	-0.3	-0.4	-0.3	-1.1	38	-0.7	1.0	57.4	-0.3	-0.7	54	0.2	-0.6	85	0.9	-0.3	53
		1202+15	Elliptical	Medium	12	-0.3	-0.4	-1.3	-1.3	38	-1.4	1.1	57.4	0.5	0.0	54	1.6	0.8	85	1.1	-0.2	53
1202+09		Elliptical	Medium	12	-1	-1.1	-0.3	-2.0	38	0.1	1.2	57.4	0.8	-0.9	54	1.3	0.8	85	0.5	-0.5	53	
1202+03		Elliptical	Medium	12	0	0.6	-0.5	-1.5	38	-0.8	0.2	57.4	0.1	-0.8	54	0.9	0.7	85	0.2	-0.3	53	
1201+97		Elliptical	Medium	12	0	0.6	-0.7	-1.2	38	-1.2	1.2	57.4	-1.0	-1.4	54	-0.2	0.9	85	0.5	-0.1	53	
1201+91		Elliptical	Medium	12	-0.8	0	-0.7	-1.9	38	-1.2	1.2	57.4	0.2	-0.6	54	0.2	0.2	85	0.5	-0.1	53	
1201+85		Elliptical	Medium	12	-0.5	-1.3	-1.3	0.2	38	-0.6	1.0	57.4	0.0	-1.3	54	0.8	-0.3	85	0.2	-1.7	53	
27 1199+70		1199+26	Elliptical	Heavy	12	0.8	-0.6	-1.0	-0.5	38	0.3	1.7	52.3	-0.8	0.5	52	1.2	0.8	90	1.2	-1.6	53
		1199+20	Elliptical	Heavy	12	0.2	0.2	0.2	-0.4	38	-1.2	0.0	52.3	-0.8	-1.7	52	1.1	-0.3	90	0.9	-0.8	53
		1199+14	Elliptical	Heavy	12	-1.3	0.1	0.7	-0.8	38	-0.6	1.8	52.3	0.2	-1.6	52	0.3	-0.3	90	0.4	-1.1	53
		1199+08	Elliptical	Heavy	12	0	0	0.1	-0.8	38	0.0	0.2	52.3	-1.2	-1.0	52	0.8	-0.3	90	0.4	-1.1	53
		1199+02	Elliptical	Heavy	12	0	0	0.6	0.6	38	0.3	0.2	52.3	-1.4	-1.6	52	1.5	-0.8	90	1.2	-0.6	53
	1198+96	Elliptical	Heavy	12	-1.3	0.7	0	0.1	38	-1.3	0.2	52.3	-1.4	-1.6	52	1	-0.9	90	1.0	-1.2	53	
	1198+90	Elliptical	Heavy	12	-0.4	0.2	0.2	-1.1	38	-1.1	1.5	52.3	0.3	-0.5	52	0.1	0.8	90	1.0	-1.2	53	
	1198+84	Elliptical	Heavy	12	-0.8	0.3	0.7	-0.7	38	-0.7	1.8	52.3	0.2	0.5	52	0.5	0.8	90	1.5	-1.4	53	
	1198+78	Elliptical	Heavy	12	-0.8	0.2	0.7	-1.2	38	-0.7	1.8	52.3	0.2	-1.5	52	0.1	0.8	90	0.7	-0.3	53	
	1198+72	Elliptical	Heavy	12	-0.7	-0.5	-0.4	-1.1	38	-0.1	1.5	52.3	1.1	-0.7	52	-0.2	0.3	90	0.3	0.0	53	
	25 1196+20	1197+87	Elliptical	Heavy	12	-0.2	0.2	-0.3	-1.3	38	-0.4	1.4	52.3	0.1	-1.6	52	1	0.5	90	-0.2	-0.6	53
		1197+81	Elliptical	Heavy	12	-0.2	0.6	-0.5	-0.3	38	-1.3	1.1	52.3	-1.0	-1.8	52	0.7	-0.7	90	0.0	-1.8	53
		1197+75	Elliptical	Heavy	12	0	0.2	-0.8	-0.9	38	0.3	1.1	52.3	0.5	-1.6	52	1	0.1	90	0.9	-0.3	53
		1197+69	Elliptical	Heavy	12	0.6	0.4	-0.1	-0.4	38	-0.9	1.7	52.3	-0.9	-0.7	52	0.9	-0.4	90	0.2	-1.6	53
		1197+63	Elliptical	Heavy	12	0.2	0.5	-0.8	-0.5	38	-1.2	1.7	52.3	0.0	0.0	52	1.7	1	90	-0.3	-1.7	53
1197+57		Elliptical	Heavy	12	0.2	0.7	-0.7	-0.3	38	-1.2	1.0	52.3	-1.0	-1.5	52	1.2	-0.3	90	0.3	-1.0	53	
1197+51		Elliptical	Heavy	12	-0.5	0.1	-0.6	-1.5	38	-0.1	1.1	52.3	0.6	-0.7	52	1.2	0.2	90	1.1	0.0	53	
1197+45		Elliptical	Heavy	12	-0.3	-0.3	-1	-0.6	38	-1.2	1.4	52.3	-1.0	-1.5	52	-0.2	0.9	90	0.1	-1.0	53	
1197+39		Elliptical	Heavy	12	-0.5	-0.5	-0.7	-1.1	38	-0.5	1.1	52.3	-0.6	-1.1	52	0.1	0.8	90	0.2	-1.5	53	
1197+33		Elliptical	Heavy	12	0.2	0.5	-0.7	-1	38	-1.8	0.5	52.3	-0.8	-0.5	52	0	-0.2	90	0.0	-1.8	53	
23 1195+70		1195+34	Elliptical	Medium	12	0.3	0.8	0.3	-0.7	38	-0.5	1.0	61.3	0.5	-0.5	54	0.9	0.3	91	1.4	-1.6	56
		1195+28	Elliptical	Medium	12	-0.6	-0.3	-0.7	-0.7	38	-0.3	-0.3	61.3	-0.3	-1.5	54	0.1	-0.3	91	0.1	-1.5	56
		1195+22	Elliptical	Medium	12	0.1	-0.3	-0.5	0.2	38	-0.6	0.4	61.3	-0.8	-1.5	54	0.8	0.6	91	0.0	-1.8	56
		1195+16	Elliptical	Medium	1																	

8 1181+70	1181+39	Round	Standard	15	1	0	0.1	-0.3	36	-0.4	1.1	59.1	-0.3	-1.7	59	0.3	-0.8	98	0.0	-1.8	63
	1181+33	Round	Standard	15	1.3	-0.7	-0.5	-0.4	36	-1.2	1.0	59.1	0.7	-1.6	59	-0.1	-0.8	98	0.0	-1.0	63
	1181+27	Round	Standard	15	-0.5	-0.6	-0.7	-0.7	36	-1.2	1.5	59.1	1.0	-0.5	59	0.8	0.3	98	1.0	0.1	63
	1181+21	Round	Standard	15	0.6	0.2	-0.8	-0.3	36	0.3	0.4	59.1	-1.0	0.0	59	1.7	-0.6	98	0.9	-1.3	63
	1181+15	Round	Standard	15	0.5	-0.3	-0.9	-0.9	36	-0.7	1.3	59.1	-1.0	-0.7	59	-0.2	0.2	98	0.0	-1.1	63
	1181+09	Round	Standard	15	0.3	-1.3	-0.8	-1.0	36	0.3	1.2	59.1	0.5	-1.3	59	1	0	98	0.9	-0.3	63
	1181+03	Round	Standard	15	-0.1	0.1	1.5	-0.7	36	-1.3	1.2	59.1	0.3	-1.4	59	-0.2	0.6	98	0.0	-0.6	63
	1180+97	Round	Standard	15	-0.2	-1	-0.3	-1.1	36	-0.1	1.7	59.1	0.5	-1.3	59	1.2	0.7	98	0.7	0.1	63
1180+91	Round	Standard	15	0	-0.8	0.0	-1.0	36	0.5	0.5	59.1	-0.8	0.5	59	1.2	0.8	98	1.4	-1.3	63	
1180+85	Round	Standard	15	-0.7	-0.3	-1.0	-1.3	36	0.5	1.6	59.1	-0.1	0.6	59	1.2	0.5	98	0.8	-0.8	63	
6 1180+20	1179+87	Round	Standard	12	-4	-0.7	-1.0	-0.8	36	-1.0	1.0	59.1	0.8	-1.9	59	0.3	-0.3	98	0.0	0.0	63
	1179+81	Round	Standard	12	-1	-0.4	0.2	-0.5	36	-1.2	2.3	59.1	-1.0	-1.5	59	0.2	0	98	1.0	-1.7	63
	1179+75	Round	Standard	12	-0.5	-0.9	-0.3	-0.3	36	-0.1	0.0	59.1	0.2	-0.7	59	0.6	0.2	98	0.8	0.0	63
	1179+69	Round	Standard	12	-0.8	-0.7	0.0	-0.5	36	0.5	0.1	59.1	0.5	-0.8	59	1.5	0.3	98	0.9	-1.3	63
	1179+63	Round	Standard	12	-0.3	-1	0.0	-0.8	36	-0.1	1.7	59.1	0.4	-1.7	59	1.6	0.8	98	0.9	-0.7	63
	1179+57	Round	Standard	12	-0.8	-0.4	-1.5	-1.3	36	-0.3	0.1	59.1	0.0	-0.1	59	1.3	-0.7	98	0.9	-1.3	63
	1179+51	Round	Standard	12	-0.4	-0.3	0.0	-1.8	36	-0.7	0.0	59.1	-0.8	-1.4	59	0	-0.6	98	-0.1	-0.6	63
	1179+45	Round	Standard	12	-1	-1.1	-0.5	-1.8	36	0.3	1.7	59.1	0.6	-0.3	59	1.2	0.8	98	1.5	0.2	63
1179+39	Round	Standard	12	-0.2	-0.5	-0.2	0.9	36	-1.2	1.8	59.1	0.3	-1.7	59	1	0.8	98	-0.1	-1.9	63	
1179+33	Round	Standard	12	0	-0.4	-0.2	-1.0	36	-0.1	-0.1	59.1	0.4	-1.3	59	1.1	-0.8	98	0.9	-1.6	63	
4 1178+70	1178+25	Round	Standard	12	0.6	-1.5	-0.3	0.5	36	-1.0	0.5	51.5	-0.1	-1.3	61	0.2	-0.2	93	0.3	-1.1	68
	1178+19	Round	Standard	12	-0.8	-1	-0.7	-1.7	36	-0.7	1.2	51.5	0.0	-1.4	61	1	0	93	0.9	-0.3	68
	1178+13	Round	Standard	12	0.3	-0.7	-0.7	-0.1	36	-0.3	0.5	51.5	-1.0	0.0	61	1	-0.6	93	1.0	-0.8	68
	1178+07	Round	Standard	12	0.6	0.2	0.9	-0.8	36	-0.3	1.1	51.5	0.4	-0.1	61	0.7	0.3	93	0.0	-1.9	68
	1178+01	Round	Standard	12	0.2	-0.5	0.5	-0.6	36	-0.2	0.2	51.5	-1.0	-1.8	61	0.2	0.6	93	0.1	-1.6	68
	1177+95	Round	Standard	12	-1	-1	-0.5	-0.4	36	-0.1	0.0	51.5	0.7	-0.2	61	0.7	0.8	93	1.0	-1.3	68
	1177+89	Round	Standard	12	-0.5	-0.9	-2.0	-0.8	36	0.5	1.5	51.5	0.1	-0.7	61	1.2	0.6	93	0.9	0.0	68
	1177+83	Round	Standard	12	-2	-0.7	-1.0	-1.5	36	-0.6	1.5	51.5	-1.0	-0.7	61	1.2	0.6	93	0.2	0.1	68
1177+87	Round	Standard	12	-0.5	0.4	-0.9	0.0	36	-0.7	1.1	51.5	-0.8	-1.3	61	1.2	-0.3	93	1.0	-1.8	68	
1177+81	Round	Standard	12	-1	-0.7	-0.9	-0.9	36	-1.1	1.3	51.5	0.4	-1.3	61	0.2	0.8	93	0.8	-0.2	68	
2 1177+20	1176+84	Round	Standard	12	-0.9	-1.6	-0.8	-1.0	36	0.1	1.3	51.5	-0.4	-0.3	61	2.2	0.3	93	2.0	-1.3	68
	1176+78	Round	Standard	12	-1.1	-0.4	-0.9	-0.8	36	-0.2	0.3	51.5	0.3	0.0	61	1.6	0	93	0.9	-1.0	68
	1176+72	Round	Standard	12	-0.5	-1	-0.8	-1.4	36	-1.3	0.8	51.5	-0.3	-1.8	61	-0.3	-0.3	93	0.8	-1.7	68
	1176+66	Round	Standard	12	-1	-0.8	-1.4	-1.1	36	-1.2	1.2	51.5	0.0	-0.5	61	1.6	0.9	93	0.6	0.1	68
	1176+60	Round	Standard	12	-1.2	-0.8	-1.1	-1.0	36	0.3	1.2	51.5	0.0	-0.5	61	1.5	0.3	93	1.5	-0.4	68
	1176+54	Round	Standard	12	-0.3	-0.7	-0.5	-0.5	36	-1.0	1.1	51.5	-0.4	-0.6	61	0.3	0.8	93	-0.3	-0.7	68
	1176+48	Round	Standard	12	-1	-0.3	0.1	-0.5	36	0.5	1.0	51.5	-1.0	-0.6	61	1	0.7	93	1.0	-1.9	68
	1176+42	Round	Standard	12	-0.4	-1.3	-0.5	-0.8	36	0.8	-0.2	51.5	-0.9	0.0	61	1.2	-0.8	93	1.2	-0.8	68
1176+36	Round	Standard	12	-0.5	-0.6	-0.6	-0.8	36	0.4	1.0	51.5	-0.8	-0.7	61	1.6	-0.2	93	1.1	-0.5	68	
1176+30	Round	Standard	12	-0.7	-0.6	-1.0	-0.7	36	0.3	1.4	51.5	0.3	-0.8	61	1.3	-0.8	93	1.0	0.2	68	
BOP	1175+44																				

Table F.2. Steel dowels, faulting section averages

Section No.	Ref. Station	Bar Type	Bar Size	Spacing (inches)	Faulting Section Averages (mm)											
					9/21/2002		4/5/2003		10/25/2003		4/10/2004		8/27/2004		4/23/2005	
					Driving	Passing	Driving	Passing	Driving	Passing	Driving	Passing	Driving	Passing	Driving	Passing
118	1328+20	Round	Standard	12	-0.29	-0.35	-0.29	-0.02	-0.73	0.45	-0.10	-0.82	0.45	-0.05	0.17	0.62
110	1302+20	Round	Standard	12	-0.39	-0.16	-0.17	-0.59	-0.67	0.23	-0.57	-0.38	0.18	0.58	0.52	0.57
103	1277+00	Round	Standard	12	-0.10	-0.38	-0.28	-0.61	-0.20	0.47	-0.49	-0.79	0.19	0.20	0.47	0.78
101	1267+70	Round	Standard	12	-0.37	-0.46	-0.40	-0.70	-0.31	0.60	-0.55	-0.87	0.63	-0.37	0.31	0.61
100	1266+50	Round	Standard	12	-0.17	-0.16	-0.37	-0.40	-0.69	0.27	-0.40	-0.82	0.53	-0.39	0.40	0.74
91	1260+20	Round	Standard	12	-0.17	-0.33	-0.40	-0.46	-0.96	0.50	-0.29	-1.09	0.45	0.06	-0.05	0.85
73	1244+20	Round	Standard	12	-0.18	-0.82	-0.31	-0.71	-0.54	0.34	-0.33	-0.66	0.71	-0.21	0.49	0.67
71	1242+70	Round	Standard	12	-0.23	-0.69	-0.67	-0.88	-0.27	0.78	-0.25	-0.73	0.57	0.12	-0.16	0.53
69	1241+20	Round	Standard	12	-0.21	-0.52	-0.52	-0.90	-0.73	0.69	-0.41	-0.86	0.58	0.19	-0.31	0.57
6	1180+20	Round	Standard	12	-0.90	-0.64	-0.35	-0.79	-0.39	0.86	0.14	-1.14	0.88	0.05	0.67	-0.89
4	1178+70	Round	Standard	12	-0.41	-0.64	-0.56	-0.63	-0.45	0.89	-0.23	-0.83	0.76	0.34	0.62	-0.89
2	1177+20	Round	Standard	12	-0.74	-0.76	-0.65	-0.67	-0.13	0.91	-0.30	-0.71	1.20	0.27	0.98	-0.80
95	1262+80	Round	Standard	15	-0.57	-0.28	-0.60	-0.78	-0.67	0.68	-0.21	-1.12	0.07	-0.07	0.09	1.12
79	1249+70	Round	Standard	15	-0.23	-0.33	-0.18	-0.77	-0.82	1.08	-0.33	-0.95	0.28	-0.09	0.48	0.62
77	1247+70	Round	Standard	15	-0.71	-0.34	-0.69	-0.47	-0.50	0.92	0.11	-0.93	0.70	0.22	0.39	0.62
11	1184+70	Round	Standard	15	-0.55	-0.46	-0.44	-0.73	-0.62	1.05	-0.10	-1.32	0.97	0.30	0.58	-0.66
10	1183+20	Round	Standard	15	-0.08	-0.46	-0.18	-0.77	-0.35	0.91	-0.05	-0.83	0.66	0.42	0.67	-0.81
8	1181+70	Round	Standard	15	0.13	-0.47	-0.28	-0.81	-0.30	1.15	-0.02	-0.74	0.69	0.09	0.57	-0.80
106	1279+70	Round	Standard	18	-0.12	-0.58	-0.27	-0.30	-0.14	0.40	-0.60	-0.53	0.35	0.36	0.88	0.68
104	1278+20	Round	Standard	18	-0.26	-0.31	-0.14	-0.39	-0.64	0.52	-0.78	-0.82	0.18	0.48	0.58	1.23
97	1264+10	Round	Standard	18	0.12	-0.38	-0.47	-0.61	-0.65	0.44	-0.73	-0.80	0.78	-0.37	-0.11	0.73
17	1191+20	Round	Standard	18	-0.75	-0.56	-0.45	-0.61	-0.57	0.94	-0.48	-0.99	0.79	-0.27	0.42	-0.92
15	1189+70	Round	Standard	18	-0.51	-0.60	-0.52	-0.66	-0.53	0.61	-0.15	-0.88	1.03	-0.08	0.38	-1.04
13	1188+20	Round	Standard	18	-0.61	-0.35	-0.38	-0.92	-0.64	1.40	0.17	-0.99	0.63	0.34	0.74	-0.74
114	1319+70	Elliptical	Medium	12	0.00	-0.44	-0.18	-0.48	-0.11	0.41	-0.32	-0.70	0.83	-0.38	0.72	0.69
112	1318+20	Elliptical	Medium	12	-0.58	-0.38	-0.48	-0.67	-0.33	0.74	-0.23	-0.89	0.22	0.63	0.52	0.75
108	1281+20	Elliptical	Medium	12	-0.22	-0.63	-0.44	-0.60	-0.81	0.01	-0.50	-0.76	0.22	0.25	0.51	0.64
98	1265+20	Elliptical	Medium	12	-0.20	-0.14	-0.49	-0.57	-0.35	0.57	-0.17	-0.41	0.91	-0.27	0.59	0.63
93	1261+50	Elliptical	Medium	12	-0.49	-0.17	-0.31	-0.39	-1.01	0.85	-0.22	-1.01	0.87	0.49	0.26	0.95
89	1257+20	Elliptical	Medium	12	-0.14	-0.05	-0.18	-0.18	-0.69	0.48	-0.11	-1.03	0.62	-0.17	0.22	0.57
87	1255+70	Elliptical	Medium	12	-0.10	-0.39	-0.55	-0.14	-0.54	0.19	-0.49	-0.93	0.35	-0.57	0.31	-0.08
85	1254+20	Elliptical	Medium	12	0.13	-0.45	-0.44	-0.69	-0.53	0.00	-0.44	-0.66	0.83	-0.17	0.57	0.50
81	1251+20	Elliptical	Medium	12	-0.05	-0.43	-0.33	-0.82	-0.43	0.33	-0.37	-0.55	0.68	0.14	0.70	0.69
47	1220+20	Elliptical	Medium	12			-0.61	-0.73	-0.68	1.00	-0.15	-1.16	0.61	-0.08	-0.79	0.86
29	1202+70	Elliptical	Medium	12	-0.33	-0.19	-0.66	-0.90	-0.67	0.88	0.13	-0.88	0.82	0.50	0.50	-0.59
23	1195+70	Elliptical	Medium	12	-0.34	-0.27	-0.42	-0.45	-0.38	0.75	-0.40	-0.80	1.08	-0.22	0.87	-1.07
19	1192+70	Elliptical	Medium	12	-0.43	-0.78	-0.57	-0.51	-0.66	0.61	0.00	-0.98	0.61	0.03	0.72	-0.77
122	1333+70	Elliptical	Medium	15	-0.35	-0.13	-0.34	-0.25	-0.77	0.05	-0.55	-0.91	0.06	0.22	0.48	0.45
120	1332+20	Elliptical	Medium	15	-0.59	-0.03	-0.38	-0.57	-0.50	0.55	-0.23	-0.76	0.26	0.74	0.74	0.73
116	1321+20	Elliptical	Medium	15	-0.28	0.04	-0.14	-0.20	-0.80	0.37	-0.59	-0.94	0.42	-0.07	0.04	0.56
39	1214+20	Elliptical	Medium	15	-0.20	-0.06	-0.44	-0.26	-0.80	0.49	-0.21	-0.89	0.93	-0.17	-0.35	0.65
35	1210+20	Elliptical	Medium	15	-0.31	0.22	-0.11	-0.14	-0.51	0.67	0.02	-1.16	0.64	0.18	0.21	0.02
33	1207+20	Elliptical	Medium	15	-0.26	-0.11	-0.50	-0.78	-0.81	0.69	0.07	-1.02	0.81	-0.04	0.47	-0.91
128	1346+20	Elliptical	Medium	18	-0.47	-0.06	-0.26	-0.28	-0.83	0.72	-0.55	-1.38	0.20	-0.47	0.19	0.66
126	1344+70	Elliptical	Medium	18	-0.39	-0.01	-0.06	-0.30	-0.75	0.20	-0.51	-0.68	0.30	-0.50	0.37	0.48
124	1340+20	Elliptical	Medium	18	-0.09	-0.36	-0.22	-0.37	-0.66	0.44	-0.43	-1.06	-0.38	0.37	0.44	0.57
45	1218+70	Elliptical	Medium	18			-0.18	-0.77	-0.70	0.62	-0.25	-0.80	0.69	-0.16	-0.48	0.74
43	1217+20	Elliptical	Medium	18			-0.25	-0.92	-0.69	0.70	0.16	-0.98	0.53	-0.07	-0.58	0.61
41	1215+70	Elliptical	Medium	18	0.10	-0.05	-0.66	-0.46	-0.53	-0.16	-0.43	-1.06	0.54	-0.46	-0.38	0.53
55	1227+70	Elliptical	Heavy	12	-0.27	-0.46	-0.36	-0.83	-0.71	0.70	-0.06	-1.16	-0.29	0.91	-0.63	1.07
51	1224+70	Elliptical	Heavy	12	-0.43	-0.20	-0.65	-0.73	-0.37	0.78	0.06	-0.92	-0.42	1.17	-0.63	0.78
27	1199+70	Elliptical	Heavy	12	-0.61	-0.02	-0.20	-0.64	-0.38	1.13	-0.12	-0.98	0.64	0.22	0.75	-0.83
25	1198+20	Elliptical	Heavy	12	-0.05	0.26	-0.62	-0.79	-0.68	1.10	-0.41	-1.11	0.76	0.18	0.23	-1.13
21	1194+20	Elliptical	Heavy	12	-0.45	-0.40	-0.51	-0.60	-0.58	1.01	-0.24	-1.33	0.55	0.08	0.62	-0.95
63	1233+70	Elliptical	Heavy	15	-0.50	-0.29	-0.22	-0.17	-0.77	0.45	-0.29	-1.02	-0.18	0.71	-0.30	0.65
61	1232+20	Elliptical	Heavy	15	-0.09	-0.16	-0.40	-0.53	-0.79	0.62	-0.32	-1.02	0.09	0.70	-0.57	0.53
59	1230+70	Elliptical	Heavy	15	-0.03	0.00	-0.44	-0.50	-0.56	0.54	-0.29	-1.02	-0.22	1.04	-0.43	0.32
49	1223+20	Elliptical	Heavy	15	0.16	0.36	-0.48	-0.38	-0.79	0.34	-0.26	-1.41	-0.45	0.87	-0.75	0.27
37	1211+70	Elliptical	Heavy	15	-0.46	0.40	-0.47	-0.85	-0.71	0.59	0.01	-1.06	0.16	0.90	-0.42	0.76
31	1205+70	Elliptical	Heavy	15	-0.18	-0.14	-0.60	-0.93	-0.61	0.44	-0.17	-0.80	1.06	0.17	0.52	-0.90
83	1252+70	Elliptical	Heavy	18	-0.26	-0.36	-0.50	-0.48	-0.61	0.59	-0.06	-0.63	0.72	-0.23	0.49	0.65
75	1245+70	Elliptical	Heavy	18	0.05	-0.33	-0.63	-0.41	-0.19	0.58	-0.31	-0.54	0.77	-0.10	0.72	0.52
67	1239+70	Elliptical	Heavy	18	-0.47	-0.34			-0.42	0.74	-0.27	-0.46	0.92	0.03	0.18	0.67
65	1238+20	Elliptical	Heavy	18	-0.36	-0.13	-0.54	-0.36	-0.26	0.53	-0.06	-0.55	1.12	0.17	0.10	0.48
57	1229+20	Elliptical	Heavy	18	-0.12	0.11	-0.46	-0.66	-0.42	0.36	-0.10	-0.98	-0.47	0.68	-0.40	0.63
53	1226+20	Elliptical	Heavy	18	-0.37	-0.31	-0.70	-0.39	-0.38	0.58	0.01	-0.85	0.04	0.74	-0.04	0.58

Table F.3. Steel dowels, standard round faulting averages

Test Date	Faulting Averages (mm)								
	12 in. spacing			15 in. spacing			18 in. spacing		
	Driving	Passing	Average	Driving	Passing	Average	Driving	Passing	Average
Fall 2002	-0.35	-0.49	-0.42	-0.34	-0.39	-0.36	-0.36	-0.46	-0.41
Spring 2003	-0.41	-0.61	-0.51	-0.40	-0.72	-0.56	-0.37	-0.58	-0.48
Fall 2003	-0.51	0.58	0.04	-0.54	0.97	0.21	-0.53	0.72	0.09
Spring 2004	-0.32	-0.81	-0.56	-0.10	-0.98	-0.54	-0.43	-0.84	-0.63
Fall 2004	0.59	0.07	0.33	0.56	0.15	0.35	0.63	0.08	0.35
Spring 2005	0.34	0.28	0.31	0.46	0.02	0.24	0.48	-0.01	0.24

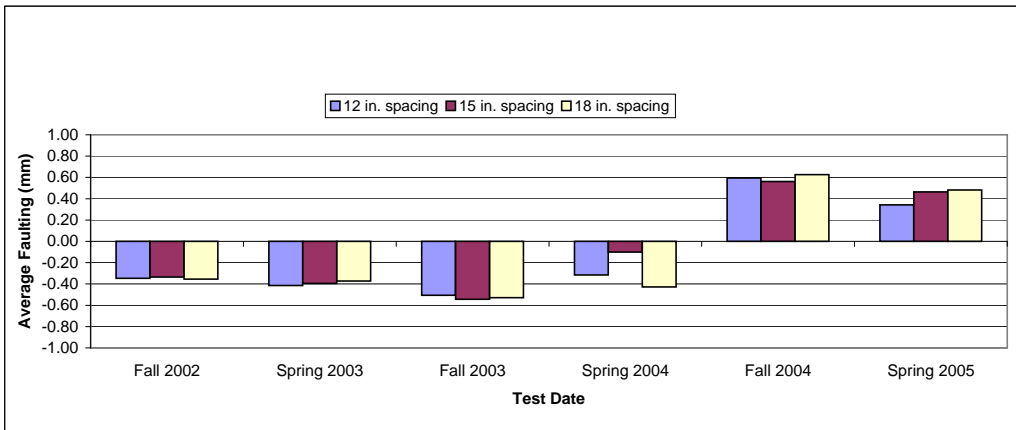


Figure F.1. Faulting averages, standard round steel dowels, driving lane

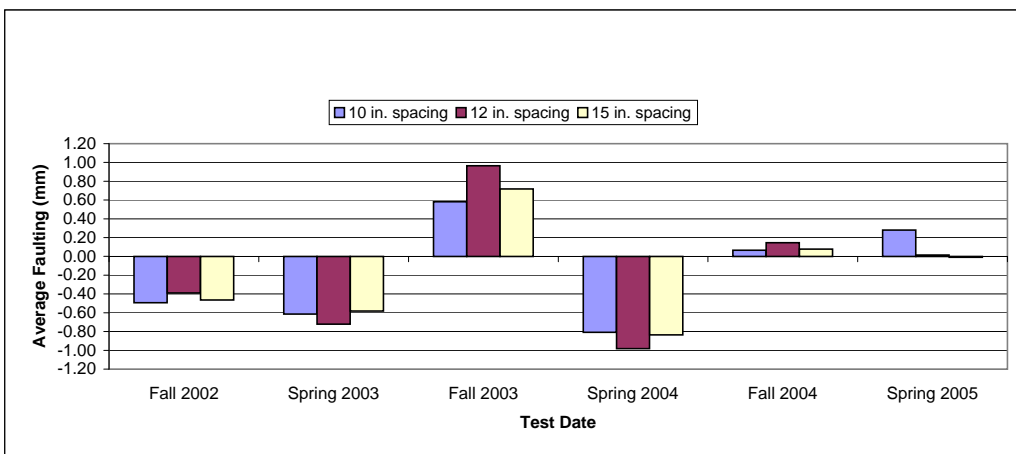


Figure F.2. Faulting averages, standard round steel dowels, passing lane

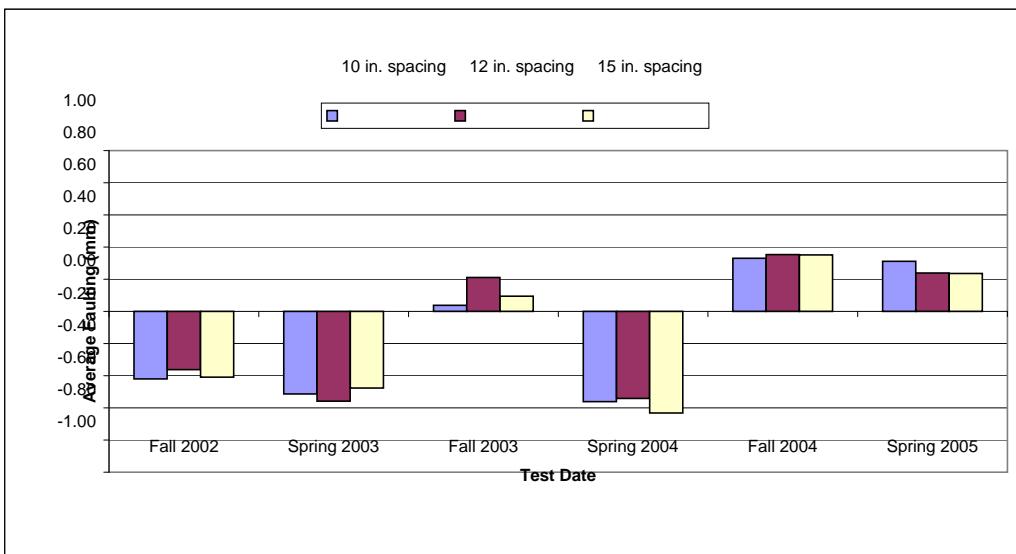


Figure F.3. Faulting averages, standard round steel dowels, average

Table F.4. Steel dowels, medium elliptical faulting averages

Test Date	Faulting Averages (mm)								
	12 in. spacing			15 in. spacing			18 in. spacing		
	Driving	Passing	Average	Driving	Passing	Average	Driving	Passing	Average
Fall 2002	-0.23	-0.36	-0.29	-0.33	-0.01	-0.17	-0.21	-0.12	-0.17
Spring 2003	-0.44	-0.55	-0.49	-0.32	-0.37	-0.34	-0.52	-0.52	-0.39
Fall 2003	-0.55	0.52	-0.01	-0.70	0.47	-0.11	-0.69	0.42	-0.14
Spring 2004	-0.25	-0.83	-0.54	-0.25	-0.95	-0.60	-0.34	-0.99	-0.66
Fall 2004	0.67	0.01	0.34	0.52	0.14	0.33	0.31	-0.22	0.05
Spring 2005	0.44	0.29	0.36	0.27	0.25	0.26	-0.07	0.60	0.26

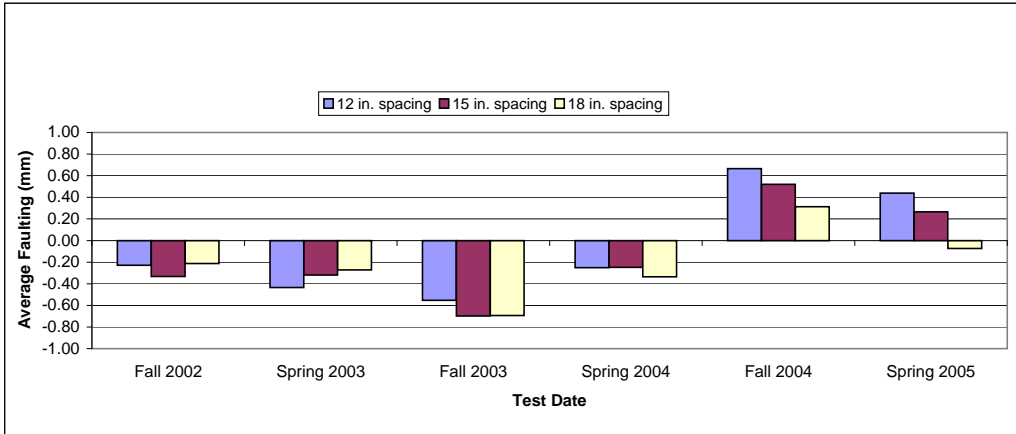


Figure F.4. Faulting averages, medium elliptical steel dowels, driving lane

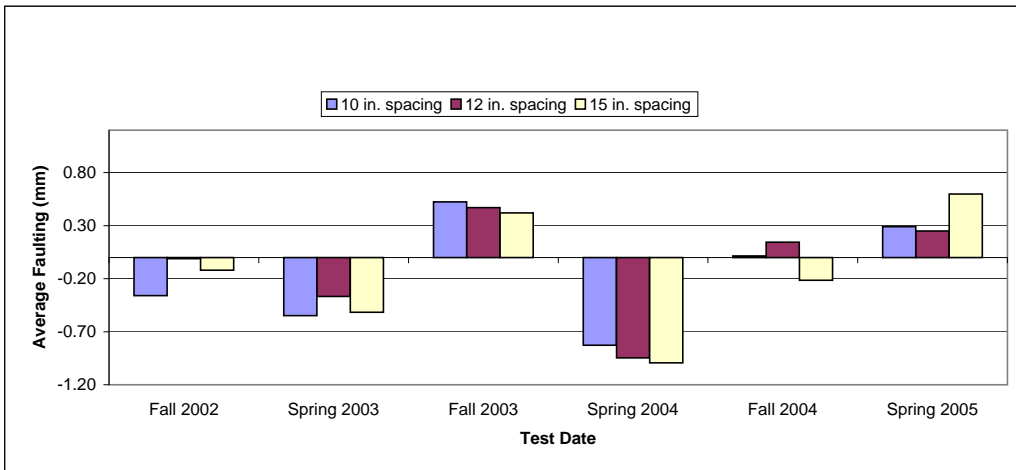


Figure F.5. Faulting averages, medium elliptical steel dowels, passing lane

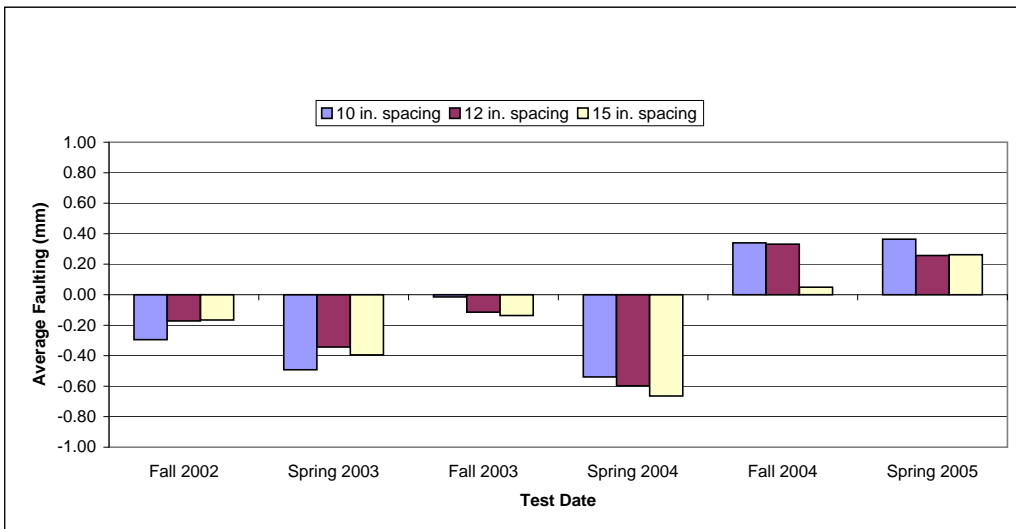


Figure F.6. Faulting averages, medium elliptical steel dowels, average

Table F.5. Steel dowels, heavy elliptical faulting averages

Test Date	Faulting Averages (mm)								
	12 in. spacing			15 in. spacing			18 in. spacing		
	Driving	Passing	Average	Driving	Passing	Average	Driving	Passing	Average
Fall 2002	-0.36	-0.16	-0.26	-0.18	0.03	-0.08	-0.26	-0.23	-0.24
Spring 2003	-0.47	-0.72	-0.59	-0.44	-0.56	-0.50	-0.57	-0.46	-0.51
Fall 2003	-0.54	0.94	0.20	-0.71	0.50	-0.10	-0.38	0.56	0.09
Spring 2004	-0.15	-1.10	-0.63	-0.22	-1.06	-0.64	-0.13	-0.67	-0.40
Fall 2004	0.25	0.51	0.38	0.08	0.73	0.40	0.52	0.22	0.37
Spring 2005	0.07	-0.21	-0.07	-0.33	0.27	-0.03	0.18	0.59	0.38

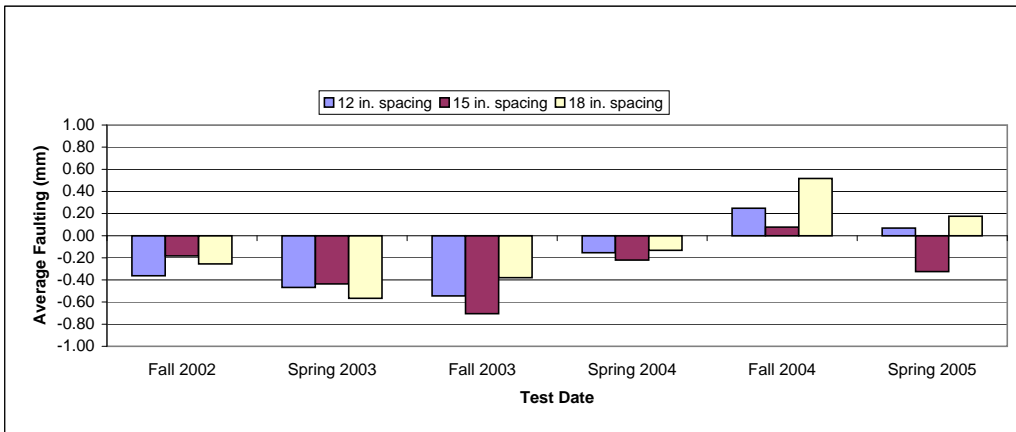


Figure F.7. Faulting averages, heavy elliptical steel dowels, driving lane

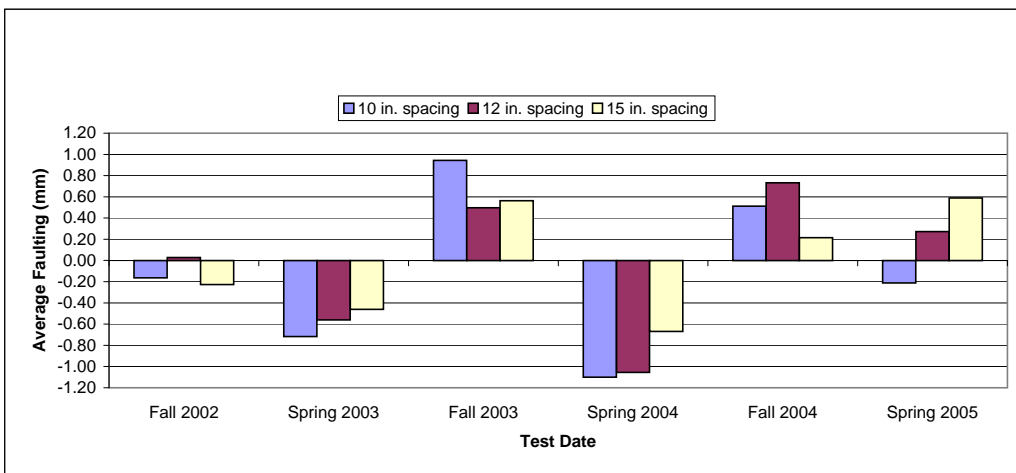


Figure F.8. Faulting averages, heavy elliptical steel dowels, passing lane

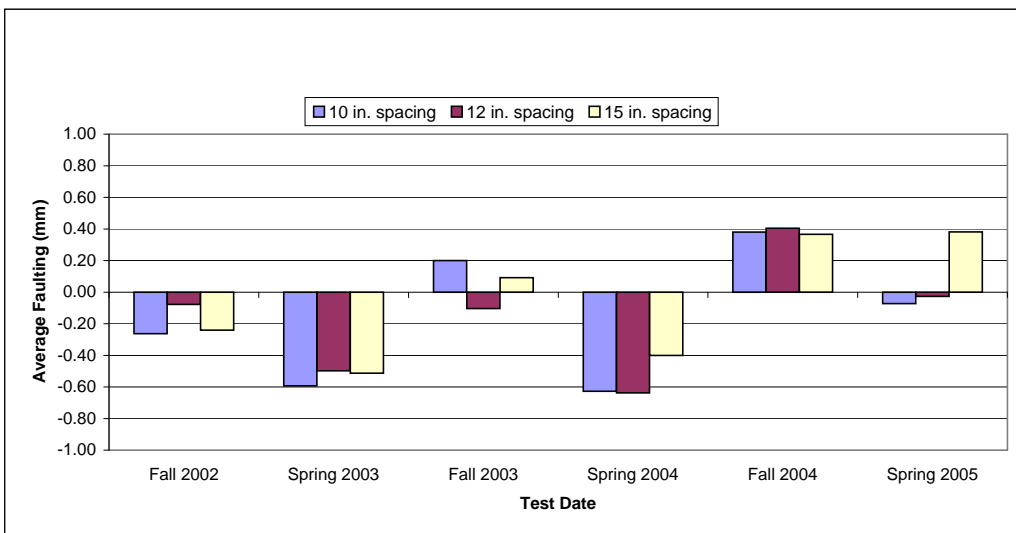


Figure F.9. Faulting averages, heavy elliptical steel dowels, average

APPENDIX G. JOINT OPENING DATA FOR STEEL

Table G.1.1. Steel dowels, joint opening field measurements

Notes: 1. All tests were taken in the northbound (south) lane.
 2. Measurements were made between nails installed 12 inches from the edge of pavement.
 3. Temperatures are measured in Degrees Fahrenheit.

Test Sect. Station Ref. EOP	Station (inches)	Bar Shape	Bar Size	Spacing (inches)	Joint Opening Measurements (mm)										Change in Joint Opening (mm)										
					8/28/2002	9/25/2002	10/25/2003	4/10/2004	8/27/2004	12/29/2005	9/21/2002	4/5/2003	10/25/2003	4/10/2004	8/27/2004	4/23/2005									
					Dist.	Temp.	Dist.	Temp.	Dist.	Temp.	Dist.	Temp.	Dist.	Temp.	Dist.	Temp.	Dist.	Temp.							
108	1280+47	Elliptical	Medium	12	254	255	252	252	256	255	253	253	253	253	253	250	250	250	250	1.9	1.9	0.7	-1.5	-4.3	
	1280+81	Elliptical	Medium	12	252	253	250	250	253	253	251	251	251	251	251	251	251	251	251	251	1.1	1.1	1.3	-1.2	-0.7
	1280+75	Elliptical	Medium	12	254	255	252	252	256	255	253	253	253	253	253	253	253	253	253	253	1.5	1.5	0.9	-0.3	-0.7
	1280+69	Elliptical	Medium	12	259	259	259	259	261	260	260	260	260	260	260	260	260	260	260	260	1.8	1.8	0.9	-0.3	-0.7
	1280+63	Elliptical	Medium	12	261	261	261	261	261	261	261	261	261	261	261	261	261	261	261	261	1.8	1.8	0.2	-1.2	-1.8
	1280+57	Elliptical	Medium	12	250	250	250	250	258	258	258	258	258	258	258	258	258	258	258	258	0.8	0.8	0.2	-0.2	-0.9
	1280+51	Elliptical	Medium	12	267	267	267	267	270	267	267	267	267	267	267	267	267	267	267	267	2.4	2.4	0.5	-0.7	-0.5
	1280+45	Elliptical	Medium	12	251	253	253	253	253	253	253	253	253	253	253	253	253	253	253	253	2.0	2.0	1.3	-0.3	0.3
	1280+39	Elliptical	Medium	12	247	247	247	247	249	249	249	249	249	249	249	249	249	249	249	249	1.7	1.7	0.1	-1.3	-6.1
	1280+33	Elliptical	Medium	12	248	248	248	248	249	249	249	249	249	249	249	249	249	249	249	249	1.7	1.7	-0.1	-1.3	-1.7
106	1279+38	Round	Standard	18	260	261	261	261	262	262	262	262	262	262	262	262	262	262	262	2.0	2.0	0.2	1.3	-0.8	
	1279+32	Round	Standard	18	248	249	249	249	250	250	250	250	250	250	250	250	250	250	250	2.0	2.0	1.1	0.3	-0.9	
	1279+26	Round	Standard	18	252	252	252	252	253	253	253	253	253	253	253	253	253	253	253	1.1	1.1	0.3	-1.9	-0.7	
	1279+20	Round	Standard	18	276	276	276	276	268	268	268	268	268	268	268	268	268	268	268	4.3	4.3	-7.9	-8.6	-10.8	
	1279+14	Round	Standard	18	253	253	253	253	253	253	253	253	253	253	253	253	253	253	253	2.5	2.5	0.5	-0.5	-2.8	
	1279+08	Round	Standard	18	266	266	266	266	266	266	266	266	266	266	266	266	266	266	266	2.4	2.4	0.1	-1.6	0.1	
	1279+02	Round	Standard	18	252	253	253	253	254	254	254	254	254	254	254	254	254	254	254	1.9	1.9	0.0	-1.4	-1.0	
	1278+96	Round	Standard	18	254	254	254	254	254	254	254	254	254	254	254	254	254	254	254	2.0	2.0	0.3	0.0	-2.5	
	1278+90	Round	Standard	18	253	254	254	254	254	254	254	254	254	254	254	254	254	254	254	1.0	1.0	0.8	-1.4	-1.2	
	1278+84	Round	Standard	18	244	245	245	245	245	245	245	245	245	245	245	245	245	245	245	1.3	1.3	-1.5	0.4	-1.4	
104	1277+89	Round	Standard	18	238	240	240	240	240	240	240	240	240	240	240	240	240	240	240	2.0	2.0	1.6	0.1	-0.3	
	1277+83	Round	Standard	18	231	232	232	232	232	232	232	232	232	232	232	232	232	232	232	1.6	1.6	0.8	-0.7	-2.0	
	1277+77	Round	Standard	18	246	246	246	246	246	246	246	246	246	246	246	246	246	246	246	1.1	1.1	0.4	0.4	-0.9	
	1277+71	Round	Standard	18	241	241	241	241	241	241	241	241	241	241	241	241	241	241	241	1.1	1.1	0.4	0.4	-0.9	
	1277+65	Round	Standard	18	238	238	238	238	238	238	238	238	238	238	238	238	238	238	238	1.1	1.1	0.4	0.4	-0.9	
	1277+59	Round	Standard	18	238	237	237	237	235	237	237	237	237	237	237	237	237	237	237	1.1	1.1	0.4	0.4	-0.9	
	1277+53	Round	Standard	18	243	243	243	243	244	244	244	244	244	244	244	244	244	244	244	1.1	1.1	0.4	0.4	-0.9	
	1277+47	Round	Standard	18	242	242	242	242	242	242	242	242	242	242	242	242	242	242	242	1.1	1.1	0.4	0.4	-0.9	
	1277+41	Round	Standard	18	250	253	253	253	251	251	251	251	251	251	251	251	251	251	251	1.4	1.4	0.4	0.4	-0.9	
	1277+35	Round	Standard	18	246	247	247	247	247	247	247	247	247	247	247	247	247	247	247	1.4	1.4	0.4	0.4	-0.9	
103	1276+65	Round	Standard	12	252	251	251	251	250	250	250	250	250	250	250	250	250	250	250	2.0	2.0	1.6	0.1	-0.3	
	1276+59	Round	Standard	12	238	240	240	240	240	240	240	240	240	240	240	240	240	240	240	2.0	2.0	1.6	0.1	-0.3	
	1276+53	Round	Standard	12	245	245	245	245	245	245	245	245	245	245	245	245	245	245	245	1.6	1.6	0.8	-0.7	-2.0	
	1276+47	Round	Standard	12	244	244	244	244	245	245	245	245	245	245	245	245	245	245	245	1.6	1.6	0.8	-0.7	-2.0	
	1276+41	Round	Standard	12	246	246	246	246	245	245	245	245	245	245	245	245	245	245	245	1.6	1.6	0.8	-0.7	-2.0	
	1276+35	Round	Standard	12	242	242	242	242	245	245	245	245	245	245	245	245	245	245	245	1.6	1.6	0.8	-0.7	-2.0	
	1276+29	Round	Standard	12	242	242	242	242	244	244	244	244	244	244	244	244	244	244	244	1.6	1.6	0.8	-0.7	-2.0	
	1276+23	Round	Standard	12	245	245	245	245	247	247	247	247	247	247	247	247	247	247	247	1.6	1.6	0.8	-0.7	-2.0	
	1276+17	Round	Standard	12	240	240	240	240	241	241	241	241	241	241	241	241	241	241	241	1.6	1.6	0.8	-0.7	-2.0	
	1276+11	Round	Standard	12	247	247	247	247	246	246	246	246	246	246	246	246	246	246	246	1.6	1.6	0.8	-0.7	-2.0	
101	1267+37	Round	Standard	12	251	255	255	255	252	252	252	252	252	252	252	252	252	252	252	5.0	5.0	3.3	-2.1	-1.9	
	1267+31	Round	Standard	12	257	257	257	257	256	256	256	256	256	256	256	256	256	256	256	3.0	3.0	-1.0	-1.0	-2.2	
	1267+25	Round	Standard	12	262	263	263	263	264	264	264	264	264	264	264	264	264	264	264	1.5	1.5	0.9	-2.1	-1.1	
	1267+19	Round	Standard	12	258	258	258	258	258	258	258	258	258	258	258	258	258	258	258	2.6	2.6	0.9	-2.6	-1.1	
	1267+13	Round	Standard	12	257	257	257	257	258	258	258	258	258	258	258	258	258	258	258	2.6	2.6	0.9	-2.6	-1.1	
	1267+07	Round	Standard	12	247	248	248	248	249	249	249	249	249	249	249	249	249	249	249	2.6	2.6	0.9	-2.6	-1.1	
	1266+95	Round	Standard	12	250	251	251	251	251	251	251	251	251	251	251	251	251	251	251	1.4	1.4	-0.1	-1.4	-0.9	
	1266+89	Round	Standard	12	256	256	256	256	256	256	256	256	256	256	256	256	256	256	256	1.8	1.8	-0.3	-1.4	-2.8	
	1266+83	Round	Standard	12	248	249	249	249	249	249	249	249	249	249	249	249	249	249	249	1.2	1.2	-0.2	-2.5	-2.2	
	1266+77	Round	Standard	12	248	248	248	248	246	246	246	246	246	246	246	246	246	246	246	1.5	1.5	-0.9	-2.5	-2.5	
100	1266+16	Round	Standard	12	267	267	267	267	266	266	266	266	266	266	266	266	266	266	266	5.0	5.0	3.3	-2.1	-1.9	
	1266+10	Round	Standard	12	265	266	266	266	266	266	266	266	266	266	266	266	266	266	266	2.6	2.6	1.0	-2.8	-2.0	
	1265+98	Round	Standard	1																					

1238+38	Heavy	Elliptical	18	238	61	239	66	238	31	239	52	237	48	237	71	201	45	-0.3	-1.5	0.3	-2.0	-2.0	-38.0
1239+32	Heavy	Elliptical	18	226	61	226	66	225	31	226	52	226	48	224	71	188	45	-0.3	-1.2	0.6	0.2	-1.4	-37.6
1239+26	Heavy	Elliptical	18	218	61	218	66	217	31	218	52	217	48	216	71	180	45	0.0	-1.6	0.0	-1.2	-1.7	-38.2
1239+14	Heavy	Elliptical	18	248	61	249	66	244	31	247	52	246	48	244	71	209	45	0.8	-3.8	-0.7	-2.2	-4.6	-39.2
1239+10	Heavy	Elliptical	18	237	61	237	66	236	31	237	52	235	48	234	71	203	45	0.3	-3.0	1.4	-2.0	-2.8	-32.0
1239+02	Heavy	Elliptical	18	227	61	227	66	226	31	227	52	225	48	224	71	188	45	-0.2	-1.6	-0.4	-2.6	-2.6	-36.6
1238+96	Heavy	Elliptical	18	231	61	231	66	230	31	231	52	230	48	229	71	194	45	0.0	-1.0	1.9	-0.9	-0.9	-36.9
1238+90	Heavy	Elliptical	18	245	61	245	66	244	31	245	52	244	48	243	71	207	45	0.5	-1.0	1.1	-0.9	-1.9	-37.9
1238+84	Heavy	Elliptical	18	249	61	249	66	247	31	249	52	246	48	247	71	211	45	-1.0	-1.7	-0.1	-2.7	-1.6	-37.7
1237+84	Heavy	Elliptical	18	276	58	277	65	273	34	277	52	273	48	274	71	237	45	1.0	-2.5	1.6	-2.8	-1.7	-38.5
1237+78	Heavy	Elliptical	18	263	58	264	65	261	34	265	52	260	48	260	71	224	45	1.3	-1.2	1.9	-2.6	-2.4	-38.6
1237+72	Heavy	Elliptical	18	274	58	274	65	274	34	276	52	274	48	274	71	236	45	0.8	-0.3	1.7	-0.3	-0.2	-38.3
1237+66	Heavy	Elliptical	18	280	58	280	65	277	34	280	52	277	48	276	71	240	45	0.0	-3.5	0.3	-3.2	-4.1	-40.2
1237+60	Heavy	Elliptical	18	285	58	285	65	282	34	286	52	283	48	282	71	225	45	0.0	-2.6	0.9	-1.7	-2.8	-38.7
1237+54	Heavy	Elliptical	18	288	58	289	65	286	34	290	52	287	48	286	71	230	45	0.8	-2.7	1.4	-1.2	-1.9	-38.2
1237+48	Heavy	Elliptical	18	296	58	296	65	294	34	297	52	294	48	294	71	246	45	0.8	-1.8	1.0	-1.6	-1.8	-38.1
1237+42	Heavy	Elliptical	18	286	58	286	65	284	34	287	52	284	48	284	71	241	45	-0.3	-1.9	1.0	-1.8	-1.8	-38.2
1237+36	Heavy	Elliptical	18	281	58	281	65	279	34	282	52	280	48	278	71	241	45	0.3	-2.0	1.0	-1.2	-3.0	-40.2
1237+30	Heavy	Elliptical	18	274	58	273	65	271	34	274	52	271	48	271	71	233	45	-0.8	-2.8	-0.3	-3.1	-3.0	-41.1
1233+37	Heavy	Elliptical	15	264	60	266	65	255	34	265	51	262	48	262	72	225	43	1.8	-8.4	0.9	-1.9	-2.0	-38.5
1233+31	Heavy	Elliptical	15	279	60	278	65	276	34	278	51	276	48	276	72	239	43	-1.0	-2.9	-0.4	-1.9	-3.2	-39.9
1233+25	Heavy	Elliptical	15	282	60	281	65	280	34	283	51	279	48	280	72	242	43	-1.3	-1.6	1.5	-2.9	-2.2	-39.9
1233+19	Heavy	Elliptical	15	264	60	263	65	261	34	265	51	262	48	262	72	224	43	-1.3	-2.9	0.1	-2.4	-2.9	-40.4
1233+13	Heavy	Elliptical	15	276	60	275	65	272	34	277	51	274	48	275	72	237	43	-0.8	-3.5	1.8	-1.6	-0.8	-38.6
1233+07	Heavy	Elliptical	15	287	60	286	65	284	34	287	51	283	48	283	72	246	43	-1.3	-3.1	-0.1	-4.3	-4.4	-41.3
1233+01	Heavy	Elliptical	15	276	60	276	65	273	34	277	51	270	48	275	72	237	43	-0.8	-3.0	0.4	-6.4	-6.4	-48.4
1232+95	Heavy	Elliptical	15	272	60	272	65	268	34	274	51	270	48	270	72	232	43	0.5	-1.6	0.5	-2.5	-2.5	-38.5
1232+89	Heavy	Elliptical	15	261	60	261	65	258	34	262	51	257	48	261	72	227	43	-1.6	-1.6	1.1	-1.1	-1.1	-38.1
1232+83	Heavy	Elliptical	15	259	60	257	65	255	34	259	51	255	48	256	72	219	43	-2.5	6.0	0.1	-4.1	-2.8	-40.1
1231+87	Heavy	Elliptical	15	283	60	282	65	280	34	282	51	278	48	280	72	243	43	-3.0	-3.2	-0.5	-3.7	-3.0	-39.7
1231+81	Heavy	Elliptical	15	280	60	277	65	276	34	280	51	276	48	276	72	240	43	-2.3	-3.0	0.2	-2.2	-1.9	-39.7
1231+75	Heavy	Elliptical	15	270	60	269	65	269	34	271	51	269	48	269	72	231	43	0.4	-1.7	0.4	-1.3	-1.5	-39.1
1231+69	Heavy	Elliptical	15	264	60	264	65	262	34	265	51	262	48	261	72	225	43	-0.8	-2.1	0.2	-2.4	-3.1	-39.4
1231+63	Heavy	Elliptical	15	277	60	276	65	275	34	278	51	275	48	275	72	238	43	-1.0	-2.2	0.7	-2.1	-2.4	-39.4
1231+57	Heavy	Elliptical	15	248	60	249	65	247	34	250	51	247	48	245	72	211	43	0.8	-1.0	1.8	-0.9	-3.0	-36.9
1231+51	Heavy	Elliptical	15	238	60	239	65	237	34	239	51	233	48	236	72	201	43	0.5	-1.0	0.4	-5.3	-1.8	-37.3
1231+45	Heavy	Elliptical	15	251	60	253	65	249	34	252	51	248	48	250	72	213	43	1.5	-2.0	0.5	-3.5	-1.2	-38.5
1231+39	Heavy	Elliptical	15	251	60	251	65	248	34	251	51	248	48	250	72	212	43	0.5	-1.6	0.5	-4.4	-0.2	-38.5
1231+33	Heavy	Elliptical	15	246	60	247	65	246	34	246	51	245	48	246	72	209	43	-0.3	-1.4	0.1	-2.5	-1.7	-38.5
1230+36	Heavy	Elliptical	15	243	65	242	65	240	36	243	53	241	48	242	70	204	46	-0.3	-1.6	1.1	-2.9	-2.4	-38.9
1230+30	Heavy	Elliptical	15	250	65	248	65	247	36	249	53	247	48	248	70	211	46	-1.5	-3.3	-0.5	-2.9	-2.4	-38.9
1230+24	Heavy	Elliptical	15	245	65	245	65	244	36	246	53	243	48	244	70	206	46	0.3	-1.6	1.2	-2.1	-1.5	-39.1
1230+18	Heavy	Elliptical	15	244	65	245	65	240	36	244	53	243	48	243	70	206	46	0.8	-4.2	-0.2	-1.3	-1.5	-38.3
1230+12	Heavy	Elliptical	15	247	65	247	65	245	36	247	53	243	48	246	70	210	46	0.8	-1.3	-0.8	-3.6	-0.6	-39.6
1230+06	Heavy	Elliptical	15	229	65	229	65	229	36	229	53	225	48	226	70	190	46	-0.3	-0.2	0.7	-4.4	-3.0	-39.4
1230+00	Heavy	Elliptical	15	241	65	241	65	238	36	241	53	236	48	238	70	202	46	-0.3	-2.7	-0.2	-4.8	-2.4	-38.6
1229+94	Heavy	Elliptical	15	236	65	236	65	237	36	236	53	234	48	232	70	197	46	-1.5	1.5	-0.3	-2.0	-4.0	-38.0
1229+88	Heavy	Elliptical	15	257	65	256	65	255	36	258	53	255	48	256	70	220	46	-0.3	-1.2	1.0	-1.5	-1.0	-38.5
1229+82	Heavy	Elliptical	15	242	65	242	65	240	36	242	53	240	48	240	70	204	46	-1.0	-1.5	0.3	-2.2	-2.2	-37.8
1228+85	Heavy	Elliptical	18	237	70	237	66	235	34	238	53	237	48	237	70	205	46	0.0	-1.1	0.0	0.5	-0.3	-37.8
1228+79	Heavy	Elliptical	18	233	70	232	66	232	34	233	53	230	48	231	70	195	46	-1.0	-4.0	-0.3	-4.0	-0.8	-38.0
1228+73	Heavy	Elliptical	18	237	70	235	66	235	34	234	53	233	48	231	70	219	46	2.5	0.8	1.7	0.3	-1.5	-36.7
1228+67	Heavy	Elliptical	18	233	70	235	66	234	34	234	53	233	48	231	70	196	46	0.8	-3.9	-2.1	-5.6	-4.4	-39.6
1228+61	Heavy	Elliptical	18	259	70	N/A	66	255	34	256	53	253	48	254	70	219	46	0.0	-1.8	0.6	1.5	0.0	-37.5
1228+55	Heavy	Elliptical	18	228	70	N/A	66	227	34	228	53	226	48	226	70	190	46	-0.6	-0.6	0.9	-1.6	-1.5	-37.6
1228+49	Heavy	Elliptical	18	241	70	242	66	240	34	242	53	239	48	238	70	204	46	1.0	-1.0	0.9	-1.8	-2.4	-36.8
1228+43	Heavy	Elliptical	18	241	70	241	66	239	34	240	53	238	48	238	70	202	46	0.5	-1.7	-1.1	-2.8	-3.0	-38.6
1228+37	Heavy	Elliptical	18	256	70	258	66	254	34	256	53	253	48	253	70	217	46	2.8	-1.7	0.2	-2.5	-2.1	-38.5
1228+31	Heavy	Elliptical	18	240	70	241	66	238	34	240	53	238	48	238	70	202	46	1.0	-1.9	0.3	-2.0	-1.8	-38.0
1227+35	Heavy	Elliptical	12	241	65	240	65	239	40	242	53	240	55	239	72	203	56	-1.3	-2.7	0.3	-1.3	1.9	-38.3
1227+29	Heavy	Elliptical	12	240	65	240	65	238	40	240	53	238	55	238	72	202	56	-1.0	0.8	1.0	-1.7	-2.1	-38.7
1227+23	Heavy	Elliptical	12	238	65	238	65	235	40	239	53	238	55	237	72	201	56	-1.8	-2.7	-0.7	-2.5	-3.4	-39.0
1227+17	Heavy	Elliptical	12	256	65	254	65	253	40	255	53	253	55	252	72	216	56	0.0	-1.8	0.6	1.5	0.0	-37.5
1227+11	Heavy	Elliptical	12	241	65	241	65	239	40	241	53	242	55	241	72	203	56	0.0	-1.8	0.6	1.5	0.0	-37.5
1227+05	Heavy	Elliptical	12	252	65	252	6																

Table G.2. Steel dowels, average change in joint opening

Section No.	Station	Bar Type	Bar Size	Spacing (inches)	Average Change in Joint Opening (mm)					
					9/21/2002	4/5/2003	10/25/2003	4/10/2004	8/27/2004	4/23/2005
118	1328+20	Round	Standard	12	NO NAILS	NO NAILS	NO NAILS	NO NAILS	NO NAILS	NO NAILS
110	1302+20	Round	Standard	12	NO NAILS	NO NAILS	NO NAILS	NO NAILS	NO NAILS	NO NAILS
103	1277+00	Round	Standard	12	1.0	-0.9	1.1	0.4	-10.7	0.1
101	1267+70	Round	Standard	12	0.7	-2.5	1.3	-0.4	-2.1	-1.7
100	1266+50	Round	Standard	12	1.6	-1.8	2.0	0.2	-1.1	-1.0
91	1260+20	Round	Standard	12	-2.2	-2.2	1.2	0.1	-1.9	-1.6
73	1244+20	Round	Standard	12	-0.7	-4.0	-0.4	-2.0	-4.4	-
71	1242+70	Round	Standard	12	0.5	-2.6	1.2	-1.8	-3.0	-
69	1241+20	Round	Standard	12	0.4	-2.7	0.8	-2.2	-3.9	-
6	1180+20	Round	Standard	12	0.7	-1.0	-0.4	-0.5	-2.2	-1.8
4	1178+70	Round	Standard	12	0.3	-1.8	-0.8	-0.5	-2.0	-2.9
2	1177+20	Round	Standard	12	-0.1	-2.6	-0.9	-0.9	-2.6	-3.0
95	1262+80	Round	Standard	15	0.2	-2.6	1.6	-0.5	-1.6	-1.3
79	1249+70	Round	Standard	15	0.8	-2.4	4.6	0.1	-1.9	-
77	1247+70	Round	Standard	15	0.9	-2.6	1.5	-0.4	-1.7	-
11	1184+70	Round	Standard	15	0.3	-1.7	-0.7	-0.4	-2.4	-2.4
10	1183+20	Round	Standard	15	0.2	-2.5	-0.9	1.9	-2.1	-2.6
8	1181+70	Round	Standard	15	1.6	-2.4	-0.2	0.3	-2.9	-1.9
106	1279+70	Round	Standard	18	-0.2	-2.4	0.5	-0.6	-2.5	-1.5
104	1278+20	Round	Standard	18	1.1	-0.6	1.4	0.8	-0.5	-0.7
97	1264+10	Round	Standard	18	1.0	-2.7	1.4	-0.2	-1.9	-1.3
17	1191+20	Round	Standard	18	-0.4	-2.4	-0.9	-1.5	-3.1	-3.0
15	1189+70	Round	Standard	18	-0.3	-1.9	-0.9	-0.5	-3.0	-2.9
13	1188+20	Round	Standard	18	0.7	-1.6	-0.2	0.0	-2.1	-2.3
114	1319+70	Elliptical	Medium	12	NO NAILS	NO NAILS	NO NAILS	NO NAILS	NO NAILS	NO NAILS
112	1318+20	Elliptical	Medium	12	NO NAILS	NO NAILS	NO NAILS	NO NAILS	NO NAILS	NO NAILS
108	1281+20	Elliptical	Medium	12	1.0	-1.5	2.3	0.5	-1.0	-1.6
98	1265+20	Elliptical	Medium	12	0.9	-2.5	1.6	-0.2	-1.4	-2.3
93	1261+50	Elliptical	Medium	12	0.3	-2.5	1.6	-0.6	-0.6	-1.1
89	1257+20	Elliptical	Medium	12	0.6	-1.5	0.5	-0.4	-1.8	-1.2
87	1255+70	Elliptical	Medium	12	1.5	0.3	0.8	0.1	-1.5	-0.4
85	1254+20	Elliptical	Medium	12	1.4	-1.5	0.6	0.1	-1.5	-1.4
81	1251+20	Elliptical	Medium	12	0.7	-2.4	1.7	-0.2	-2.7	-
47	1220+20	Elliptical	Medium	12						
29	1202+70	Elliptical	Medium	12	0.3	-2.3	-0.3	-0.9	-2.2	-2.5
23	1195+70	Elliptical	Medium	12	0.0	-2.6	-1.4	-1.5	-2.5	-3.3
19	1192+70	Elliptical	Medium	12	0.1	-2.4	-1.1	-0.8	-2.7	-2.9
122	1333+70	Elliptical	Medium	15	NO NAILS	NO NAILS	NO NAILS	NO NAILS	NO NAILS	NO NAILS
120	1332+20	Elliptical	Medium	15	NO NAILS	NO NAILS	NO NAILS	NO NAILS	NO NAILS	NO NAILS
116	1321+20	Elliptical	Medium	15	NO NAILS	NO NAILS	NO NAILS	NO NAILS	NO NAILS	NO NAILS
39	1214+20	Elliptical	Medium	15	0.1	-2.1	-0.4	-1.8	-2.6	-2.6
35	1210+20	Elliptical	Medium	15	-0.4	-2.6	-0.8	-1.8	-3.0	-3.7
33	1207+20	Elliptical	Medium	15	-0.4	-2.2	-0.1	-2.3	-3.1	-3.0
128	1346+20	Elliptical	Medium	18	NO NAILS	NO NAILS	NO NAILS	NO NAILS	NO NAILS	NO NAILS
126	1344+70	Elliptical	Medium	18	NO NAILS	NO NAILS	NO NAILS	NO NAILS	NO NAILS	NO NAILS
124	1340+20	Elliptical	Medium	18	NO NAILS	NO NAILS	NO NAILS	NO NAILS	NO NAILS	NO NAILS
45	1218+70	Elliptical	Medium	18						
43	1217+20	Elliptical	Medium	18						
41	1215+70	Elliptical	Medium	18	-0.2	-2.6	-0.5	-1.8	-2.4	-3.0
55	1227+70	Elliptical	Heavy	12	0.0	-1.6	0.2	-1.4	-1.4	-
51	1224+70	Elliptical	Heavy	12	0.4	-2.1	-0.3	-2.1	-1.9	-
27	1199+70	Elliptical	Heavy	12	-0.1	-0.1	-1.6	0.0	-1.8	-1.5
25	1198+20	Elliptical	Heavy	12	-0.1	-2.3	-1.2	-2.1	-3.3	-3.4
21	1194+20	Elliptical	Heavy	12	0.3	-1.9	-0.7	-1.6	-2.4	-2.6
63	1233+70	Elliptical	Heavy	15	-0.8	-2.3	0.6	-2.9	-2.4	-
61	1232+20	Elliptical	Heavy	15	-0.2	-2.3	0.4	-2.6	-2.1	-
59	1230+70	Elliptical	Heavy	15	-0.1	-1.6	0.2	-2.2	-1.9	-
49	1223+20	Elliptical	Heavy	15	0.6	-1.4	0.4	-1.8	-1.5	-
37	1211+70	Elliptical	Heavy	15	-0.1	-2.4	-0.2	-1.8	-2.4	-2.9
31	1205+70	Elliptical	Heavy	15	-0.3	-2.3	-0.7	-1.5	-3.1	-3.0
83	1252+70	Elliptical	Heavy	18	-0.2	-3.4	1.0	-0.6	-2.7	-2.7
75	1245+70	Elliptical	Heavy	18	0.5	-2.8	1.1	-0.7	-2.9	-
67	1239+70	Elliptical	Heavy	18	0.0	-1.7	0.5	-1.5	-2.7	-
65	1238+20	Elliptical	Heavy	18	0.3	-2.2	1.0	-1.9	-2.3	-
57	1229+20	Elliptical	Heavy	18	0.9	-1.6	0.0	-2.3	-2.0	-
53	1226+20	Elliptical	Heavy	18	0.2	-1.5	0.3	-6.0	-1.5	-

Table G.3. Steel dowels, change in joint opening, section averages

Bar Type	Spacing (inches)	Change in Joint Opening - Section Averages (mm)					
		Fall 2002	Spring 2003	Fall 2003	Spring 2004	Fall 2004	Spring 2005
Steel - Standard 1.5"φ	12	0.2	-2.2	0.5	-0.8	-3.4	-1.7
Steel - Standard 1.5"φ	15	0.7	-2.4	1.0	0.2	-2.1	-2.1
Steel - Standard 1.5"φ	18	0.3	-2.0	0.2	-0.3	-2.2	-2.0
Steel - Elliptical - Medium	12	0.7	-1.9	0.6	-0.4	-1.8	-1.8
Steel - Elliptical - Medium	15	-0.3	-2.3	-0.4	-2.0	-2.9	-3.1
Steel - Elliptical - Medium	18	-0.2	-2.6	-0.5	-1.8	-2.4	-3.0
Steel - Elliptical - Heavy	12	0.1	-1.6	-0.7	-1.4	-2.1	-2.5
Steel - Elliptical - Heavy	15	-0.2	-2.0	0.1	-2.1	-2.2	-3.0
Steel - Elliptical - Heavy	18	0.3	-2.2	0.7	-2.2	-2.4	-2.7

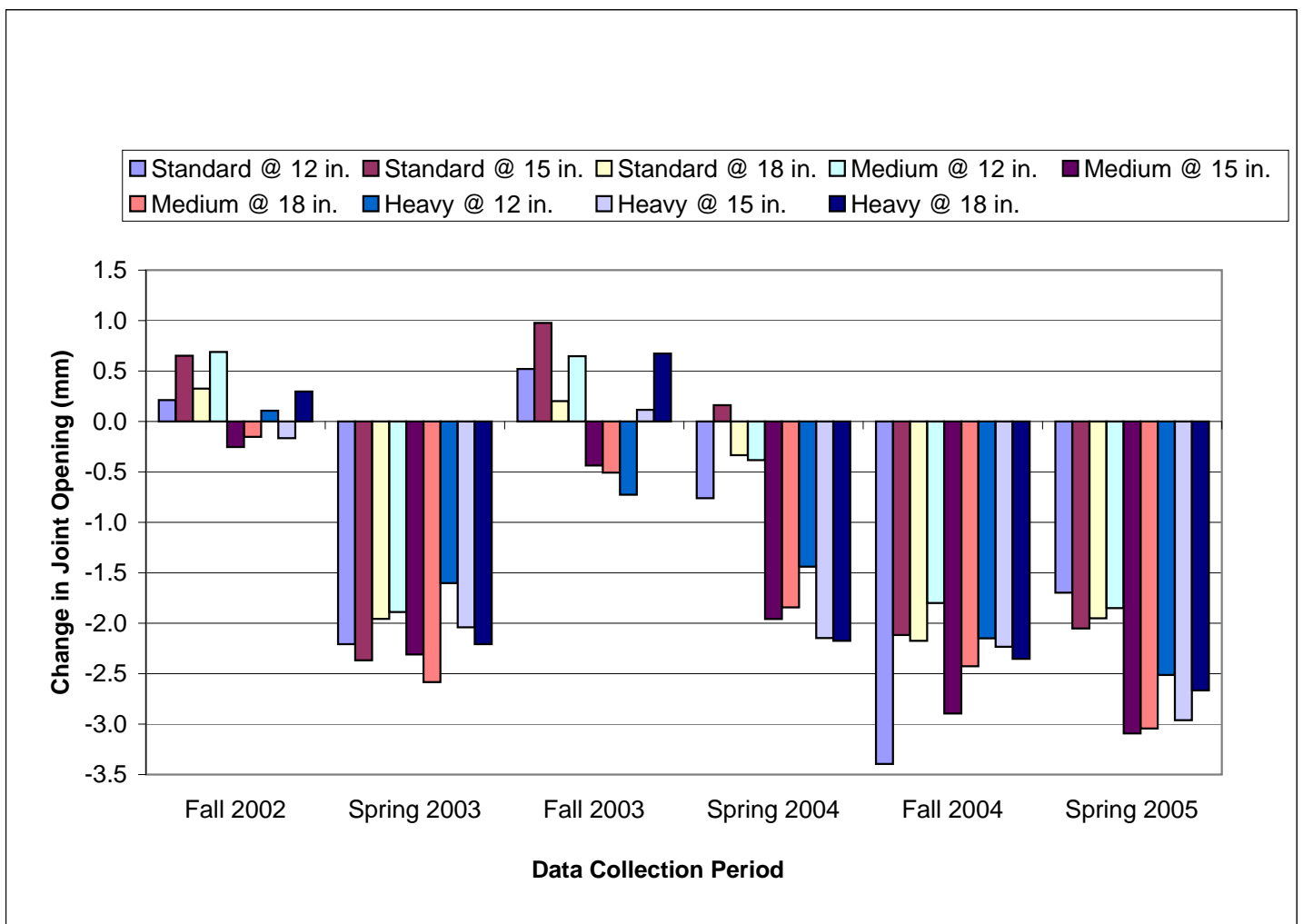


Figure G.1. Changes in joint opening averages, steel dowels